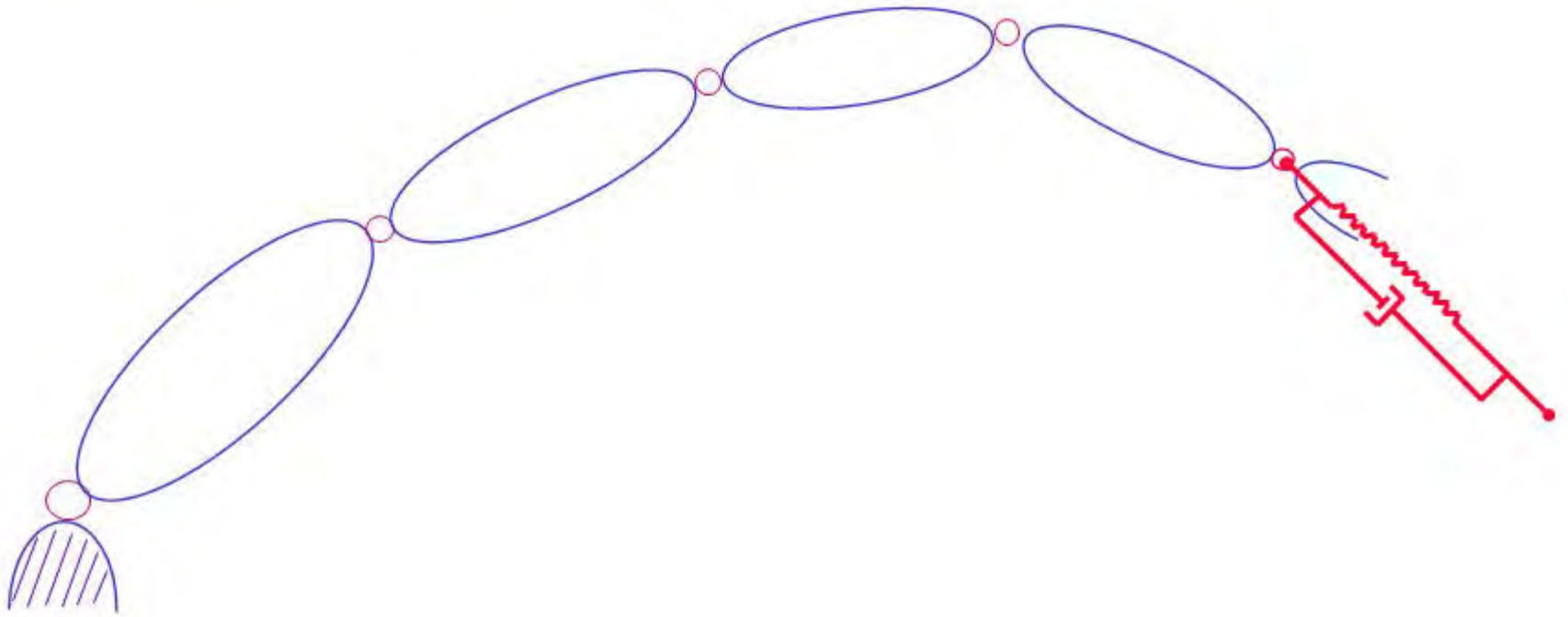


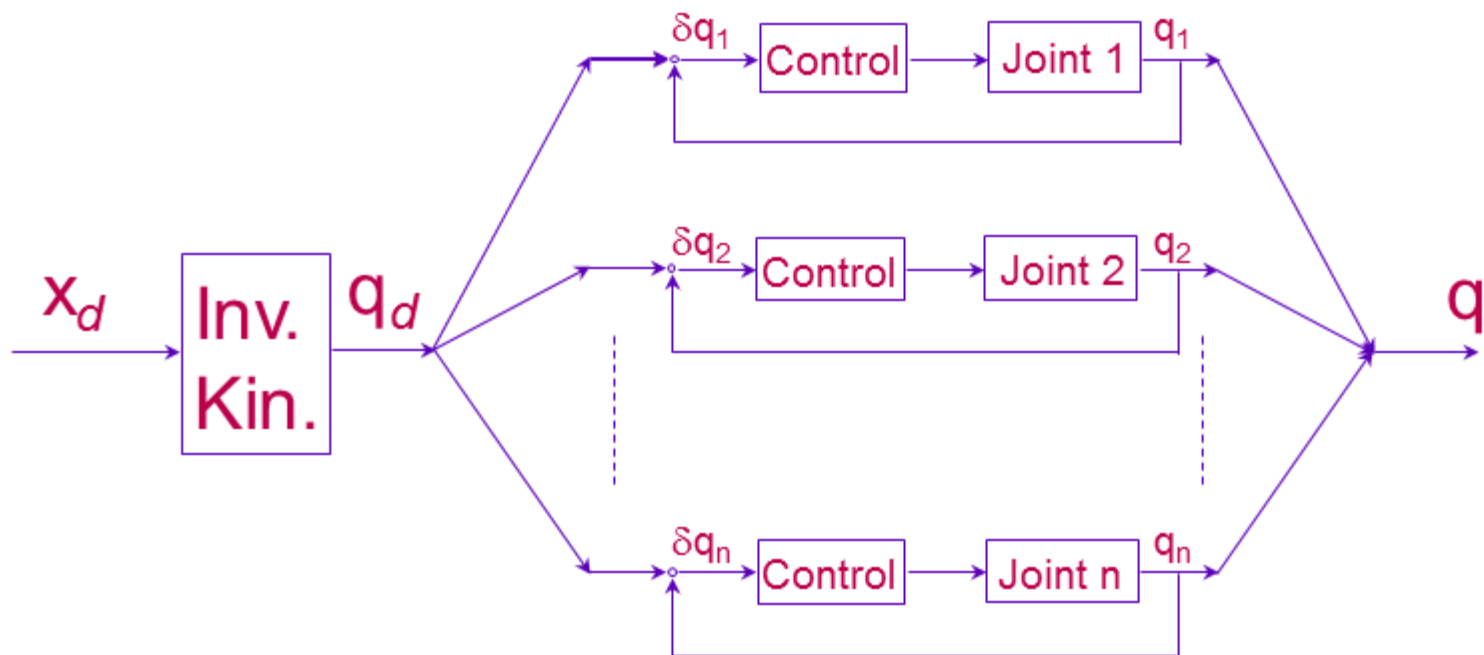
Video Segment

Valkyrie: NASA's Superhero
Robot, IEEE Spectrum, 2013

Task-Oriented Control



Joint Space Control



Resolved Motion Rate Control (Whitney 72)

$$\delta x = J(\theta)\delta\theta$$

Outside singularities

$$\delta\theta = J^{-1}(\theta)\delta x$$

Arm at Configuration θ

