

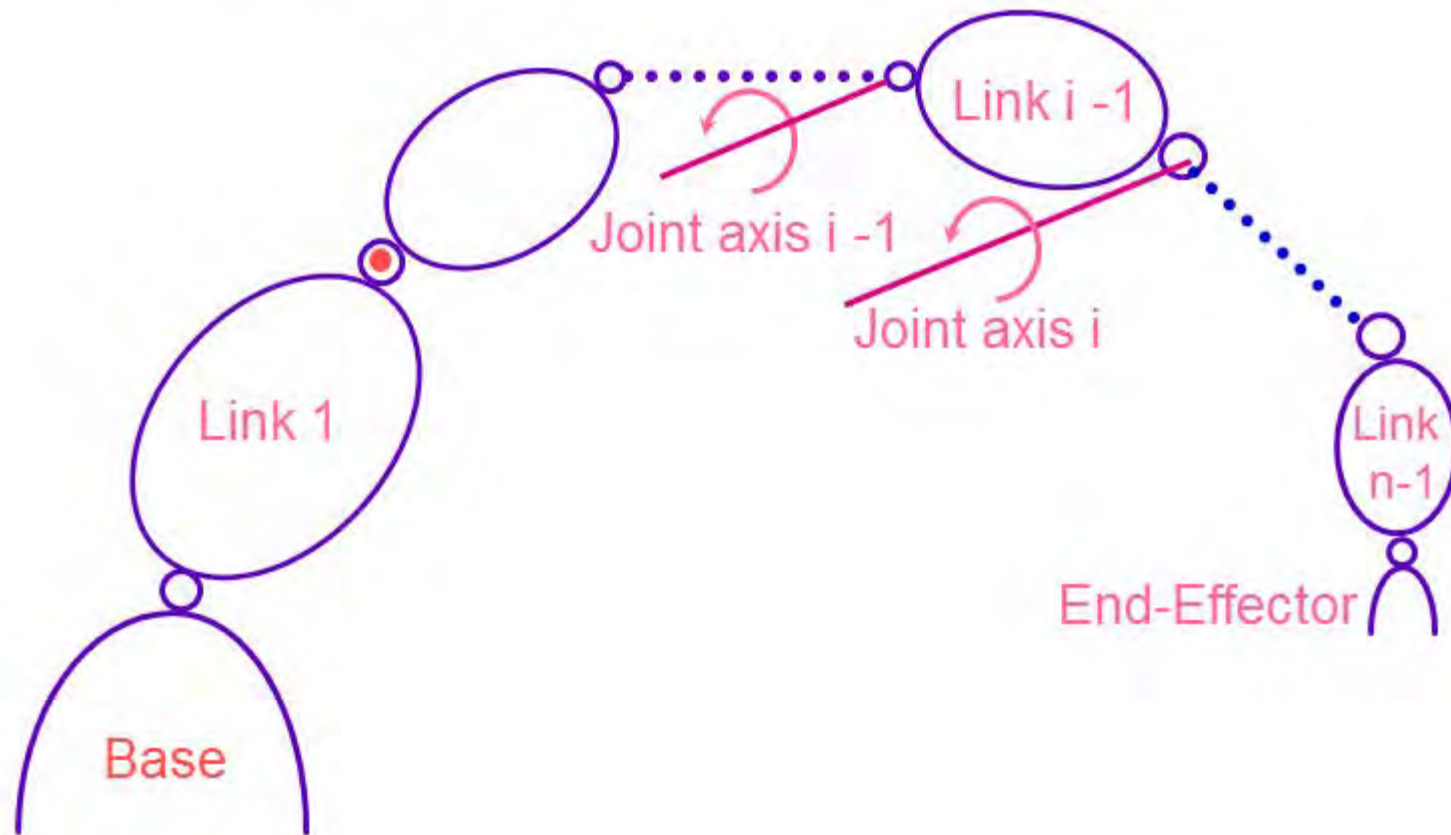
Movie Segment

HRP-4, AIST and Kwada
Industries, 2010.

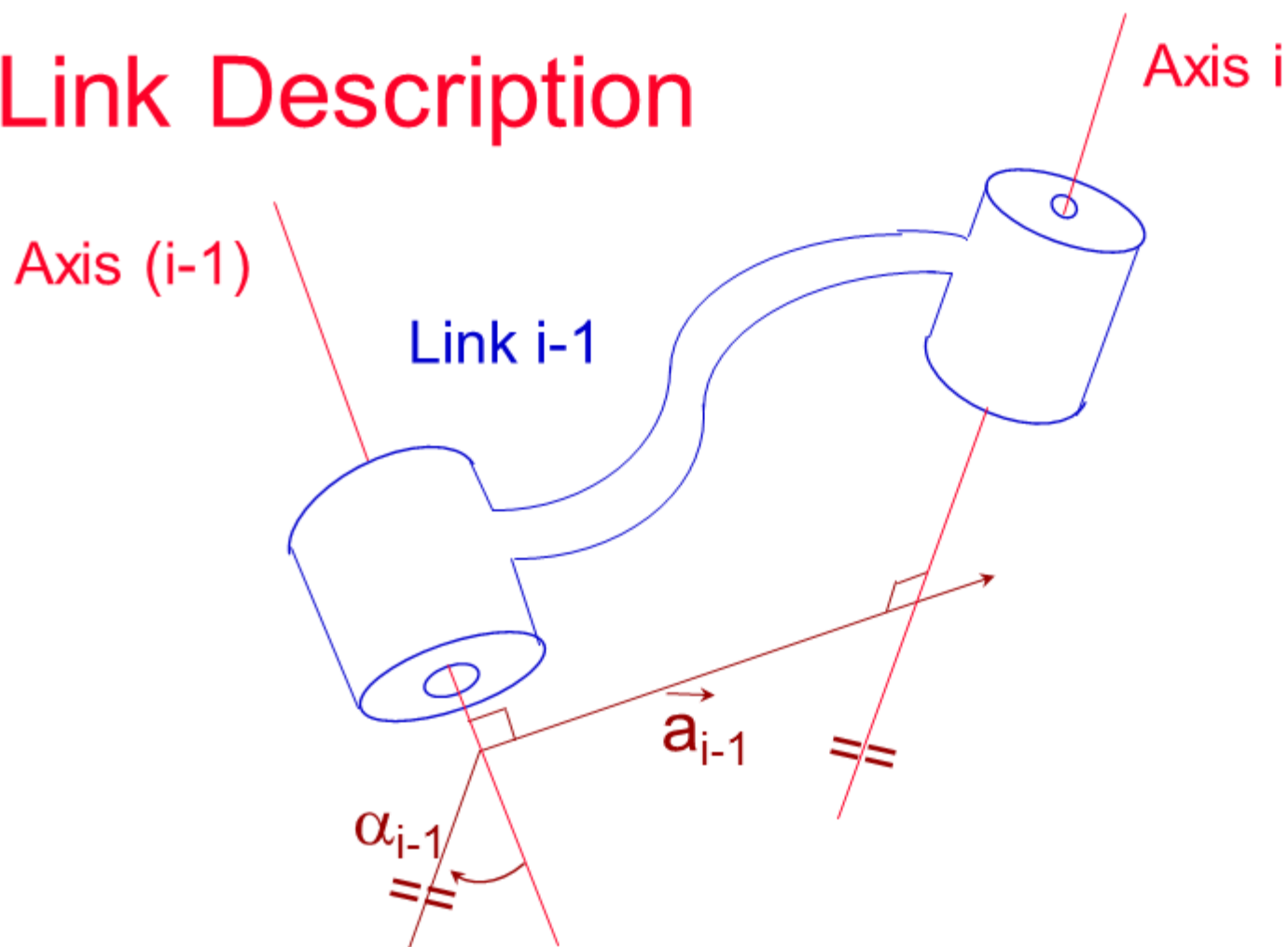
Manipulator Kinematics

- Link Description
- *Denavit-Hartenberg* Notation
- Frame Attachment
- Forward Kinematics

