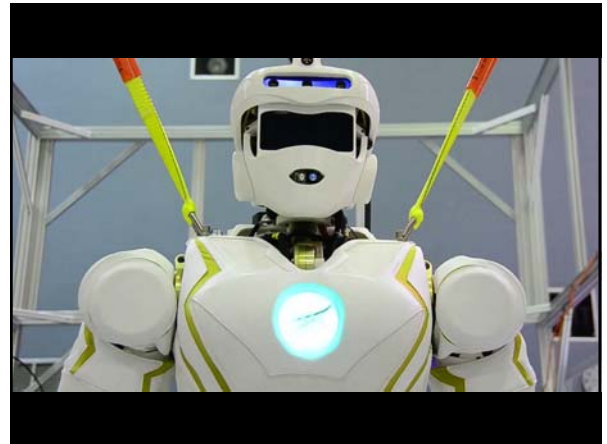


Video Segment

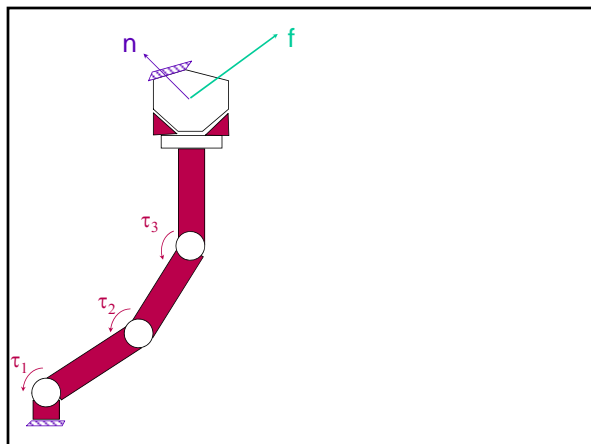
Valkyrie: NASA's Superhero Robot, IEEE Spectrum, 2013



Robot Control

Control

- Natural Systems
- PID Control
- Joint-Space Dynamic Control
- Task-Oriented Control
- Force Control



Velocity/Force Duality

$$\dot{x} = J \dot{\theta}$$

$$\tau = J^T F$$

Example (Static Forces)

$$J = \begin{pmatrix} -(l_1 s_1 + l_2 s_12) & -l_2 s_12 \\ l_1 c_1 + l_2 c_12 & l_2 c_12 \end{pmatrix}$$

$$J^T = \begin{pmatrix} -(l_1 s_1 + l_2 s_12) & l_1 c_1 + l_2 c_12 \\ -l_2 s_12 & l_2 c_12 \end{pmatrix}$$