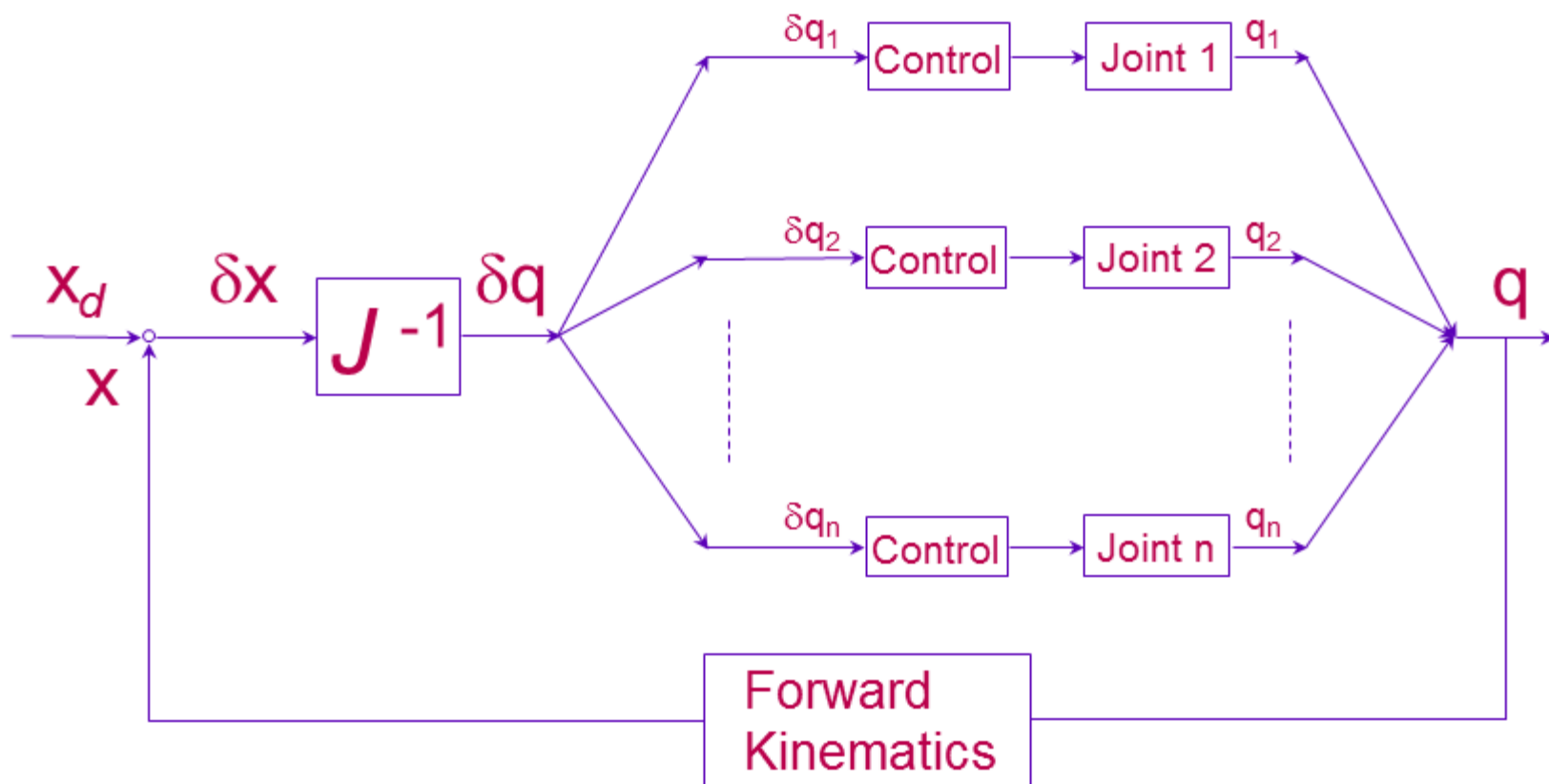
$$x = f(\theta)$$

$$\delta x = x_d - x$$

$$\delta\theta = J^{-1}\delta x$$

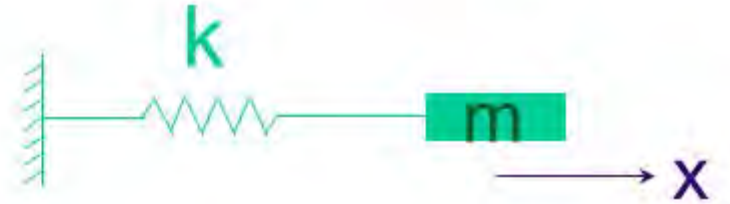
$$\theta^+ = \theta + \delta\theta$$

Resolved Motion Rate Control



Natural Systems

Conservative Systems



$$\frac{d}{dt} \left(\frac{\partial(K-V)}{\partial \dot{x}} \right) - \frac{\partial(K-V)}{\partial x} = 0$$

