

Video Segment

From Compliant Balancing to
Dynamic Walking, ATR/NICT,
Japan, ICRA 2010

Dynamics

- Rigid Body Dynamics
- Newton-Euler Formulation
- Articulated Multi-Body Dynamics
- Recursive Algorithm
- Lagrange Formulation
- Explicit Form



MA23

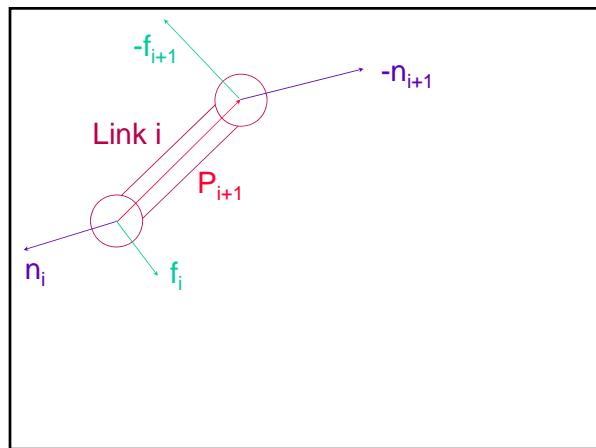
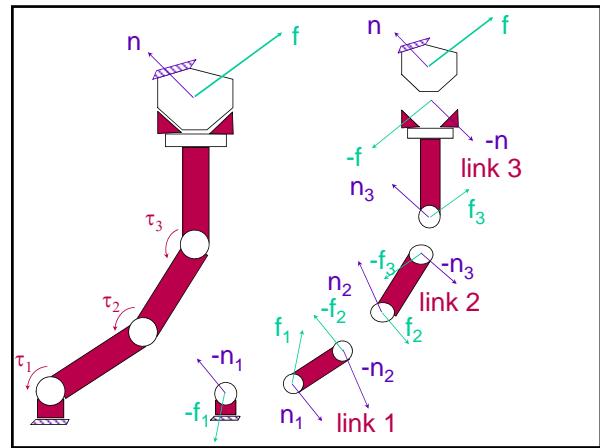
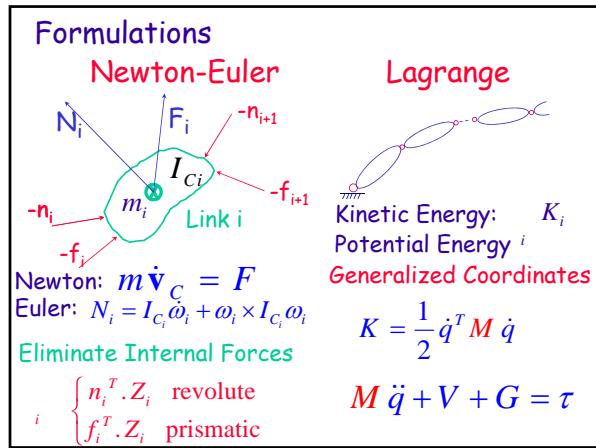
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DESCRIPTIVE EQUATIONS OF MOTION
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$$\begin{aligned} \dot{x}_{11} &= \ddot{x}_{11} + \eta_{11}x_{11}^2 - \eta_{12}x_{12}^2 - \eta_{13}x_{13}^2 - \eta_{14}x_{14}^2 + \eta_{15}x_{15}^2 + \eta_{16}x_{16}^2 + \eta_{17}x_{17}^2 + \eta_{18}x_{18}^2 + \eta_{19}x_{19}^2 + \eta_{20}x_{20}^2 \\ \dot{x}_{12} &= \ddot{x}_{12} + \eta_{11}x_{11}^2 - \eta_{12}x_{12}^2 - \eta_{13}x_{13}^2 - \eta_{14}x_{14}^2 + \eta_{15}x_{15}^2 + \eta_{16}x_{16}^2 + \eta_{17}x_{17}^2 + \eta_{18}x_{18}^2 + \eta_{19}x_{19}^2 + \eta_{20}x_{20}^2 \\ \dot{x}_{13} &= \ddot{x}_{13} + \eta_{11}x_{11}^2 - \eta_{12}x_{12}^2 - \eta_{13}x_{13}^2 - \eta_{14}x_{14}^2 + \eta_{15}x_{15}^2 + \eta_{16}x_{16}^2 + \eta_{17}x_{17}^2 + \eta_{18}x_{18}^2 + \eta_{19}x_{19}^2 + \eta_{20}x_{20}^2 \\ \dot{x}_{14} &= \ddot{x}_{14} + \eta_{11}x_{11}^2 - \eta_{12}x_{12}^2 - \eta_{13}x_{13}^2 - \eta_{14}x_{14}^2 + \eta_{15}x_{15}^2 + \eta_{16}x_{16}^2 + \eta_{17}x_{17}^2 + \eta_{18}x_{18}^2 + \eta_{19}x_{19}^2 + \eta_{20}x_{20}^2 \\ \dot{x}_{15} &= \ddot{x}_{15} + \eta_{11}x_{11}^2 - \eta_{12}x_{12}^2 - \eta_{13}x_{13}^2 - \eta_{14}x_{14}^2 + \eta_{15}x_{15}^2 + \eta_{16}x_{16}^2 + \eta_{17}x_{17}^2 + \eta_{18}x_{18}^2 + \eta_{19}x_{19}^2 + \eta_{20}x_{20}^2 \\ \dot{x}_{16} &= \ddot{x}_{16} + \eta_{11}x_{11}^2 - \eta_{12}x_{12}^2 - \eta_{13}x_{13}^2 - \eta_{14}x_{14}^2 + \eta_{15}x_{15}^2 + \eta_{16}x_{16}^2 + \eta_{17}x_{17}^2 + \eta_{18}x_{18}^2 + \eta_{19}x_{19}^2 + \eta_{20}x_{20}^2 \\ \dot{x}_{17} &= \ddot{x}_{17} + \eta_{11}x_{11}^2 - \eta_{12}x_{12}^2 - \eta_{13}x_{13}^2 - \eta_{14}x_{14}^2 + \eta_{15}x_{15}^2 + \eta_{16}x_{16}^2 + \eta_{17}x_{17}^2 + \eta_{18}x_{18}^2 + \eta_{19}x_{19}^2 + \eta_{20}x_{20}^2 \\ \dot{x}_{18} &= \ddot{x}_{18} + \eta_{11}x_{11}^2 - \eta_{12}x_{12}^2 - \eta_{13}x_{13}^2 - \eta_{14}x_{14}^2 + \eta_{15}x_{15}^2 + \eta_{16}x_{16}^2 + \eta_{17}x_{17}^2 + \eta_{18}x_{18}^2 + \eta_{19}x_{19}^2 + \eta_{20}x_{20}^2 \\ \dot{x}_{19} &= \ddot{x}_{19} + \eta_{11}x_{11}^2 - \eta_{12}x_{12}^2 - \eta_{13}x_{13}^2 - \eta_{14}x_{14}^2 + \eta_{15}x_{15}^2 + \eta_{16}x_{16}^2 + \eta_{17}x_{17}^2 + \eta_{18}x_{18}^2 + \eta_{19}x_{19}^2 + \eta_{20}x_{20}^2 \\ \dot{x}_{20} &= \ddot{x}_{20} + \eta_{11}x_{11}^2 - \eta_{12}x_{12}^2 - \eta_{13}x_{13}^2 - \eta_{14}x_{14}^2 + \eta_{15}x_{15}^2 + \eta_{16}x_{16}^2 + \eta_{17}x_{17}^2 + \eta_{18}x_{18}^2 + \eta_{19}x_{19}^2 + \eta_{20}x_{20}^2 \\ \end{aligned}$$