$\tau = J^T F$

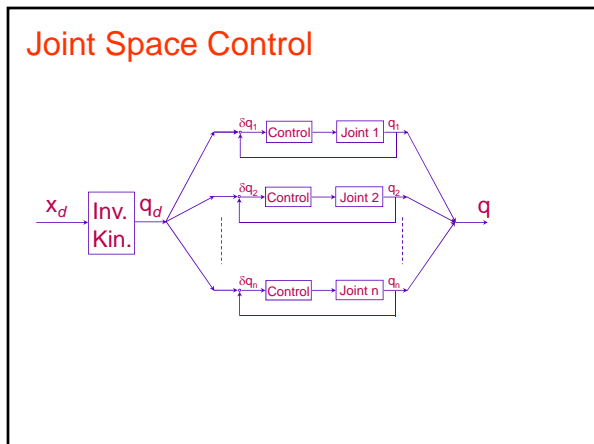
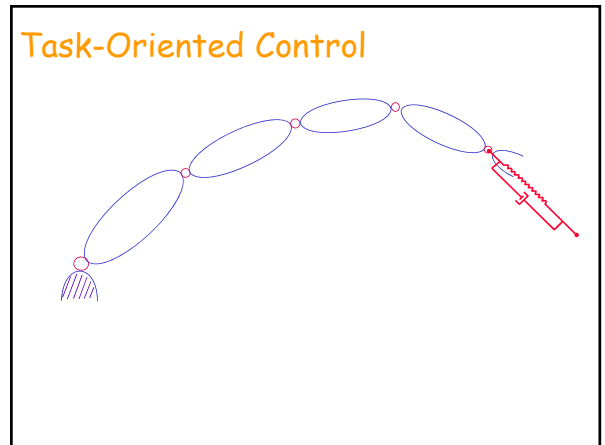
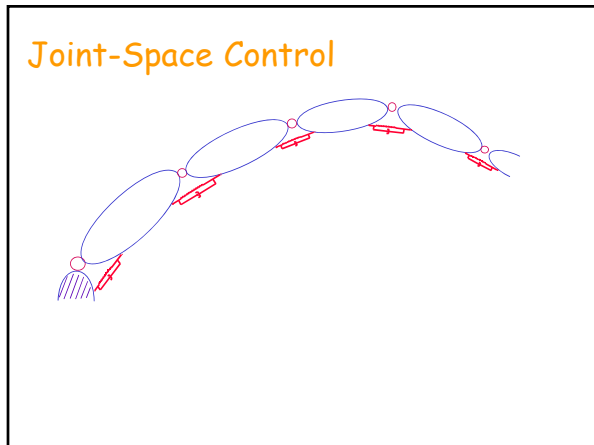
$l_1 = l_2 = 1; \theta_1 = 0; \theta_2 = 60^\circ$

$$\tau = \begin{pmatrix} -(l_1 s_1 + l_2 s_12) & l_1 c_1 + l_2 c_12 \\ -l_2 s_12 & l_2 c_12 \end{pmatrix} \begin{bmatrix} 0 \\ -1 \end{bmatrix} = - \begin{bmatrix} l_1 c_1 + l_2 c_12 \\ l_2 c_12 \end{bmatrix} = - \begin{bmatrix} 3/2 \\ 1/2 \end{bmatrix}$$

Example (Static Forces)

$$\tau = \begin{pmatrix} -(l_1 s_1 + l_2 s_12) & l_1 c_1 + l_2 c_12 \\ -l_2 s_12 & l_2 c_12 \end{pmatrix} \begin{bmatrix} 0 \\ -1000 \end{bmatrix} = \begin{bmatrix} l_1 c_1 + l_2 c_12 \\ l_2 c_12 \end{bmatrix} (-1000) = \begin{bmatrix} 0 \\ 0 \end{bmatrix}$$

$l_1 = l_2 = 1; \theta_1 = 90; \theta_2 = 0^\circ$



Resolved Motion Rate Control (Whitney 72)

$$\dot{x} = J(\theta) \dot{\theta}$$

Outside singularities

$$\dot{\theta} = J^{-1}(\theta) \dot{x}$$

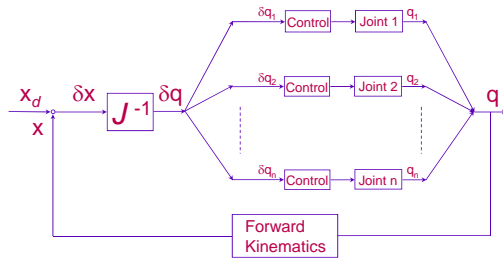
Arm at Configuration

$$\dot{x} = f(\theta)$$

$$\dot{x} = \dot{x}_d$$

$$\dot{\theta} = J^{-1}(\theta) \dot{x}_d$$

Resolved Motion Rate Control



Natural Systems

Conservative Systems



$$\frac{d}{dt} \left(\frac{\partial(K-V)}{\partial \dot{x}} \right) - \frac{\partial(K-V)}{\partial x} = 0 \quad K = \frac{1}{2} m \dot{x}^2$$