$$K = \frac{1}{2} m \dot{x}^2$$

Natural Systems

Conservative Forces



$$\frac{d}{dt} \left(\frac{\partial K}{\partial \dot{x}} \right) - \frac{\partial K}{\partial x} = - \frac{\partial V}{\partial x}$$

$$m \ddot{x} = F = -kx$$

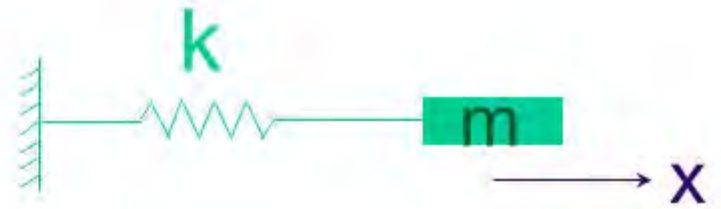
Potential Energy of a spring

$$V = \text{Work} = \int_x^0 (-kx) \delta x = \frac{1}{2} kx^2$$

$$- \frac{\partial}{\partial x} \left(\frac{1}{2} kx^2 \right)$$

Natural Systems

Conservative Forces



$$\frac{d}{dt} \left(\frac{\partial K}{\partial \dot{x}} \right) - \frac{\partial K}{\partial x} = - \frac{\partial V}{\partial x}$$

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Natural Systems

Conservative Systems



$$\frac{d}{dt} \left(\frac{\partial(K-V)}{\partial \dot{x}} \right) - \frac{\partial(K-V)}{\partial x} = 0$$