Joint Space Dynamics

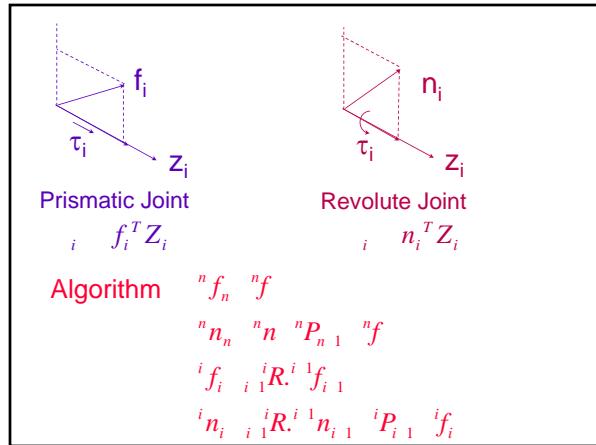
$$M(q)\ddot{q} + V(q, \dot{q}) + G(q) = \Gamma$$

- q :** Generalized Joint Coordinates
- $M(q)$:** Mass Matrix - Kinetic Energy Matrix
- $V(q, \dot{q})$:** Centrifugal and Coriolis forces
- $G(q)$:** Gravity forces
- Γ :** Generalized forces



Link i

Static Equilibrium
 $\Sigma \text{ forces} = 0$
 $\Sigma \text{ moments / a point} = 0$
 About origin {i}
 $f_i = (-f_{i+1}) = 0$
 $n_i = (-n_{i+1}) = P_{i+1} = (-f_{i+1}) = 0$
 $\parallel f_i = f_{i+1}$
 $\parallel n_i = n_{i+1} = P_{i+1} = f_{i+1}$

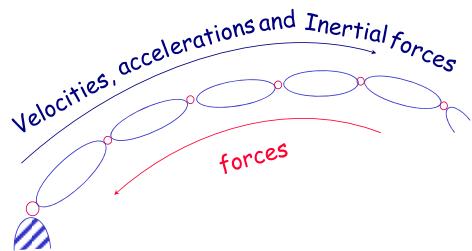


Link i

Recursive Equations

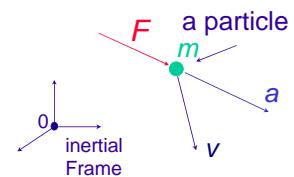
$$\begin{array}{|c|c|c|} \hline & f_i & F_i & f_{i-1} \\ \hline & n_i & N_i & n_{i-1} \\ \hline & \parallel & \parallel & \parallel \\ \hline & \begin{cases} \mathbf{n}_i \cdot \mathbf{Z}_i & \text{revolute} \\ \mathbf{f}_i \cdot \mathbf{Z}_i & \text{prismatic} \end{cases} & \mathbf{p}_{C_i} & \mathbf{F}_i \\ \hline \end{array}$$

Newton-Euler Algorithm



Newton's Law

$$\underline{F} = m\underline{a}$$



$$\frac{d}{dt}(mv) = \underline{F}$$

Linear Momentum
 $\phi = mv$

rate of change of the linear momentum is equal to the applied force

Angular Momentum

$$m\dot{\underline{v}} = \underline{F}$$

take the moment /0

$$\frac{d}{dt}(\underline{p} - mv) = \underline{p} - m\dot{\underline{v}} + \underline{N}$$

$\frac{d}{dt}(\underline{p} \times m\underline{v}) = \underline{N}$

angular momentum $\phi = \underline{p} \times mv$

applied moment

Rigid Body

Rotational Motion

$$\begin{aligned} \text{Angular Momentum} &= \int_V \underline{p} \times (\omega \times \underline{p}) \rho dV \\ &= \int_V \underline{p} \times (\underline{\omega} \times \underline{p}) \rho dV \\ &= \int_V \underline{p} \times \underline{\omega} \rho dV \quad (\because \underline{\omega} \text{ is constant}) \\ &= I \underline{\omega} \end{aligned}$$

$$\phi = \int_V \underline{p} \times (\underline{\omega} \times \underline{p}) \rho dV$$

$$\underline{p} \cdot (\underline{p}) \hat{\underline{p}} \cdot (\hat{\underline{p}})$$

$$\phi = \left[\int_V -\hat{\underline{p}} \hat{\underline{p}} \rho dv \right] \underline{\omega}$$

