

Video Segment

SCHAFT: DARPA Robotics Challenge 8 Tasks + Special Walking, 2013

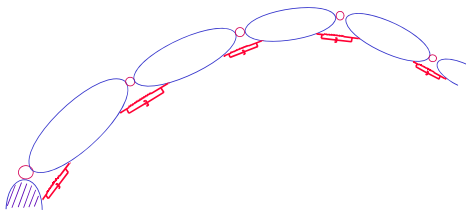


Robot Control

Control

- Natural Systems
- PID Control
- Joint-Space Dynamic Control
- Task-Oriented Control
- Force Control

Joint-Space Control



Proportional-Derivative Control (PD)

$$m\ddot{x} + k_v\dot{x} + k_p(x - x_d) = 0$$

Velocity gain Position gain

$$1. \ddot{x} + \frac{k_v}{m}\dot{x} + \frac{k_p}{m}(x - x_d) = 0$$

$$1. \ddot{x} + 2\xi\omega\dot{x} + \omega^2(x - x_d) = 0$$

$\frac{k_v}{2\sqrt{k_p m}}$ closed loop damping ratio

$\sqrt{\frac{k_p}{m}}$ closed loop frequency

Gains

$$k_p \quad m^{-2}$$

$$k_v \quad m^{-1}$$

Gain Selection

$$\text{set } \begin{pmatrix} k_p \\ k_v \end{pmatrix} \begin{matrix} m^{-2} \\ m^{-1} \end{matrix}$$

Unit mass system **m - mass system**

$$k_p \quad 2 \quad \quad \quad k_p \quad m \quad k_p$$

$$k_v \quad 2 \quad \quad \quad k_v \quad m \quad k_v$$

Control Partitioning

$$m\ddot{x} = f \implies m(1.\ddot{x}) = m f'$$

$$f = -k_v\dot{x} - k_p(x - x_d)$$

$$f = m[-k'_v\dot{x} - k'_p(x - x_d)] = m f'$$

$$m\ddot{x} = m f' \quad f'$$

1. $\ddot{x} = f'$ unit mass system

$$1.\ddot{x} + k'_v\dot{x} + k'_p(x - x_d) = 0$$

$$2 \quad \uparrow \quad \quad \uparrow_2$$

Non Linearities

$$m\ddot{x} = b(x, \dot{x}) + f$$

Control Partitioning

with \hat{m}

$$m\ddot{x} = b(x, \dot{x}) + \hat{m}f + \hat{b}(x, \dot{x})$$

$$\rightarrow 1.\ddot{x} = f$$

Unit mass system

Motion Control

$$m\ddot{x} = b(x, \dot{x}) + f \implies 1.\ddot{x} = f/b$$

Goal Position (x_d):

Control: $f = k_v\dot{x} + k_p(x - x_d)$

Closed-loop System: $1.\ddot{x} + k_v\dot{x} + k_p(x - x_d) = 0$

Trajectory Tracking

$x_d(t)$; $\dot{x}_d(t)$; and $\ddot{x}_d(t)$

Control: $f = \ddot{x}_d + k_v(\dot{x} - \dot{x}_d) + k_p(x - x_d)$

Closed-loop System:

$$(\ddot{x} - \ddot{x}_d) + k_v(\dot{x} - \dot{x}_d) + k_p(x - x_d) = 0$$

with $e = x - x_d$

$$\ddot{e} + k_v\dot{e} + k_p e = 0$$

Disturbance Rejection

$$\ddot{x}_d = m\ddot{x} = b(x, \dot{x}) + f$$

$$\ddot{e} + k_v\dot{e} + k_p e = 0$$

Disturbance Rejection

$$\ddot{x}_d = m\ddot{x} = b(x, \dot{x}) + f$$

Control $f = m\ddot{x} - b(x, \dot{x}) + f_{dist}$

Closed loop $\ddot{e} + k_v\dot{e} + k_p e = \frac{f_{dist}}{m}$

bounded $\{ |f_{dist}| \leq a \}$

Steady-State Error

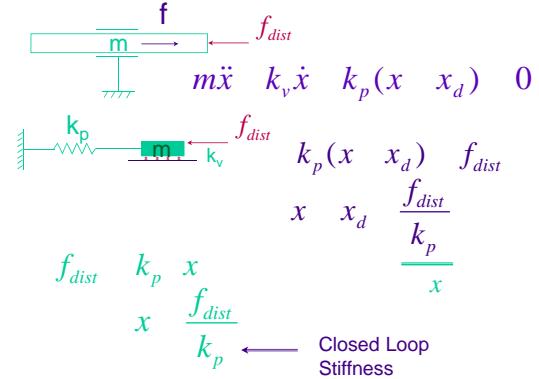
$$\ddot{e} + k_v \dot{e} + k_p e = \frac{f_{dist}}{m}$$