Manipulator



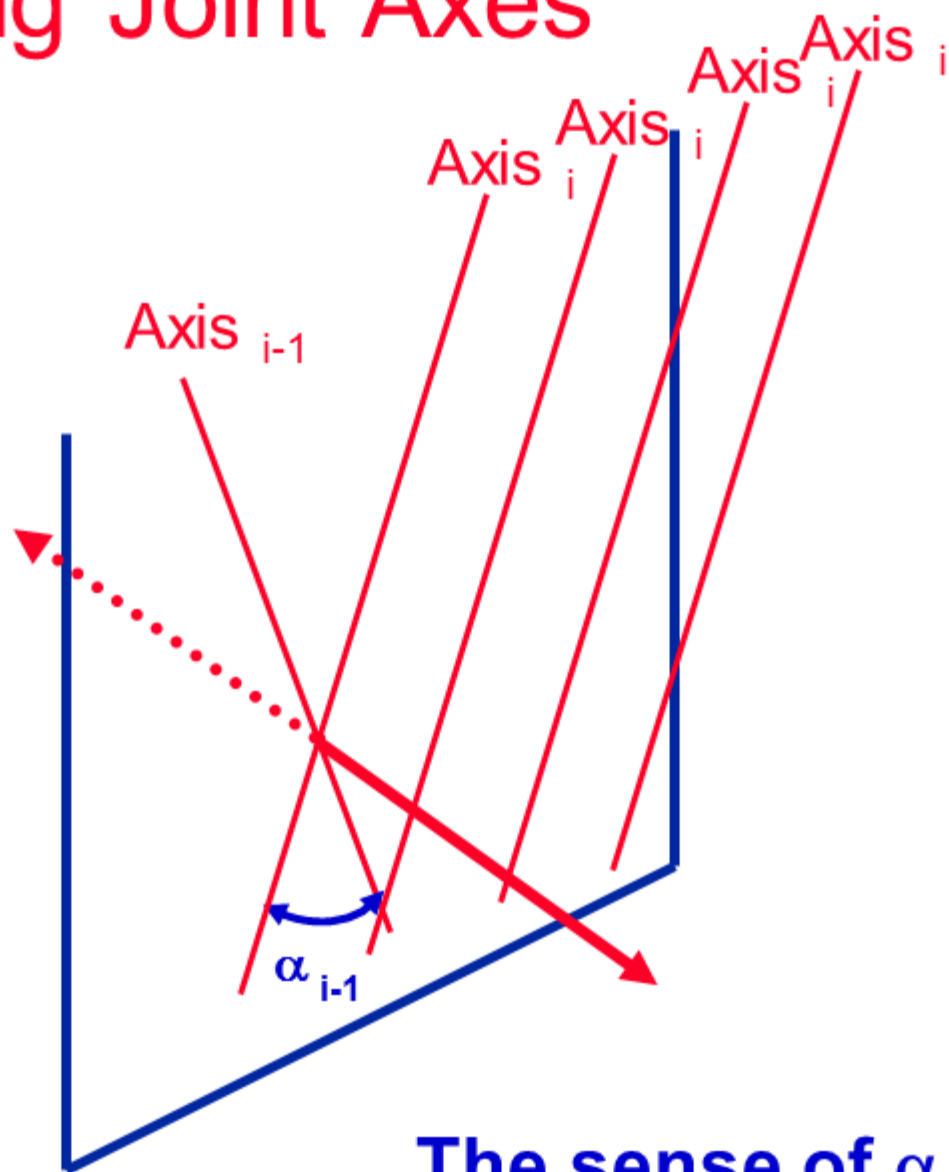
Link Description



— : Link Length - mutual perpendicular
unique except for parallel axis

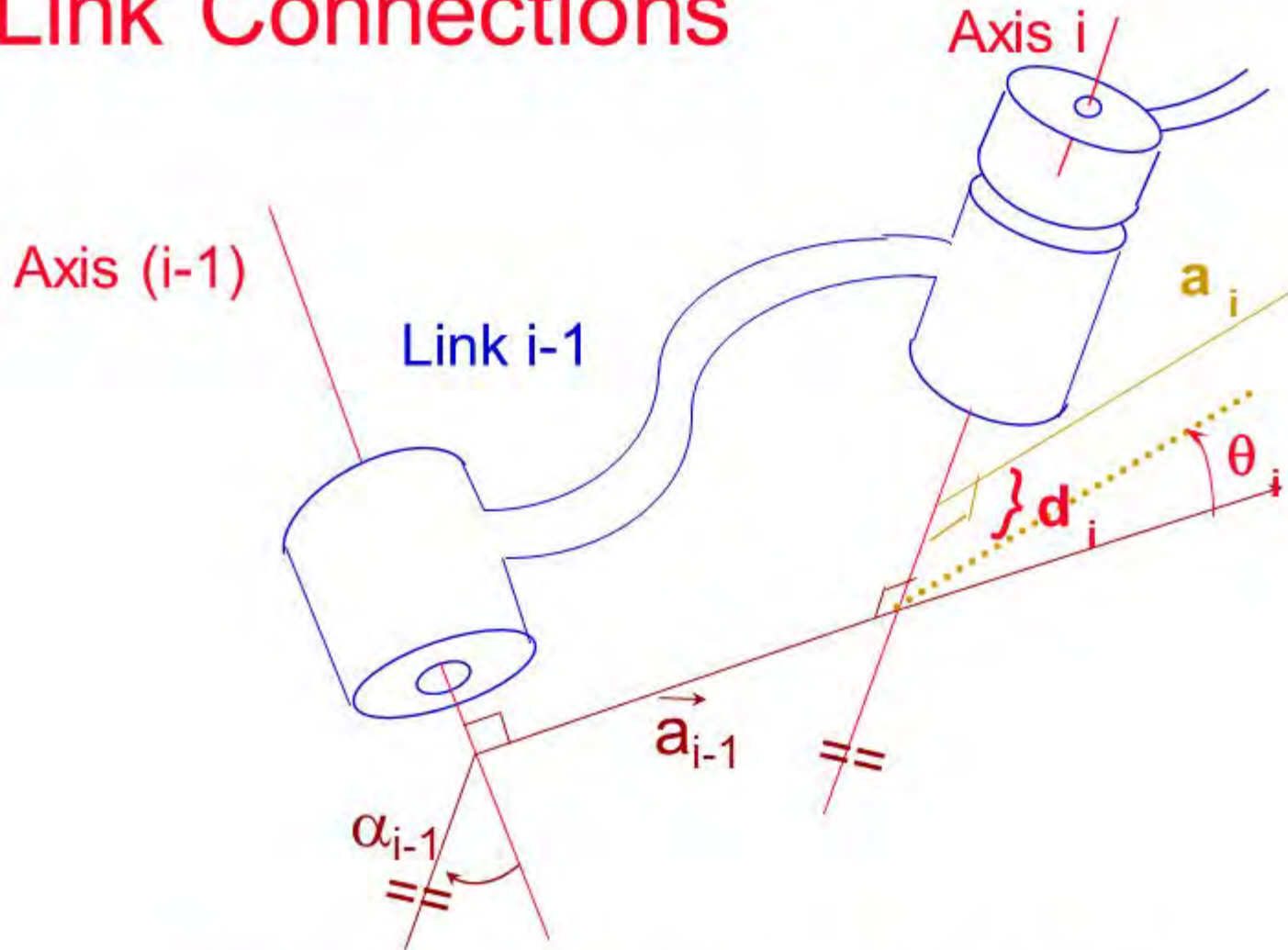
— : Link Twist - measured in the right-hand sense about \vec{a}_{i-1}