$$K = \frac{1}{2} m \dot{x}^2$$

$$m \ddot{x} + kx = 0$$

$$V = \frac{1}{2} kx^2$$

Natural Systems

Conservative Systems

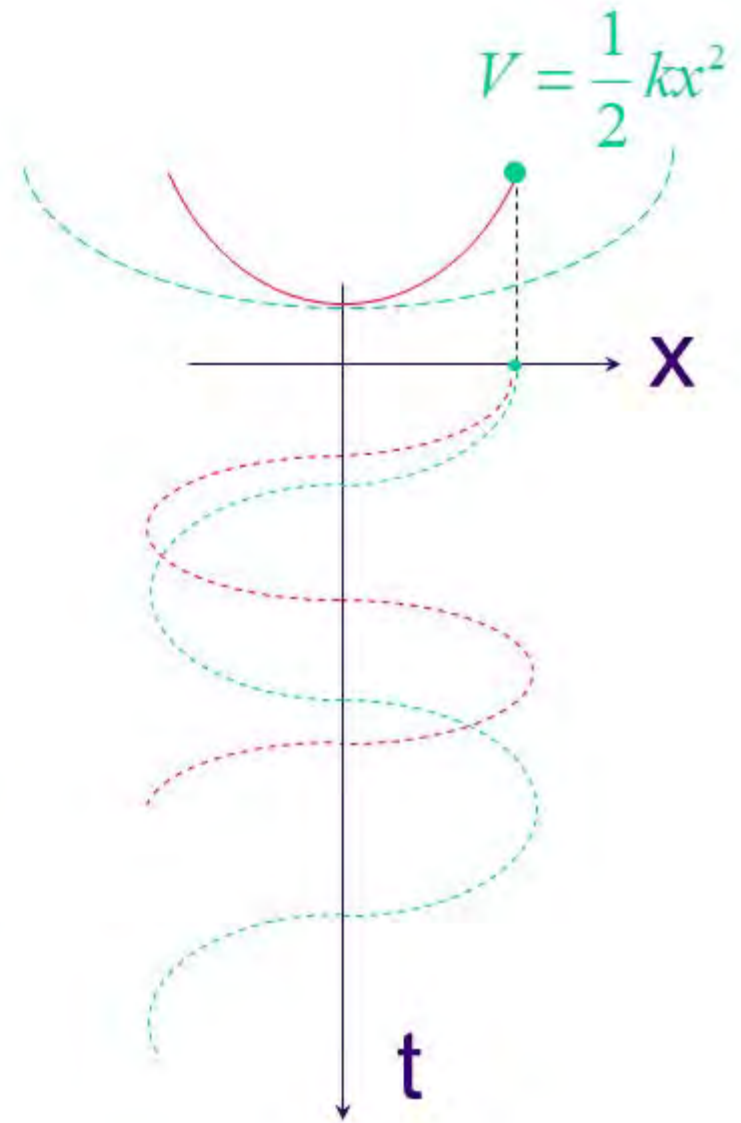
$$m \ddot{x} + kx = 0$$

Frequency increases
with **stiffness**
and **inverse mass**

Natural Frequency $\omega_n = \sqrt{\frac{k}{m}}$

$$\ddot{x} + \omega_n^2 x = 0$$

$$x(t) = c \cos(\omega_n t + \phi)$$



Natural Systems

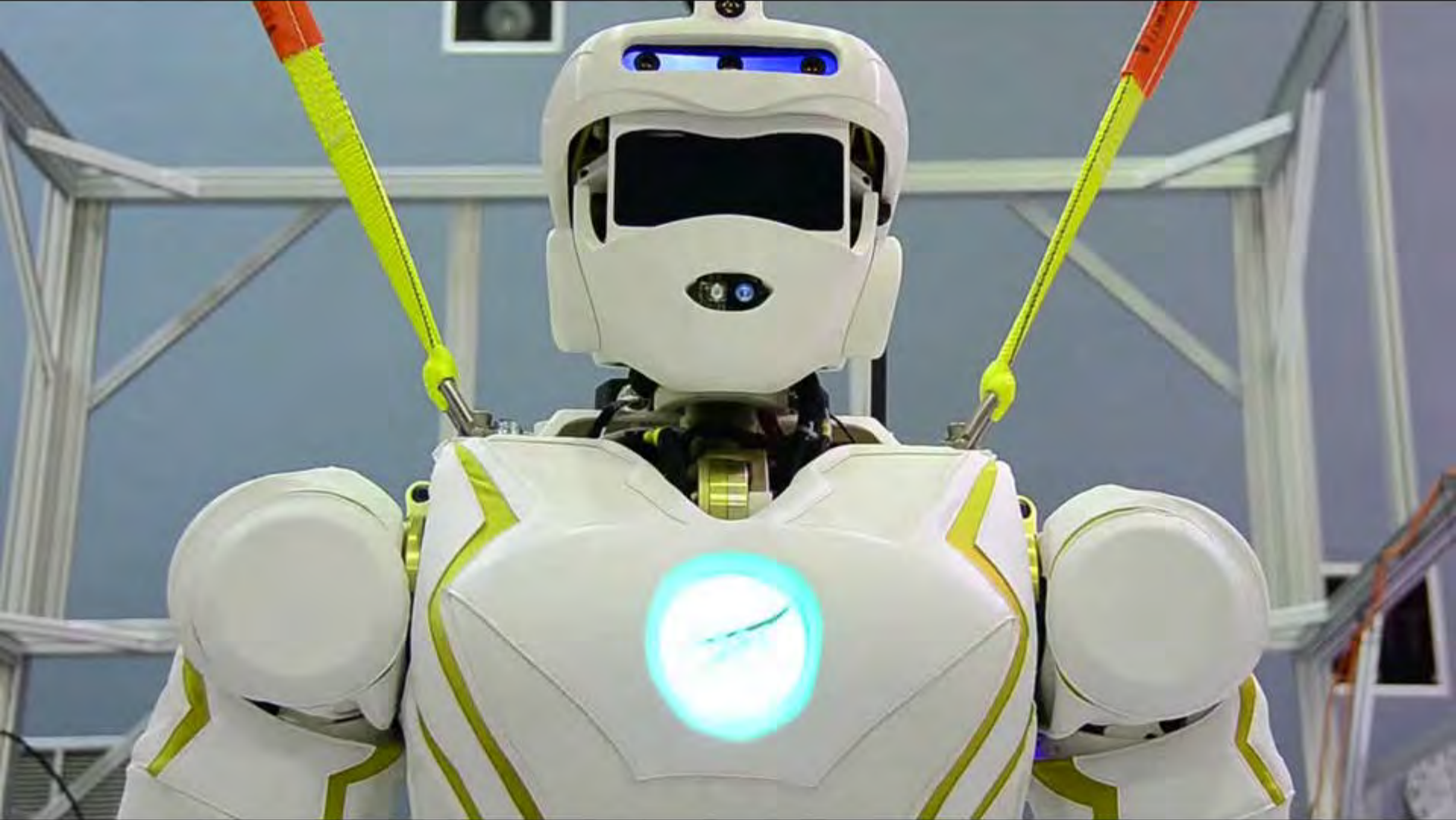
Dissipative Systems



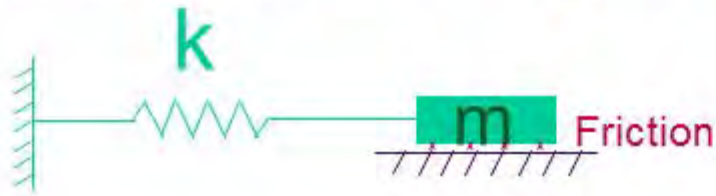
$$\frac{d}{dt} \left(\frac{\partial(K-V)}{\partial \dot{x}} \right) - \frac{\partial(K-V)}{\partial x} = f_{friction}$$

Viscous friction: $f_{friction} = -b\dot{x}$

$$m\ddot{x} + b\dot{x} + kx = 0$$

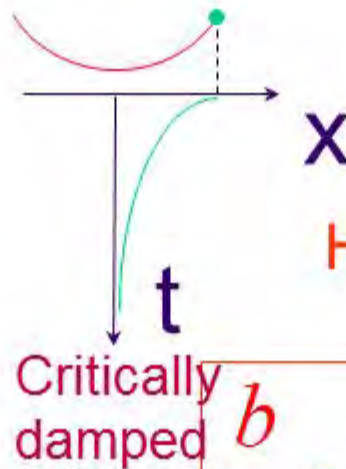
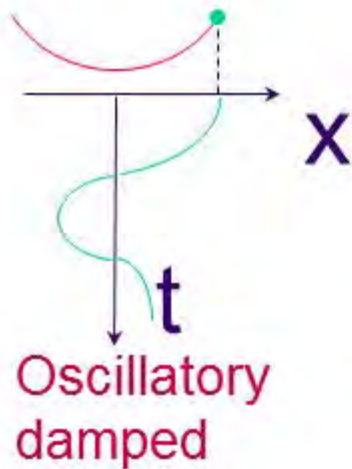