The steady-state ($\dot{e} = \ddot{e} = 0$):

$$e = \frac{f_{dist}}{mk_p} = \frac{f_{dist}}{k_p} \cdot \frac{1}{m}$$

Closed loop position gain (stiffness)

Steady-State Error - Example



PID (adding Integral action)

System $m\ddot{x} + b(x, \dot{x}) = f - f_{dist}$

Control $f = mf + b(x, \dot{x})$

$f = \ddot{x}_d + k_v(\dot{x} - \dot{x}_d) + k_p(x - x_d) + k_i \int (x - x_d) dt$

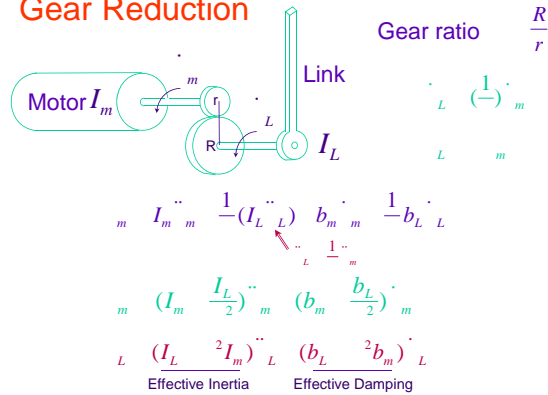
Closed-loop System

$$\ddot{e} + k_v \dot{e} + k_p e + k_i \int e dt = \frac{f_{dist}}{m}$$

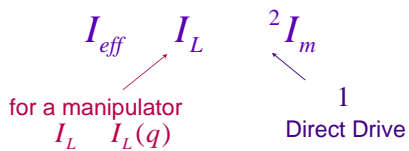
consistent

Steady-state Error $e = 0$

Gear Reduction



Effective Inertia



Gain Selection

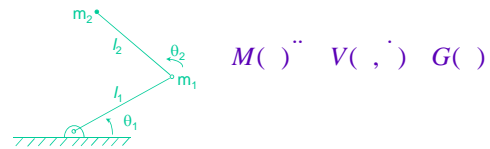
$$k_p = (I_L + 2I_m)k_p$$

$$k_v = (I_L + 2I_m)k_v$$

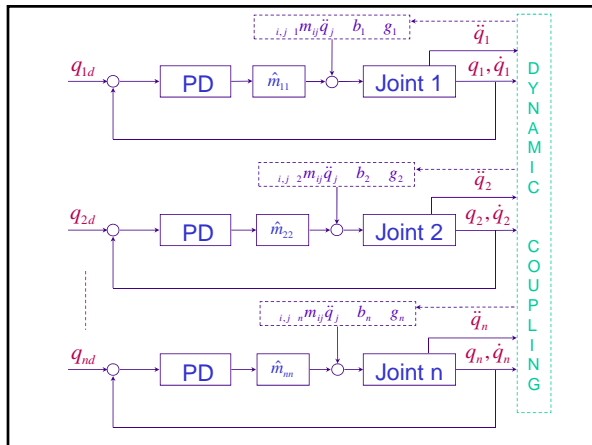
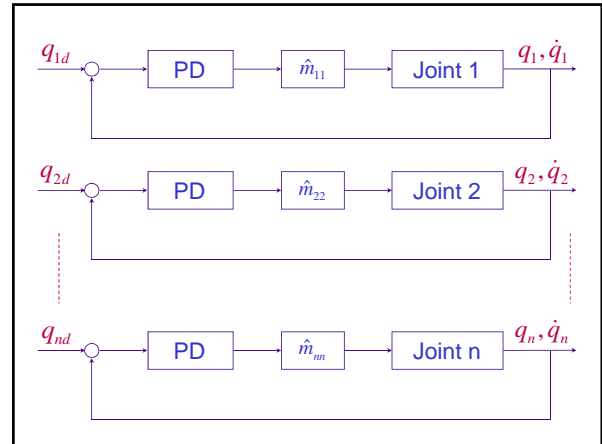
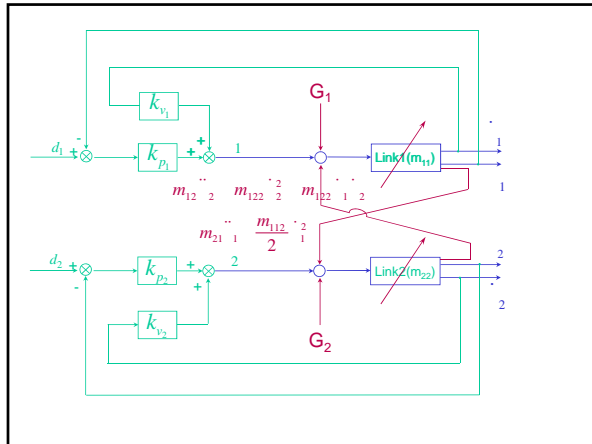
Time Optimal Selection