Intersecting Joint Axes

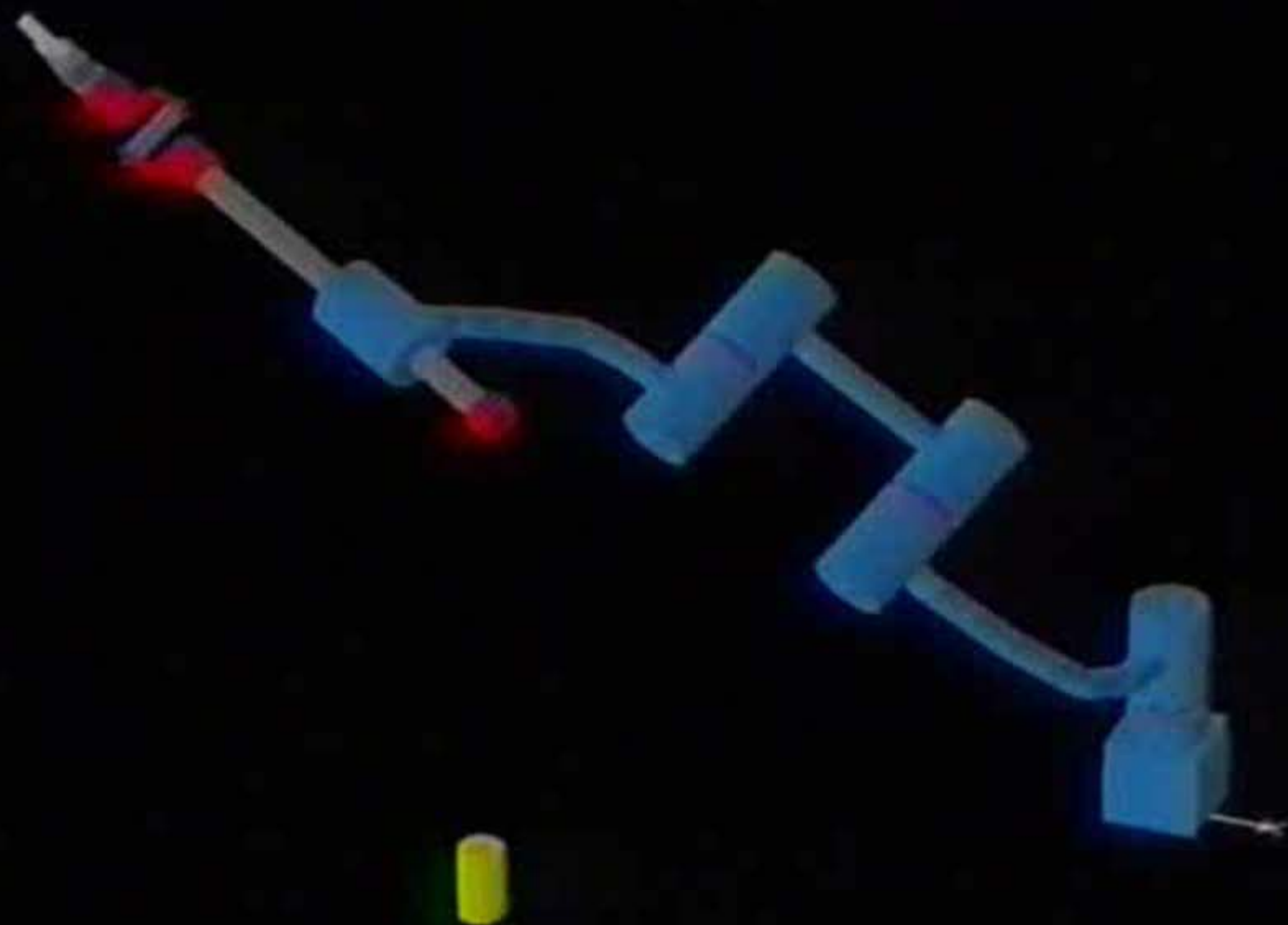


The sense of α_{i-1} is free

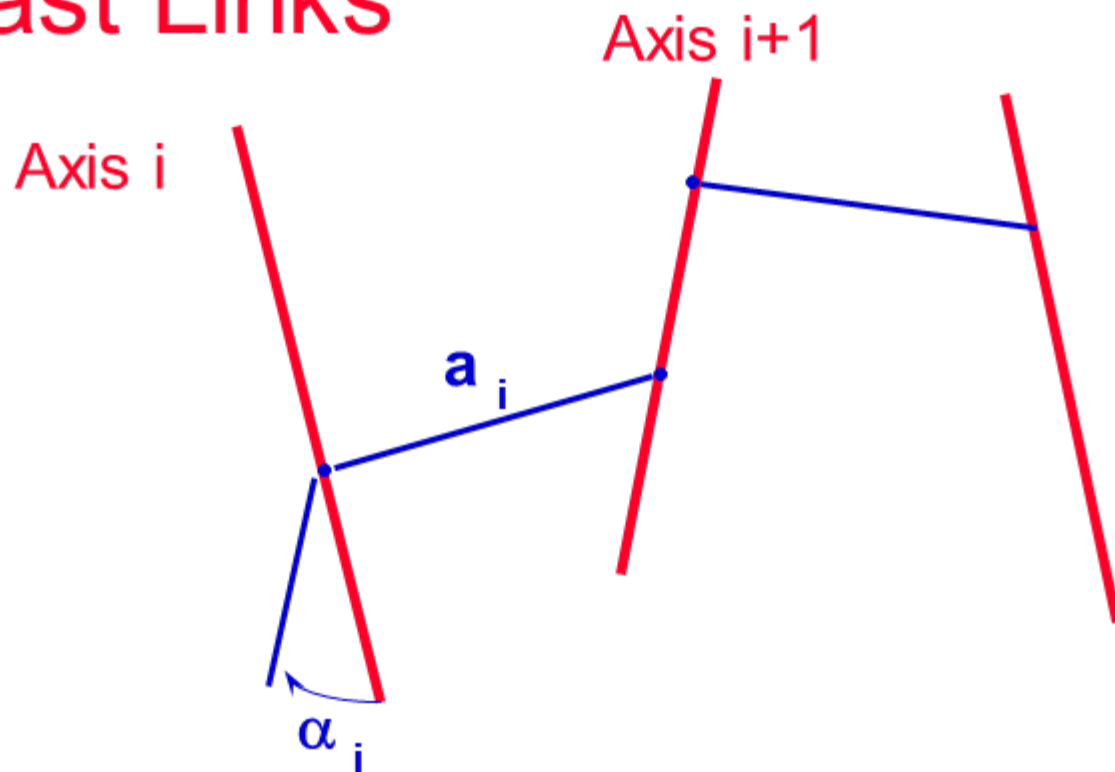
Link Connections



- : Link Offset -- variable if joint i is _____
- : Joint Angle -- variable if joint i is _____



First & Last Links



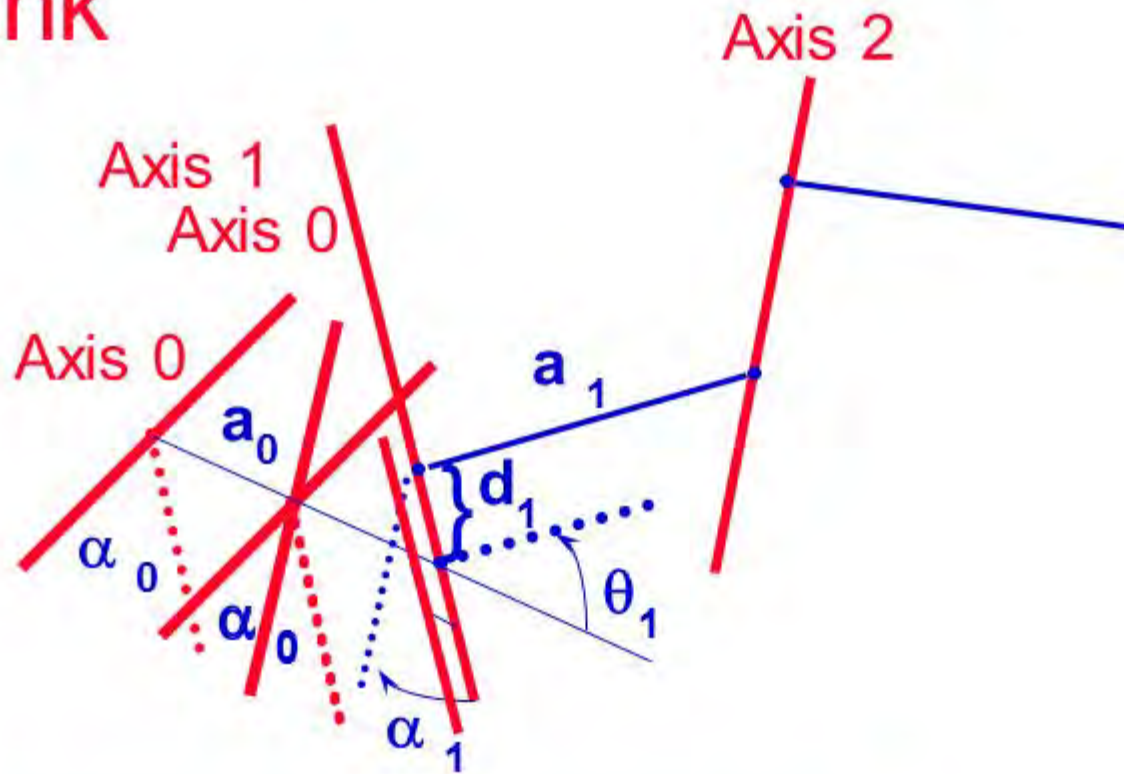
and depend on joint axes i and $i+1$

Axes 1 to n : determined

➔ $a_1, a_2 \dots a_{n-1}$ and $\alpha_1, \alpha_2 \dots \alpha_{n-1}$

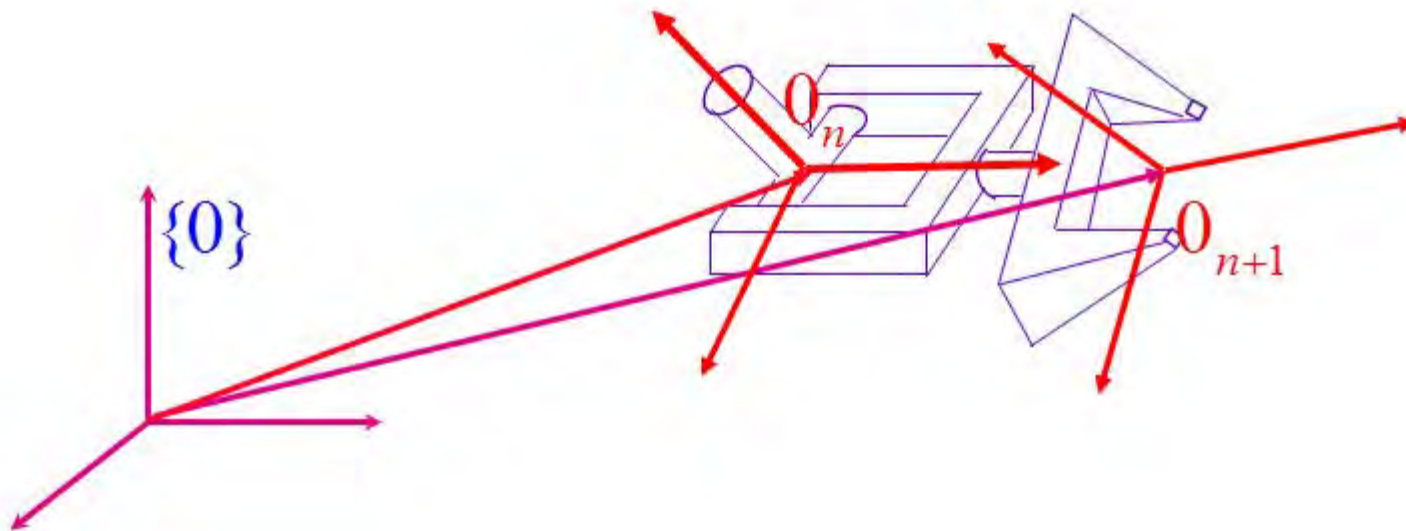
Convention: $a_0 = a_n = \underline{\quad}$ and $\alpha_0 = \alpha_n = \underline{\quad}$