Dissipative Systems

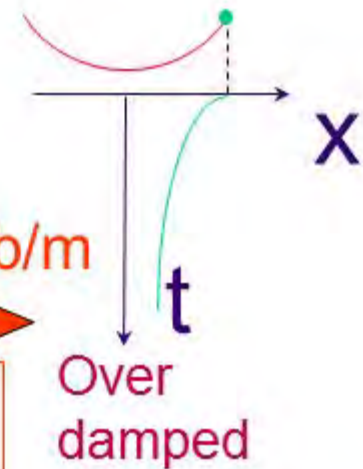


$$m\ddot{x} + b\dot{x} + kx = 0$$

$$\ddot{x} + \frac{b}{m}\dot{x} + \frac{k}{m}x = 0$$



Higher b/m



$$\frac{b}{m} = 2\omega_n$$

2^d order systems

$$m\ddot{x} + b\dot{x} + kx = 0$$

$$\ddot{x} + \frac{b}{m}\dot{x} + \frac{k}{m}x = 0$$

$$\frac{b/m}{2\omega_n}$$

$$2\omega_n$$

$$\omega_n^2$$

Natural damping ratio

Critically damped when $b/m=2\omega_n$

$$\xi_n = \frac{b}{2\omega_n m} = \frac{b}{2\sqrt{km}}$$

Critically damped system: $\xi_n = 1$ ($b = 2\sqrt{km}$)

Time Response

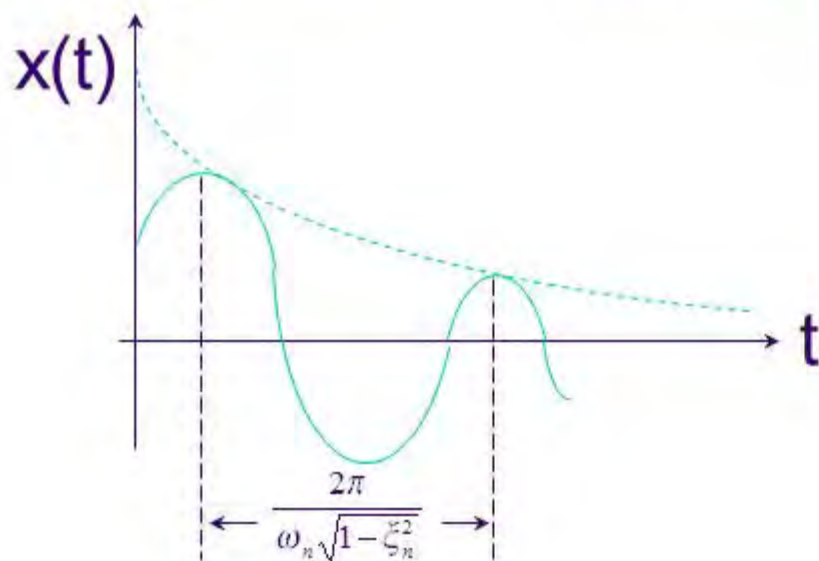
$$\ddot{x} + 2\xi_n \omega_n \dot{x} + \omega_n^2 x = 0$$

Natural
frequency

$$\omega_n = \sqrt{\frac{k}{m}} ; \xi_n = \frac{b}{2\sqrt{km}}$$

Natural
damping
ratio

$$x(t) = ce^{-\xi_n \omega_n t} \cos(\underbrace{\omega_n \sqrt{1 - \xi_n^2}}_{\omega} t + \phi)$$



ω

damped
Natural
frequency

$$\omega = \omega_n \sqrt{1 - \xi_n^2}$$

Example



$$m = 2.0$$

$$b = 4.8$$

$$k = 8.0$$

$$m\ddot{x} + b\dot{x} + kx = 0$$

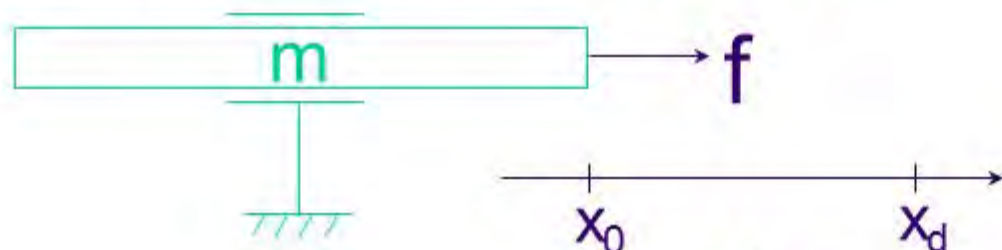
what is the “damped Natural frequency”