Inertia Tensor

$$\underline{I}$$

$$I = \int_V \hat{\underline{p}} \hat{\underline{p}} dv$$

Linear Momentum

$$\underline{\phi} = \underline{mv}$$

Newton Equation

$$\frac{d}{dt}(mv) = \underline{F}$$

$$\dot{\underline{\phi}} = \underline{F}$$

$$ma = \underline{F}$$

Angular Momentum

$$\underline{I}$$

Euler Equation

$$\frac{d}{dt}(I\underline{\omega}) = \underline{N}$$

$$\dot{I} \cdot \underline{\omega} = \underline{N}$$

Inertia Tensor

$$I = \int_V \hat{\mathbf{p}}\hat{\mathbf{p}}^T dv = (\hat{\mathbf{p}}\hat{\mathbf{p}})^T (\mathbf{p}^T \mathbf{p}) I_3 \mathbf{p} \mathbf{p}^T$$

$$\mathbf{p} = \begin{bmatrix} x \\ y \\ z \end{bmatrix}; \mathbf{p}^T \mathbf{p} = x^2 + y^2 + z^2$$

$$(\mathbf{p}^T \mathbf{p}) I_3 = \begin{bmatrix} x^2 & xy & xz \\ xy & y^2 & yz \\ xz & yz & z^2 \end{bmatrix}$$

$$\mathbf{p} \mathbf{p}^T = \begin{bmatrix} x & y & z \\ x & y & z \\ x & y & z \end{bmatrix} \begin{bmatrix} x^2 & xy & xz \\ xy & y^2 & yz \\ xz & yz & z^2 \end{bmatrix} = \begin{bmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{bmatrix}$$

$$(-\hat{\mathbf{p}}\hat{\mathbf{p}}) = \begin{bmatrix} y^2 & z^2 & xy & xz \\ xy & z^2 & x^2 & yz \\ xz & yz & x^2 & y^2 \end{bmatrix}$$

Inertia Tensor

$$I = \begin{bmatrix} I_{xx} & I_{xy} & I_{xz} \\ I_{xy} & I_{yy} & I_{yz} \\ I_{xz} & I_{yz} & I_{zz} \end{bmatrix}$$

Moments of Inertia

$$I_{xx} = \iiint (y^2 + z^2) dx dy dz$$

$$I_{yy} = \iiint (z^2 + x^2) dx dy dz$$

$$I_{zz} = \iiint (x^2 + y^2) dx dy dz$$

Products of Inertia

$$I_{xy} = \iiint xy dx dy dz$$

$$I_{xz} = \iiint xz dx dy dz$$

$$I_{yz} = \iiint yz dx dy dz$$

Parallel Axis theorem

$$I = \int_V \hat{\mathbf{p}}\hat{\mathbf{p}}^T dv = (\hat{\mathbf{p}}\hat{\mathbf{p}})^T (\mathbf{p}^T \mathbf{p}) I_3 \mathbf{p} \mathbf{p}^T$$

$$I_A = I_C + m [(\mathbf{p}_c^T \mathbf{p}_c) I_3 - \mathbf{p}_c \mathbf{p}_c^T]$$