First Link

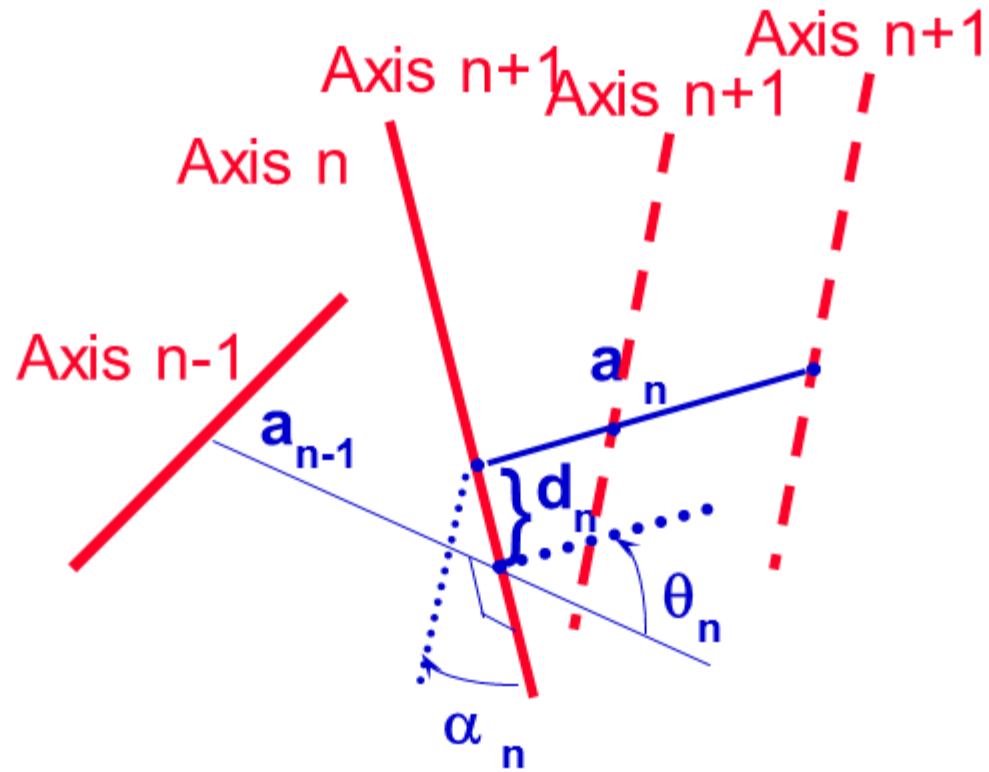


$a_0 = \underline{\quad}$ and $\alpha_0 = \underline{\quad}$

End-Effector Frame

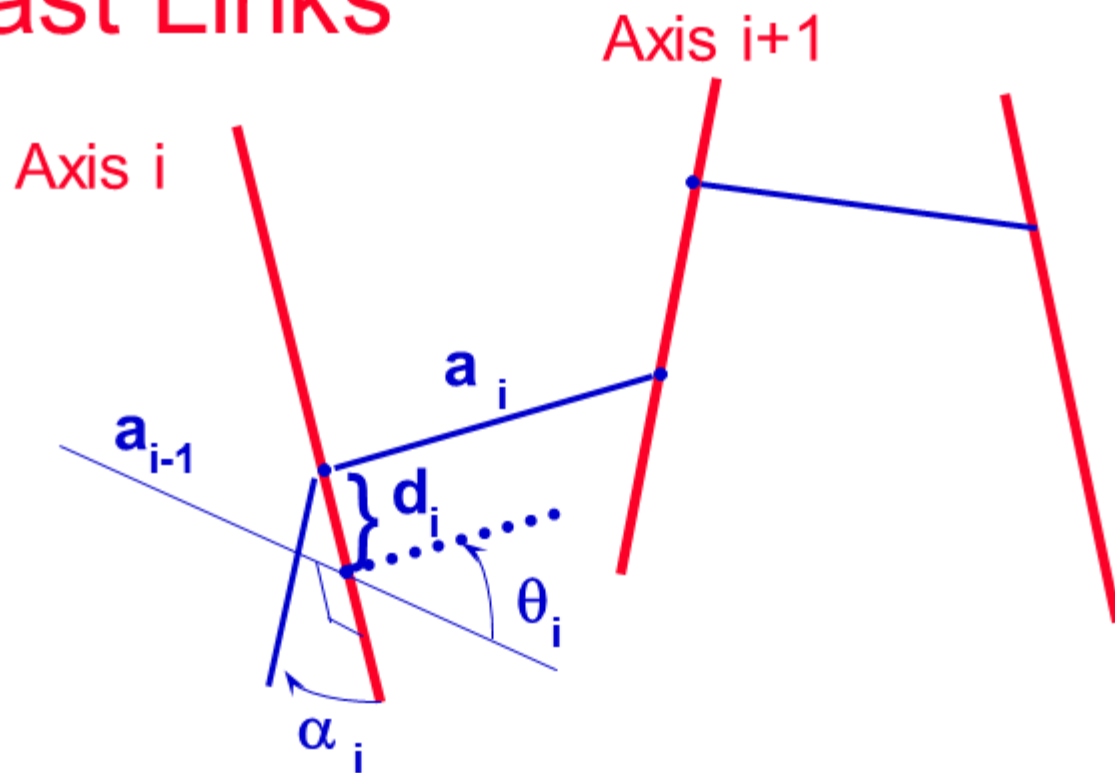


Last Link



$$a_n = \underline{\quad} \text{ and } \alpha_n = \underline{\quad}$$

First & Last Links



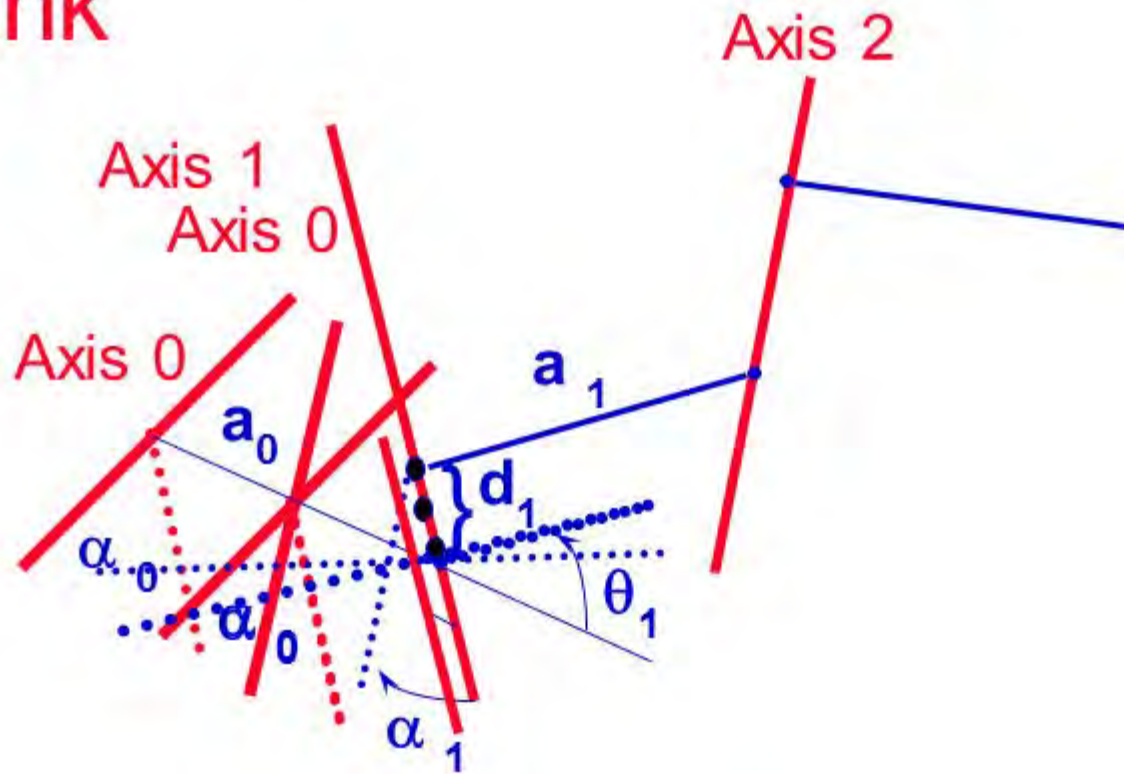
θ_i and d_i depend on links $i-1$ and i

→ $\theta_2, \theta_3, \dots, \theta_{n-1}$ and d_2, d_3, \dots, d_{n-1}

Convention: set the constant parameters to zero