$$\omega = \omega_n \sqrt{1 - \xi_n^2}$$

$$\omega_n = \sqrt{\frac{k}{m}} = 2 ; \quad \xi_n = \frac{b}{2\sqrt{km}} = 0.6$$

$$\omega = 2\sqrt{1 - 0.36} = 1.6$$

1-dof Robot Control

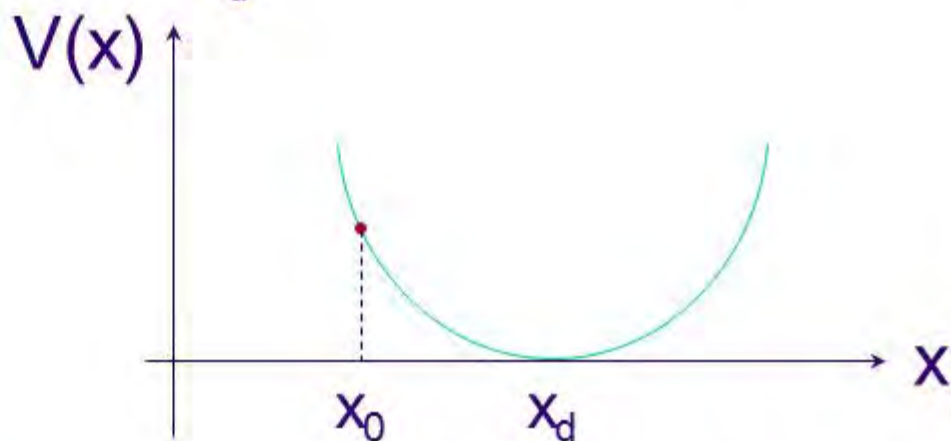


$$m\ddot{x} = f$$

Potential Field

$$V(x) > 0, x \neq x_d$$

$$V(x) = 0, x = x_d$$



$$V(x) = \frac{1}{2}k_p(x - x_d)^2 ; f = -\nabla V(x) = -\frac{\partial V}{\partial x}$$

$$m\ddot{x} = -\frac{\partial}{\partial x} \left[\frac{1}{2}k_p(x - x_d)^2 \right] ; m\ddot{x} + k_p(x - x_d) = 0$$

Position gain 

Passive Systems (Stability)

$$V_{goal} = \frac{1}{2} k_p (x - x_g)^T (x - x_g)$$

System

$$\frac{d}{dt} \left(\frac{\partial K}{\partial \dot{x}} \right) - \frac{\partial K}{\partial x} = f$$

$$\Downarrow f = - \frac{\partial V_{goal}}{\partial x}$$

$$\frac{d}{dt} \left(\frac{\partial K}{\partial \dot{x}} \right) - \frac{\partial (K - V_{goal})}{\partial x} = 0$$

Conservative Forces

Stable

Asymptotic Stability

a system $\frac{d}{dt} \left(\frac{\partial K}{\partial \dot{x}} \right) - \frac{\partial (K - V_{goal})}{\partial x} = F_s$

is asymptotically stable if

$$F_s^T \dot{x} < 0 \quad ; \quad \text{for } \dot{x} \neq 0$$



$$F_s = -k_v \dot{x} \quad \rightarrow \quad k_v > 0$$

Control

$$F = -k_p (x - x_{goal}) - k_v \dot{x}$$

Proportional-Derivative Control (PD)

$$m\ddot{x} = f = -k_p(x - x_d) - k_v\dot{x}$$

$$m\ddot{x} + k_v\dot{x} + k_p(x - x_d) = 0$$

Velocity gain

Position gain

$$1. \ddot{x} + \frac{k_v}{m}\dot{x} + \frac{k_p}{m}(x - x_d) = 0$$

$$1. \ddot{x} + 2\xi\omega\dot{x} + \omega^2(x - x_d) = 0$$

$$\xi = \frac{k_v}{2\sqrt{k_p m}}$$

closed loop
damping ratio

$$\omega = \sqrt{\frac{k_p}{m}}$$

closed loop
frequency

Gains

$$k_p = m\omega^2$$

$$k_v = m(2\xi\omega)$$

Gain Selection

$$\text{set } \begin{pmatrix} \xi \\ \omega \end{pmatrix} \rightarrow \begin{matrix} k_p = m\omega^2 \\ k_v = m(2\xi\omega) \end{matrix}$$