$$\hat{I}_L = \frac{1}{4} (\sqrt{I_{L_{min}}} + \sqrt{I_{L_{max}}})^2$$

Manipulator Control



$$\begin{pmatrix} m_{11} & m_{12} \\ m_{21} & m_{22} \end{pmatrix} \begin{pmatrix} \ddot{\theta}_1 \\ \ddot{\theta}_2 \end{pmatrix} + \begin{pmatrix} m_{112} \\ 0 \end{pmatrix} \begin{pmatrix} \dot{\theta}_1 \\ \dot{\theta}_2 \end{pmatrix} + \begin{pmatrix} 0 & m_{122} \\ \frac{m_{112}}{2} & 0 \end{pmatrix} \begin{pmatrix} \dot{\theta}_1 \\ \dot{\theta}_2 \end{pmatrix} + \begin{pmatrix} G_1 \\ G_2 \end{pmatrix} = \begin{pmatrix} \tau_1 \\ \tau_2 \end{pmatrix}$$



PD Control Stability

$$M(q)\ddot{q} + B(q)[\dot{q}\dot{q}] + C(q)[\dot{q}^2] + G(\theta) = \tau$$

$$\tau = -k_p(q - q_d) - k_v\dot{q}$$

$$V_d = 1/2k_p(q - q_d)^2$$

$$\frac{d}{dt} \left(\frac{\partial K}{\partial \dot{q}} \right) - \frac{\partial K}{\partial q} + \frac{\partial V_s}{\partial q} = \tau - \frac{\partial V_d}{\partial q} - k_v\dot{q}$$

PD Control Stability

$$M(q)\ddot{q} + B(q)[\dot{q}\dot{q}] + C(q)[\dot{q}^2] + G(\theta) = \tau$$

$$\tau = -k_p(q - q_d) - k_v\dot{q}$$

$$V_d = 1/2k_p(q - q_d)^T(q - q_d)$$

$$\frac{d}{dt} \left(\frac{\partial K}{\partial \dot{q}} \right) - \frac{\partial K}{\partial q} + \frac{\partial (V_s - V_d)}{\partial q} = \tau_s$$

$\tau_s = -k_v\dot{q}$ with $\tau_s^T \dot{q} < 0$ for $\dot{q} \neq 0$; $k_v > 0$

Performance

High Gains \rightarrow better disturbance rejection

Gains are limited by

- structural flexibilities
- time delays (actuator-sensing)
- sampling rate

$n \frac{res}{2}$ \leftarrow lowest structural flexibility

$n \frac{delay}{3}$ \leftarrow largest delay $\left(\frac{2}{delay} \right)$

$n \frac{sampling\ rate}{5}$

Nonlinear Dynamic Decoupling

$$M(q) \ddot{q} + V(q, \dot{q}) = G(q)$$

$$\hat{M}(q) \ddot{q} + \hat{V}(q, \dot{q}) = \hat{G}(q)$$

1. $\ddot{q} = (M^{-1} \hat{M}) \ddot{q} + M^{-1} [V - \hat{V}] + (G - \hat{G})$
 with perfect estimates

$$\ddot{q} = \ddot{q}_d + k_v \dot{e} + k_p e \quad (t)$$

\ddot{q}_d : input of the unit-mass systems

$$\ddot{q}_d = \ddot{q}_d + k_v \dot{e} + k_p e$$

Closed-loop

$$\ddot{E} + k_v \dot{E} + k_p E = 0 \quad (t)$$