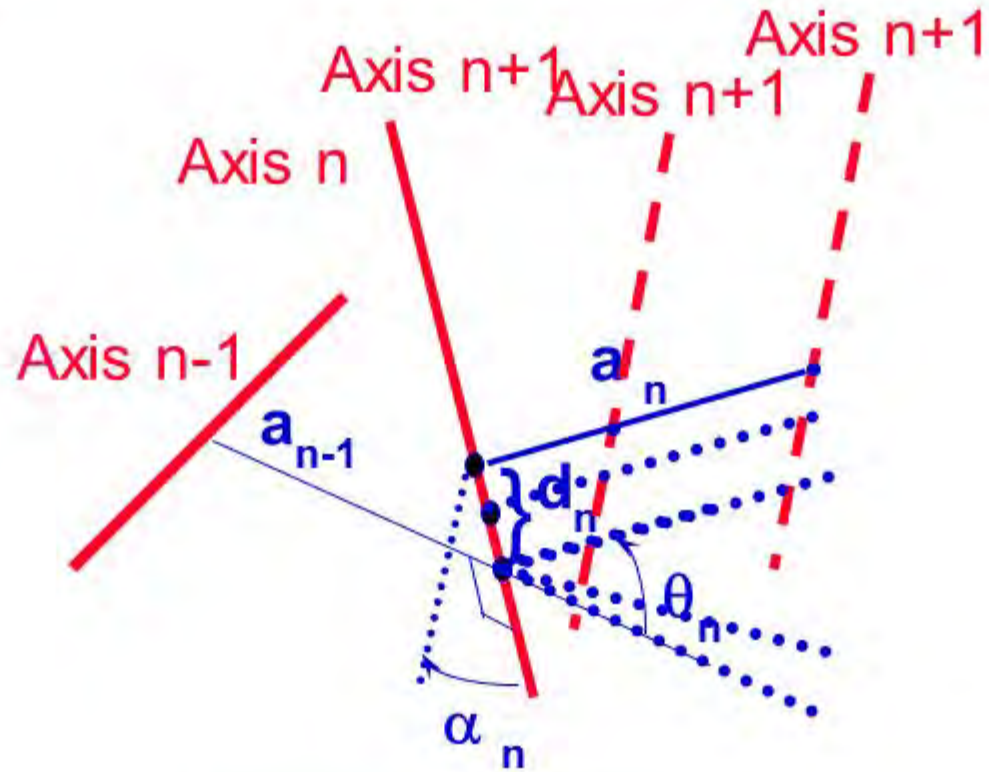
Following joint type: d_1 or $\theta_1 = 0$ and d_n or $\theta_n = 0$

First Link



d_1 or $\theta_1 = \underline{\quad}$

Last Link



$$d_n \text{ or } \theta_n = \underline{\quad}$$

Denavit-Hartenberg Parameters

4 D-H parameters (α_i , a_i , d_i , θ_i)

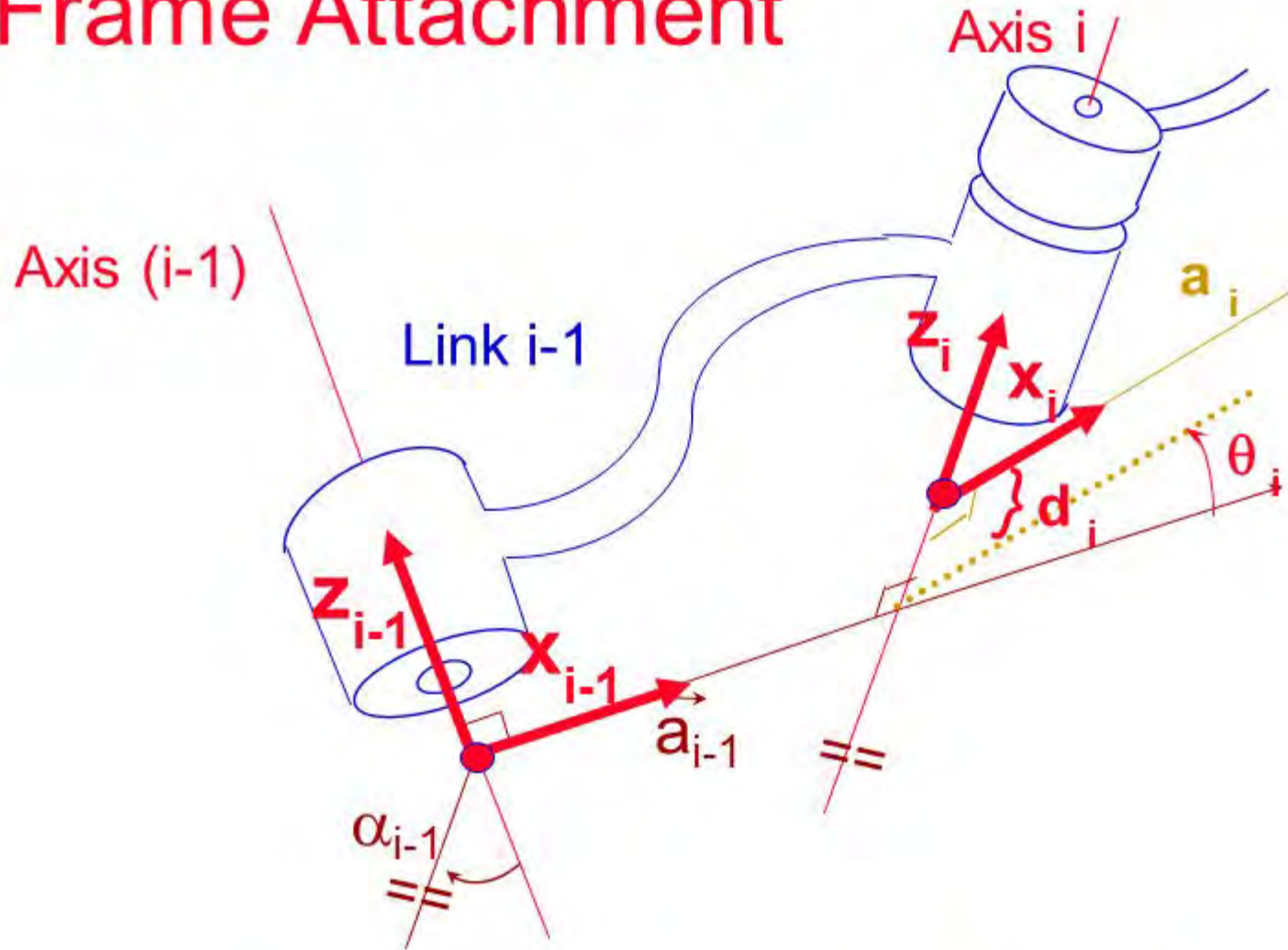
3 fixed link parameters

1 joint variable $\left\{ \begin{array}{l} \theta_i \text{ revolute joint} \\ d_i \text{ prismatic joint} \end{array} \right.$