Unit mass system

$$k'_p = \omega^2$$

$$k'_v = 2\xi\omega$$

m - mass system

$$k_p = m k'_p$$

$$k_v = m k'_v$$

Control Partitioning

$$m\ddot{x} = f \implies m (1 \cdot \ddot{x}) = m f'$$

$$f = -k_v \dot{x} - k_p (x - x_d)$$

$$f = m \underline{[-k'_v \dot{x} - k'_p (x - x_d)]} = m f'$$

$$m\ddot{x} = m f' \quad f'$$

$$1 \cdot \ddot{x} = f' \quad \text{unit mass system}$$

$$1 \cdot \ddot{x} + k'_v \dot{x} + k'_p (x - x_d) = 0$$

$$2\xi\omega$$

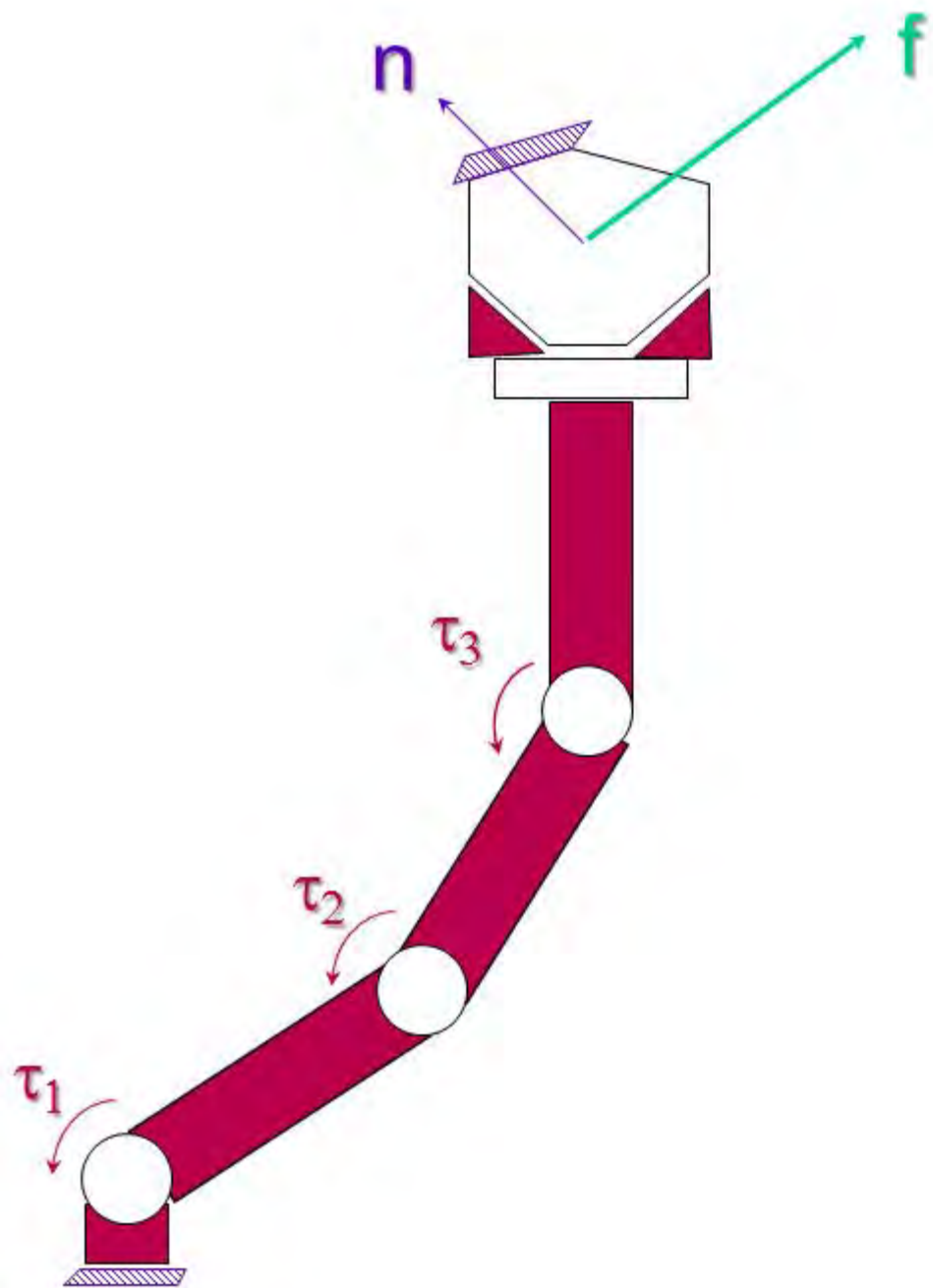
$$\omega^2$$



Robot Control

Control

- Natural Systems
- PID Control
- Joint-Space Dynamic Control
- Task-Oriented Control
- Force Control