Natural Systems

Conservative Forces



$$\frac{d}{dt} \left(\frac{\partial K}{\partial \dot{x}} \right) - \frac{\partial K}{\partial x} = - \frac{\partial V}{\partial x}$$

$$m \ddot{x} = F = -kx$$

Potential Energy of a spring

$$V = \text{Work} = \int_x^0 (-kx) \delta x = \frac{1}{2} kx^2$$

Natural Systems

Conservative Forces



$$\frac{d}{dt} \left(\frac{\partial K}{\partial \dot{x}} \right) - \frac{\partial K}{\partial x} = - \frac{\partial V}{\partial x}$$

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Natural Systems

Conservative Systems



$$\frac{d}{dt} \left(\frac{\partial(K-V)}{\partial \dot{x}} \right) - \frac{\partial(K-V)}{\partial x} = 0 \quad K = \frac{1}{2} m \dot{x}^2$$

$$m \ddot{x} + kx = 0$$

$$V = \frac{1}{2} kx^2$$

Natural Systems

Conservative Systems

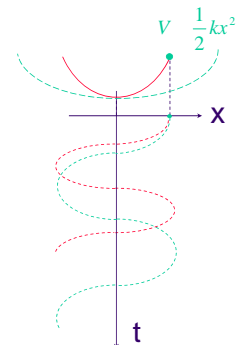
$$m \ddot{x} + kx = 0$$

Frequency increases with stiffness and inverse mass

$$\text{Natural Frequency } \omega_n = \sqrt{\frac{k}{m}}$$

$$\ddot{x} + \omega_n^2 x = 0$$

$$x(t) = c \cos(\omega_n t)$$



Natural Systems

Dissipative Systems

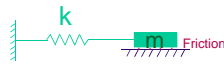


$$\frac{d}{dt} \left(\frac{\partial(K-V)}{\partial \dot{x}} \right) - \frac{\partial(K-V)}{\partial x} = f_{friction}$$

Viscous friction: $f_{friction} = b\dot{x}$

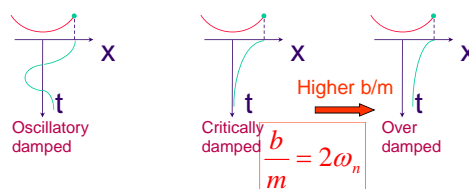
$$m\ddot{x} + b\dot{x} + kx = 0$$

Dissipative Systems



$$m\ddot{x} + b\dot{x} + kx = 0$$

$$\ddot{x} + \frac{b}{m}\dot{x} + \frac{k}{m}x = 0$$



2nd order systems

$$m\ddot{x} + b\dot{x} + kx = 0$$

$$\ddot{x} + \frac{b}{m}\dot{x} + \frac{k}{m}x = 0$$

$$\frac{b/m}{2\omega_n}$$

Critically damped when $b/m = 2\omega_n$

Natural damping ratio

$$\zeta = \frac{b}{2\omega_n m} = \frac{b}{2\sqrt{km}}$$

Critically damped system: $\zeta = 1$ ($b = 2\sqrt{km}$)

Time Response

$$\ddot{x} + 2\zeta\omega_n\dot{x} + \omega_n^2x = 0$$

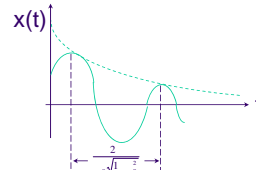
Natural frequency

$$\omega_n = \sqrt{\frac{k}{m}}$$

Natural damping ratio

$$\zeta = \frac{b}{2\sqrt{km}}$$

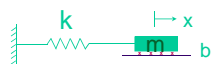
$$x(t) = e^{-\zeta\omega_n t} \cos(\omega_n \sqrt{1-\zeta^2} t)$$



damped Natural frequency

$$\omega = \omega_n \sqrt{1-\zeta^2}$$

Example



$m = 2.0$

$b = 4.8$

$k = 8.0$

$$m\ddot{x} + b\dot{x} + kx = 0$$

what is the "damped Natural frequency"

$$\omega = \omega_n \sqrt{1-\zeta^2} = \sqrt{\frac{k}{m}} \sqrt{1-\left(\frac{b}{2\sqrt{km}}\right)^2} = 1.6$$