α_i and a_i : describe the Link i

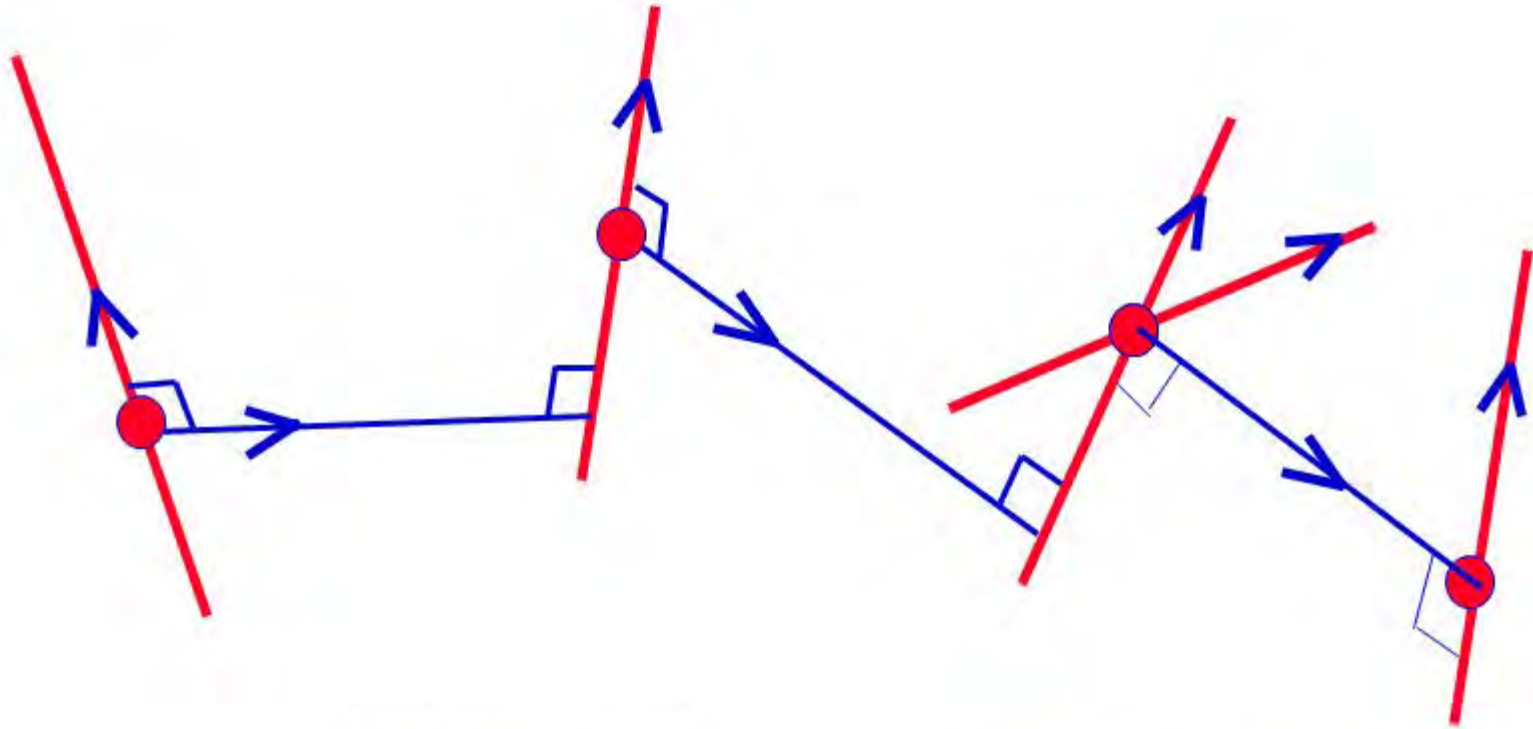
d_i and θ_i : describe the Link's connection

Frame Attachment



y-vectors: complete right-hand frames

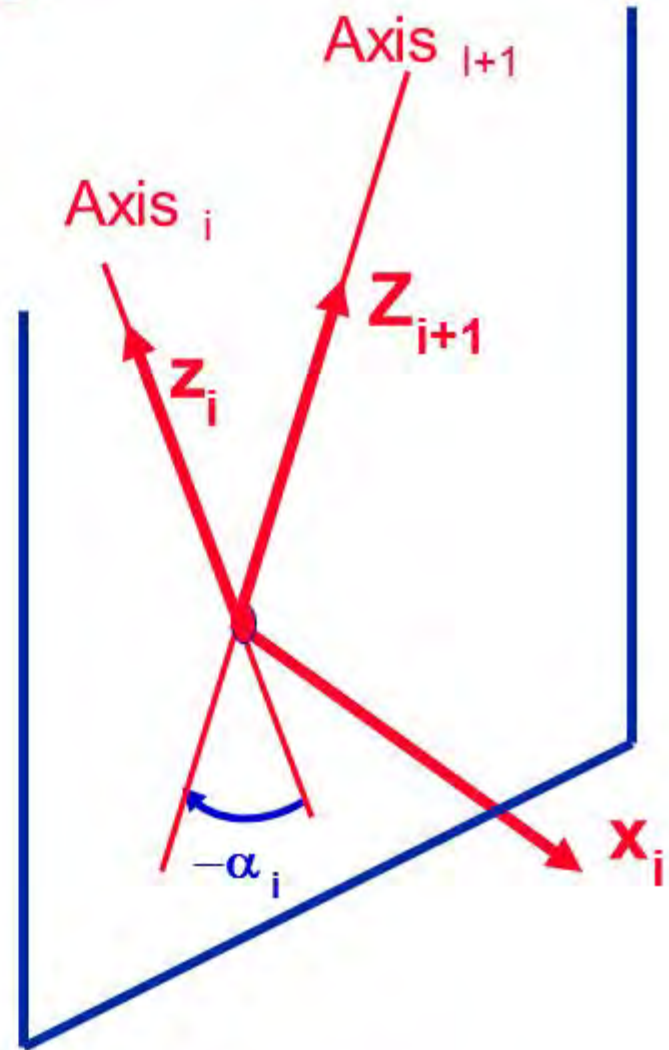
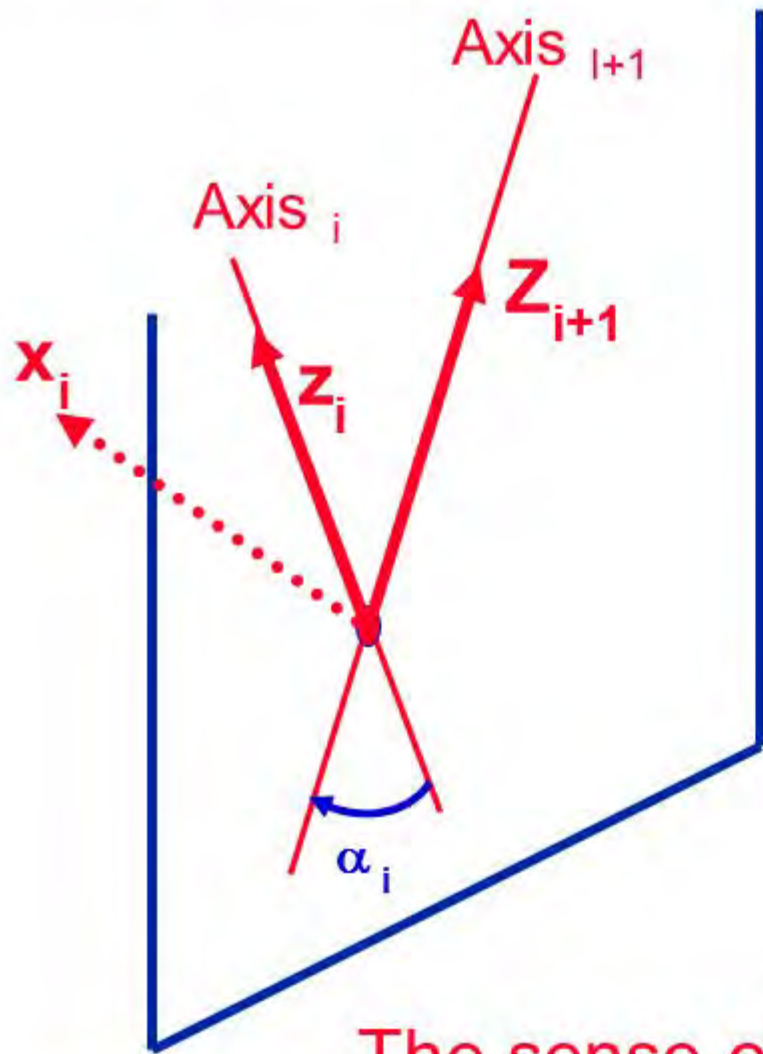
Summary – Frame Attachment