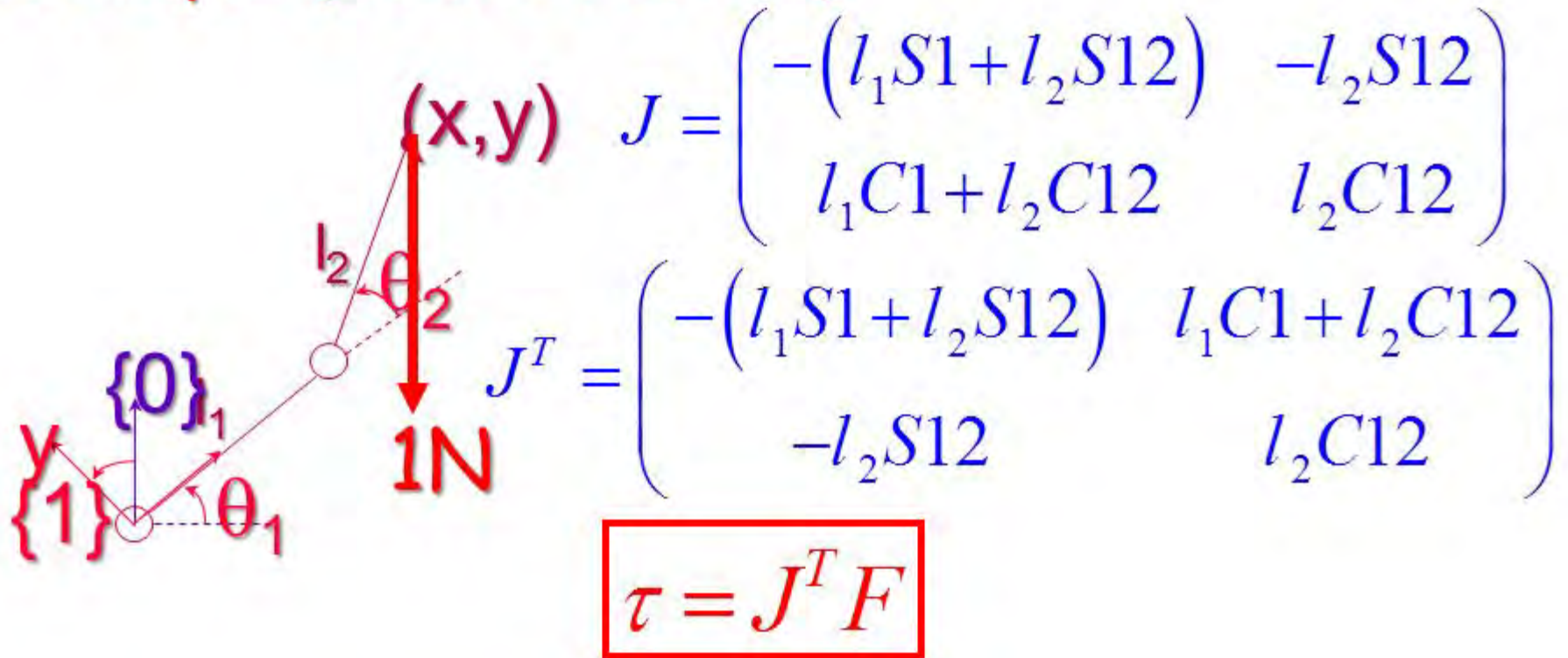


Velocity/Force Duality

$$\dot{x} = J \dot{\theta}$$

$$\tau = J^T F$$

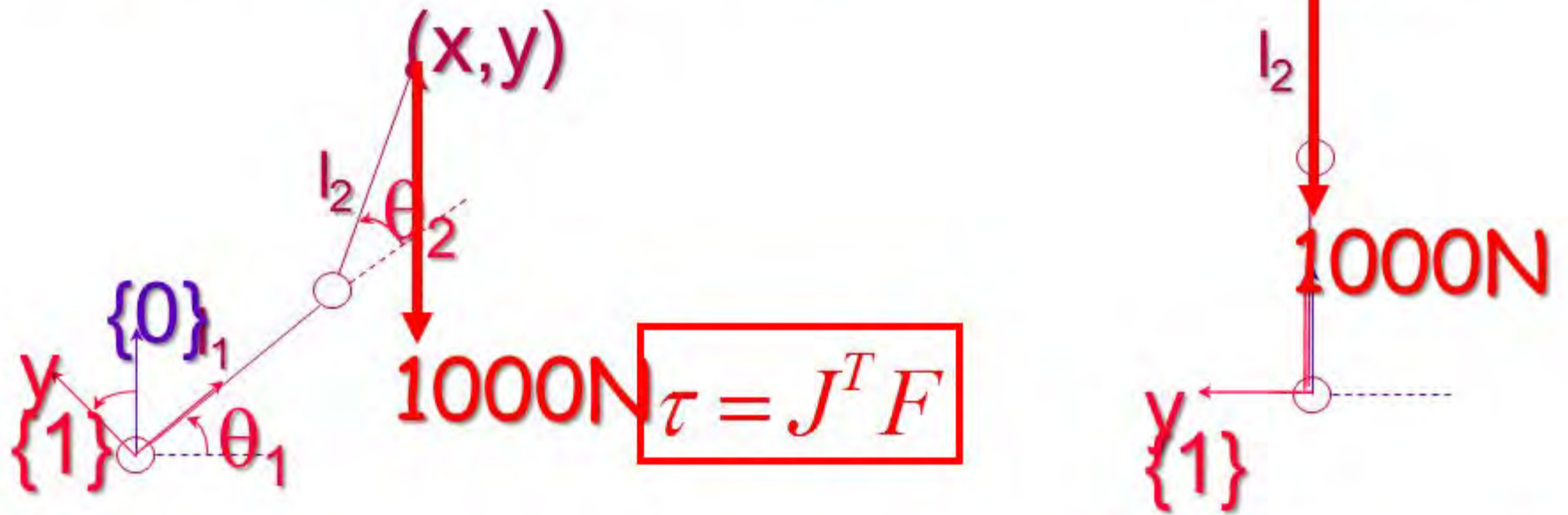
Example (Static Forces)



$$l_1 = l_2 = 1; \quad \theta_1 = 0; \quad \theta_2 = 60^\circ$$

$$\tau = \begin{pmatrix} -(l_1 S1 + l_2 S12) & l_1 C1 + l_2 C12 \\ -l_2 S12 & l_2 C12 \end{pmatrix} \begin{bmatrix} 0 \\ -1 \end{bmatrix} = - \begin{bmatrix} l_1 C1 + l_2 C12 \\ l_2 C12 \end{bmatrix} = - \begin{bmatrix} 3/2 \\ 1/2 \end{bmatrix}$$

Example (Static Forces)



$$\tau = \begin{pmatrix} -(l_1 S1 + l_2 S12) & l_1 C1 + l_2 C12 \\ -l_2 S12 & l_2 C12 \end{pmatrix} \begin{bmatrix} 0 \\ -1K \end{bmatrix} = \begin{bmatrix} l_1 C1 + l_2 C12 \\ l_2 C12 \end{bmatrix} (-1K) = \begin{bmatrix} 0 \\ 0 \end{bmatrix}$$

$$l_1 = l_2 = 1; \quad \theta_1 = 90; \quad \theta_2 = 0^\circ$$

Joint-Space Control