$$I_{Azz} = I_{Czz} + m(x_c^2 + y_c^2)$$

$$I_{Axy} = I_{Cxy} + m x_c y_c$$

Example

$$I_{Czz} = \int_{-\frac{a}{2}}^{\frac{a}{2}} \iiint \rho(x^2 + y^2) dx dy dz$$

$$I_{Czz} = \frac{1}{6} \rho a^5; \quad m = a^3$$

$$I_{Cxx} = I_{Cyy} = I_{Czz} = \frac{ma^2}{6}$$

$$I_{Axx} = I_{Ayy} = I_{Azz} = I_{Czz} + \frac{ma^2}{2} = \frac{2}{3} ma^2$$

$$I_{Axy} = I_{Axz} = I_{Ayz} = \frac{ma^2}{4}$$

Newton-Euler Algorithm

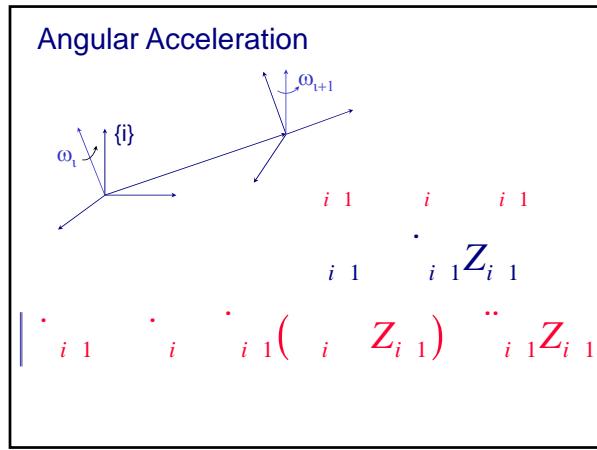
Newton-Euler Equations

Translational Motion

$$m \dot{\mathbf{v}}_C = \mathbf{F}$$

Rotational Motion

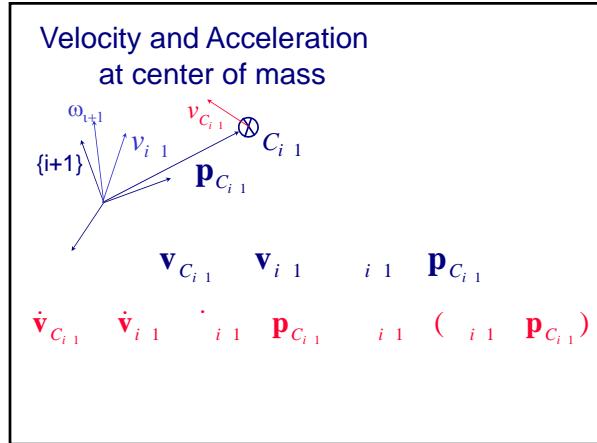
$$I_C \ddot{\omega} + \boldsymbol{\omega} \times I_C \boldsymbol{\omega} = N$$



Linear Acceleration

$$v_{i+1} = v_i + \omega_i \times p_{i+1} + V_{i+1}$$

$$a_{i+1} = a_i + \ddot{\omega}_i \times p_{i+1} + 2\dot{\omega}_i \times \dot{p}_{i+1} + \ddot{V}_{i+1}$$

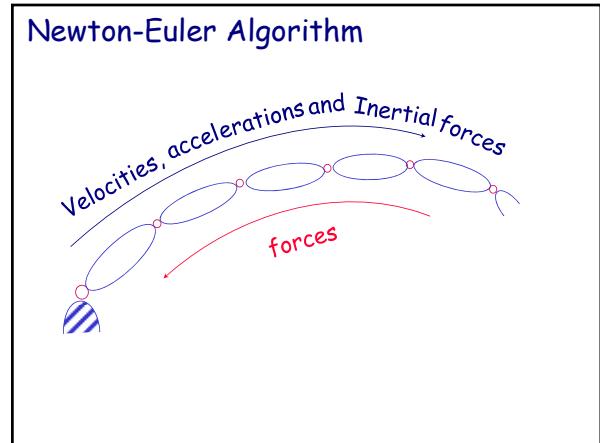
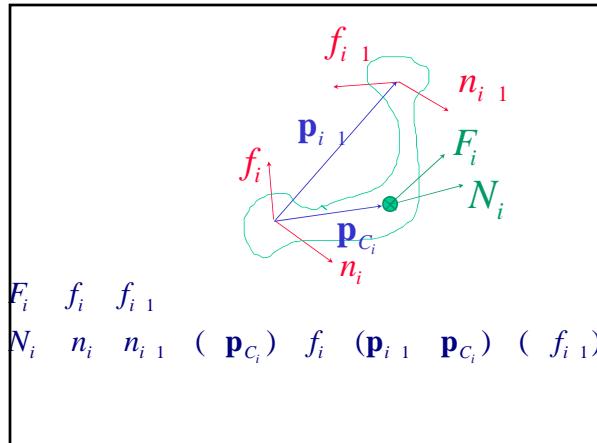