1. Normals
2. Origins

3. Z-axes
4. X-axes

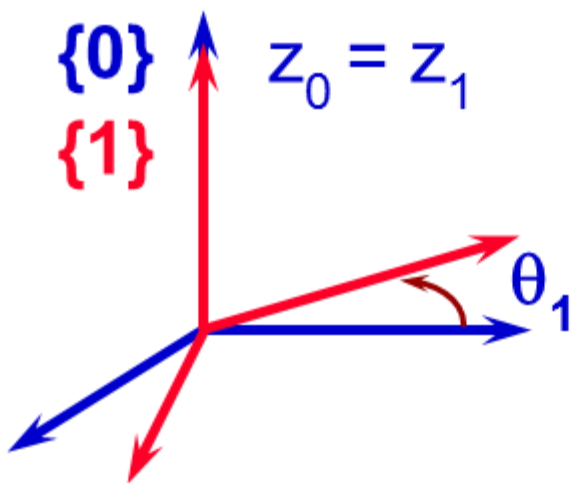
Intersecting Joint Axes



The sense of α_i is determined by the direction of x

First Link

Revolute



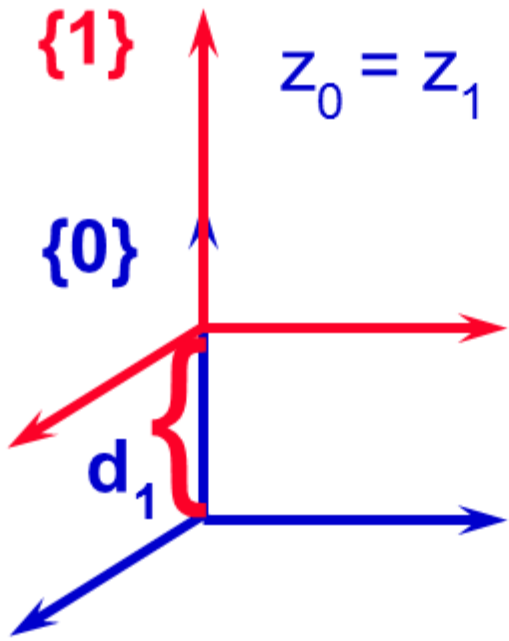
$$a_0 = 0$$

$$\alpha_0 = 0$$

$$d_1 = 0$$

$$\theta_1 = \text{---} \longrightarrow \{0\} \equiv \{1\}$$

Prismatic



$$a_0 = 0$$

$$\alpha_0 = 0$$

$$\theta_1 = 0$$

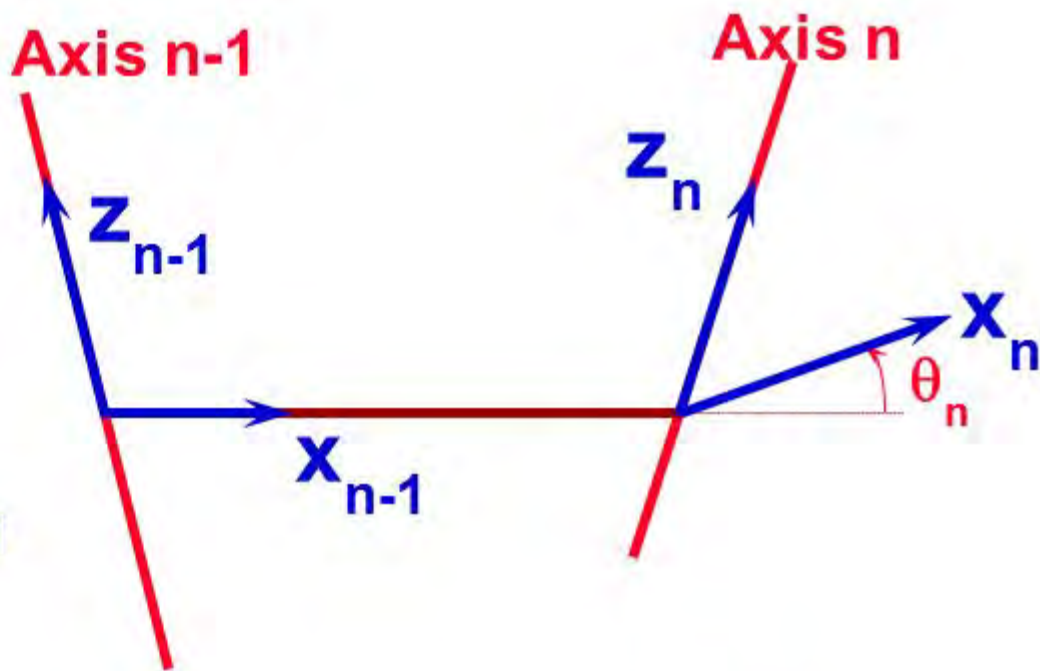
$$d_1 = \text{---} \longrightarrow \{0\} \equiv \{1\}$$

Last Link

Revolute

$$d_n = 0$$

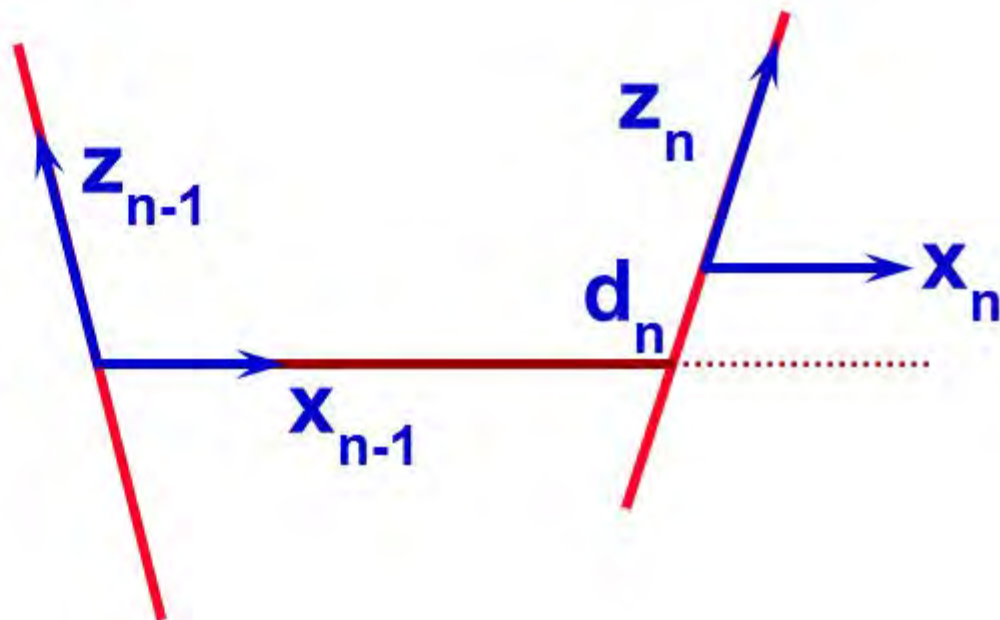
$$\theta_n = 0 \rightarrow x_n = x_{n-1}$$