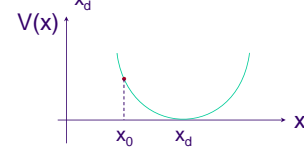
$$\omega = 2\sqrt{1-0.36} = 1.6$$

1-dof Robot Control



$$m\ddot{x} = f$$

Potential Field



$$V(x) = \frac{1}{2}k_p(x - x_d)^2$$

$$V(x) = \frac{1}{2}k_p(x - x_d)^2$$

$$V(x) = \frac{1}{2}k_p(x - x_d)^2; f = -\frac{dV(x)}{dx}$$

$$m\ddot{x} = -\left[\frac{1}{2}k_p(x - x_d)^2\right]; m\ddot{x} = k_p(x - x_d) = 0$$

Position gain

Passive Systems (Stability)

$$V_{goal} = \frac{1}{2} k_p (x - x_g)^T (x - x_g)$$

System $\frac{d}{dt} \left(\frac{\partial K}{\partial \dot{x}} \right) - \frac{\partial K}{\partial x} = f$

$$\Downarrow f = -\frac{\partial V_{goal}}{\partial x}$$

$$\frac{d}{dt} \left(\frac{\partial K}{\partial \dot{x}} \right) - \frac{\partial (K - V_{goal})}{\partial x} = 0 \quad \text{Conservative Forces}$$

Stable

Asymptotic Stability

a system $\frac{d}{dt} \left(\frac{\partial K}{\partial \dot{x}} \right) - \frac{\partial (K - V_{goal})}{\partial x} = 0_s$

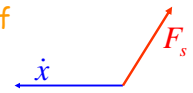
is asymptotically stable if

$$F_s^T \dot{x} < 0 \quad ; \quad \text{for } \dot{x} \neq 0$$

$$F_s = -k_v \dot{x} \rightarrow k_v > 0$$

Control

$$F = -k_p (x - x_{goal}) - k_v \dot{x}$$



Proportional-Derivative Control (PD)

$$m\ddot{x} + f + k_p(x - x_d) + k_v\dot{x} = 0$$

$$m\ddot{x} + k_v\dot{x} + k_p(x - x_d) = 0$$

Velocity gain Position gain

$$1. \ddot{x} + \frac{k_v}{m} \dot{x} + \frac{k_p}{m} (x - x_d) = 0$$

$$1. \ddot{x} + 2\xi\omega\dot{x} + \omega^2(x - x_d) = 0$$

$$\frac{k_v}{2\sqrt{k_p m}} \quad \text{closed loop damping ratio} \quad \sqrt{\frac{k_p}{m}} \quad \text{closed loop frequency}$$

Gains

$$k_p \quad m^2$$

$$k_v \quad m(2 \quad)$$

Gain Selection

$$\text{set} \left(\begin{matrix} k_p & m^2 \\ k_v & m(2 \quad) \end{matrix} \right)$$

Unit mass system

$$k_p \quad 2$$

$$k_v \quad 2$$

m - mass system

$$k_p \quad m \cdot k_p$$

$$k_v \quad m \cdot k_v$$

Control Partitioning

$$m\ddot{x} + f \implies m(1.\ddot{x}) = m f'$$

$$f = -k_v\dot{x} - k_p(x - x_d)$$

$$f = m[-k'_v\dot{x} - k'_p(x - x_d)] = m f'$$

$$m\ddot{x} = m f' \quad f$$

1. $\ddot{x} + f$ unit mass system

$$1.\ddot{x} + k'_v\dot{x} + k'_p(x - x_d) = 0$$

$$2 \quad \uparrow \quad \uparrow_2$$