Dynamic forces on Link i

$$I_{Ci}\dot{\omega}_i + \omega_i \times I_{Ci}\omega_i = \sum \text{moments / } c_i$$

$$F_i = m_i \dot{v}_{C_i}$$

$$N_i = I_{Ci}\dot{\omega}_i + \omega_i \times I_{Ci}\omega_i$$



Recursive Equations

$$\begin{aligned}
 & f_i = F_i - f_{i-1} \\
 & n_i = N_i - n_{i-1} - \mathbf{p}_{C_i} \cdot F_i - \mathbf{p}_{i-1} \cdot f_{i-1} \\
 & \quad \begin{cases} n_i \cdot Z_i \text{ revolute} \\ f_i \cdot Z_i \text{ prismatic} \end{cases} \\
 & \text{with } F_i = m_i \dot{\mathbf{v}}_{C_i} \\
 & N_i = I_{Ci} \ddot{\omega}_i + \boldsymbol{\omega}_i \times I_{Ci} \boldsymbol{\omega}_i
 \end{aligned}$$

where

$$\begin{aligned}
 & \dot{\mathbf{v}}_i = \dot{\mathbf{v}}_{i-1} + \mathbf{p}_{i-1} - \mathbf{p}_i - (\mathbf{r}_i - \mathbf{r}_{i-1}) \cdot 2\dot{\mathbf{d}}_{i-1} - \mathbf{Z}_{i-1} \cdot \ddot{\mathbf{d}}_{i-1} \mathbf{Z}_i \\
 & \ddot{\mathbf{v}}_{C_i} = \dot{\mathbf{v}}_{i-1} + \mathbf{p}_{C_{i-1}} - \mathbf{p}_{C_i} - (\mathbf{r}_{C_i} - \mathbf{r}_{C_{i-1}}) \cdot (\mathbf{r}_{C_i} - \mathbf{r}_{C_{i-1}})
 \end{aligned}$$

Outward iterations: $i : 0 \rightarrow 5$

$$\begin{aligned}
 & {}^{i+1}f_i = {}^iR^{i+1}f_i - {}^iR^{i+1}\mathbf{Z}_{i+1} \\
 & {}^{i+1}\dot{\mathbf{v}}_i = {}^iR^{i+1}(\dot{\mathbf{v}}_{i+1} - {}^iR^{i+1}\mathbf{p}_{i+1} - {}^iR^{i+1}(\mathbf{r}_{i+1} - \mathbf{r}_i) \cdot {}^i\dot{\mathbf{v}}_i) \\
 & {}^{i+1}\dot{\mathbf{v}}_{C_{i+1}} = {}^{i+1}(\mathbf{p}_{C_{i+1}} - {}^{i+1}R^{i+1}(\mathbf{r}_{C_{i+1}} - \mathbf{r}_{C_i}) \cdot {}^{i+1}\dot{\mathbf{v}}_{C_i}) - {}^{i+1}\dot{\mathbf{v}}_{i+1} \\
 & {}^{i+1}F_i = m_i {}^{i+1}\dot{\mathbf{v}}_{C_i} \\
 & {}^{i+1}N_{i+1} = {}^{C_{i+1}}I_{i+1}({}^{i+1}\dot{\mathbf{v}}_{i+1} - {}^{i+1}R^{i+1}(\mathbf{r}_{C_{i+1}} - \mathbf{r}_{C_i}) \cdot {}^{i+1}\dot{\mathbf{v}}_{C_i})
 \end{aligned}$$

Inward iterations: $i : 6 \rightarrow 1$

$$\begin{aligned}
 & {}^if_i = {}^{i-1}R^if_i - {}^iF_i \\
 & {}^in_i = {}^{i-1}N_{i-1} - {}^{i-1}R^{i-1}n_{i-1} - {}^i\mathbf{p}_{C_i} \cdot {}^iF_i - {}^i\mathbf{p}_{i-1} \cdot {}^{i-1}R^{i-1}f_{i-1} \\
 & {}^in_i \cdot {}^i\mathbf{n}^T \mathbf{Z}_i \quad \text{Gravity: set } {}^0\dot{\mathbf{v}}_0 = 1G
 \end{aligned}$$