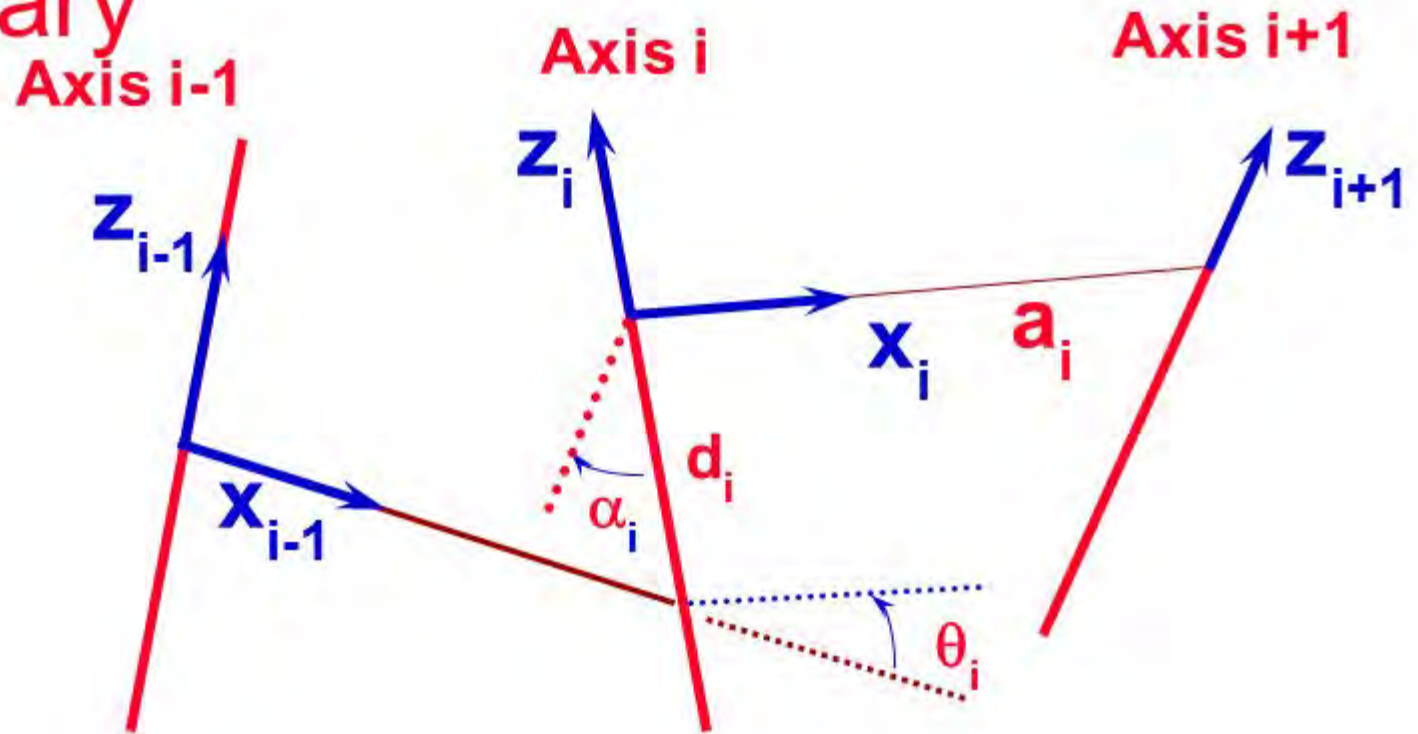
Prismatic

$$\theta_n = 0$$

$$d_n = 0 \rightarrow x_n = x_{n-1}$$



Summary



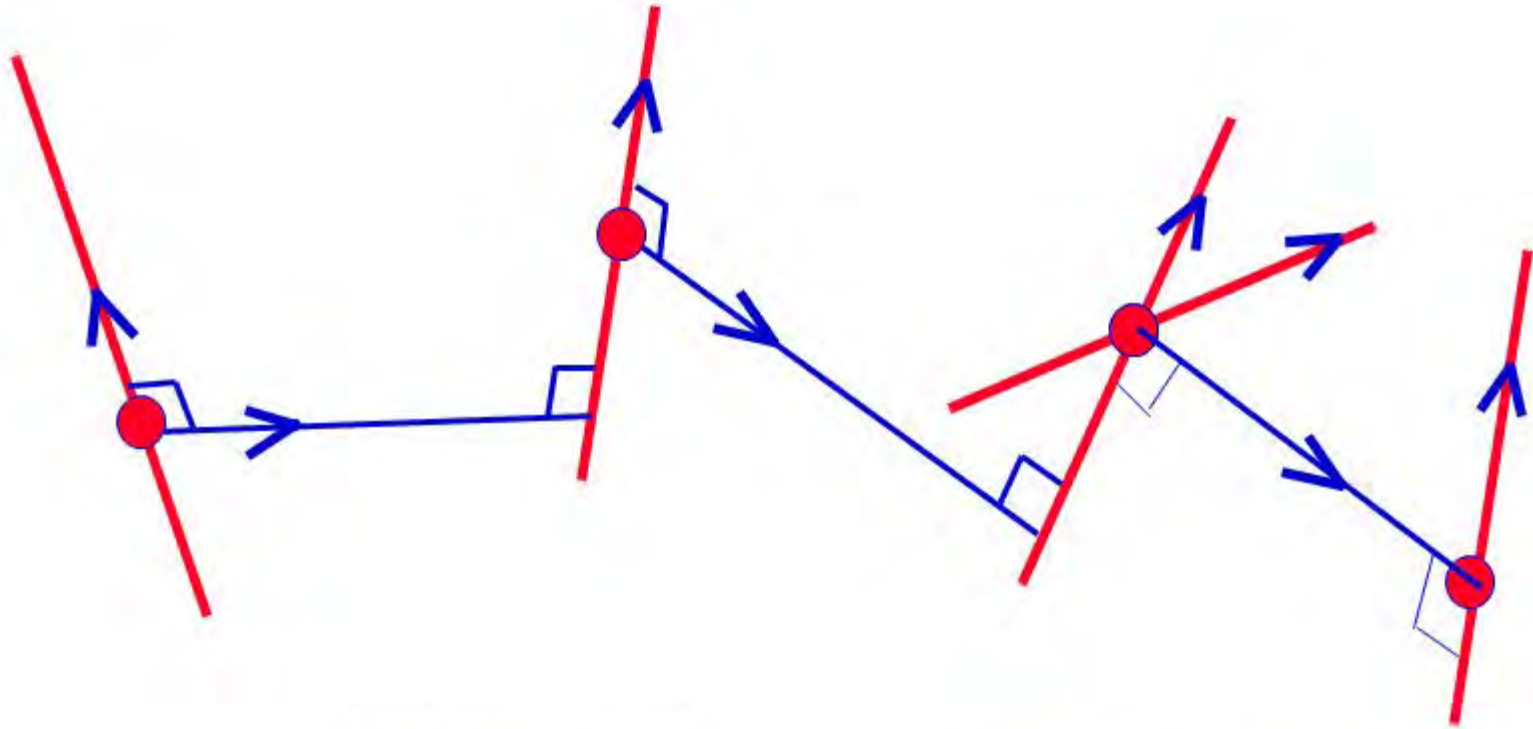
a_i : distance (z_i, z_{i+1}) along x_i

α_i : angle (z_i, z_{i+1}) about x_i

d_i : distance (x_{i-1}, x_i) along z_i

θ_i : angle (x_{i-1}, x_i) about z_i

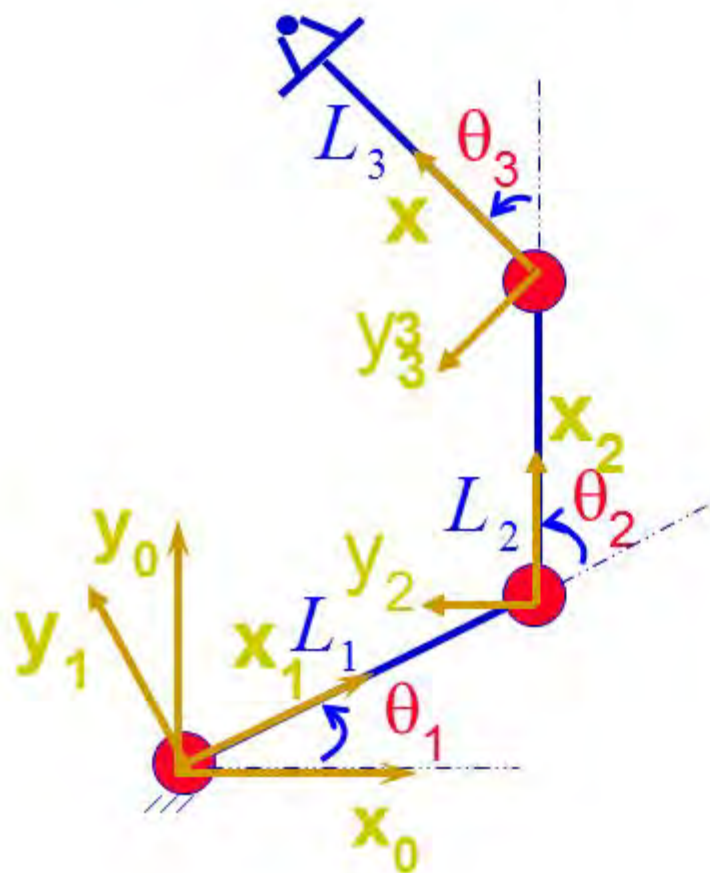
Summary – Frame Attachment



1. Normals
2. Origins

3. Z-axes
4. X-axes

Example – RRR Arm



i	α_{i-1}	a_{i-1}	d_i	θ_i
1	—	—	—	—
2	—	—	—	—
3	—	—	—	—

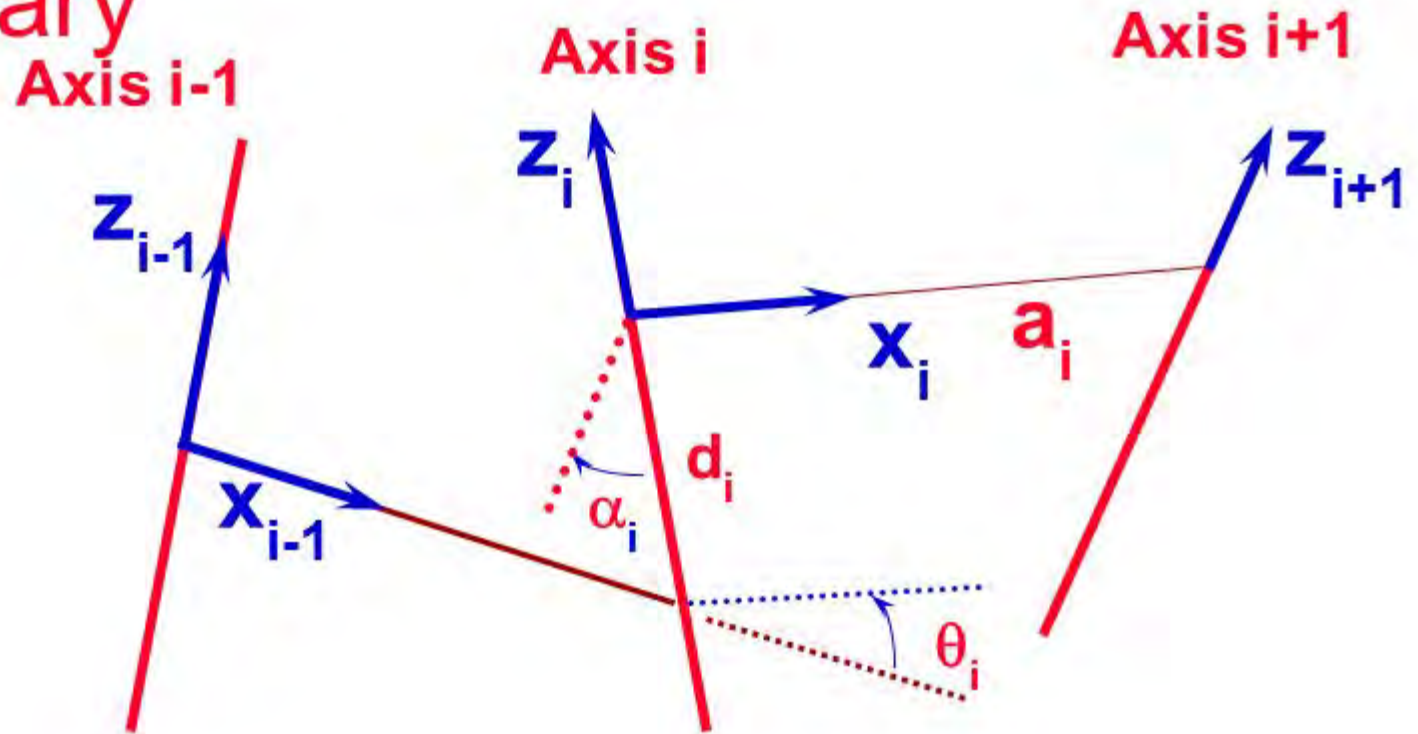
Movie Segment

BigDog, Boston Dynamics, 2010



Boston Dynamics

Summary



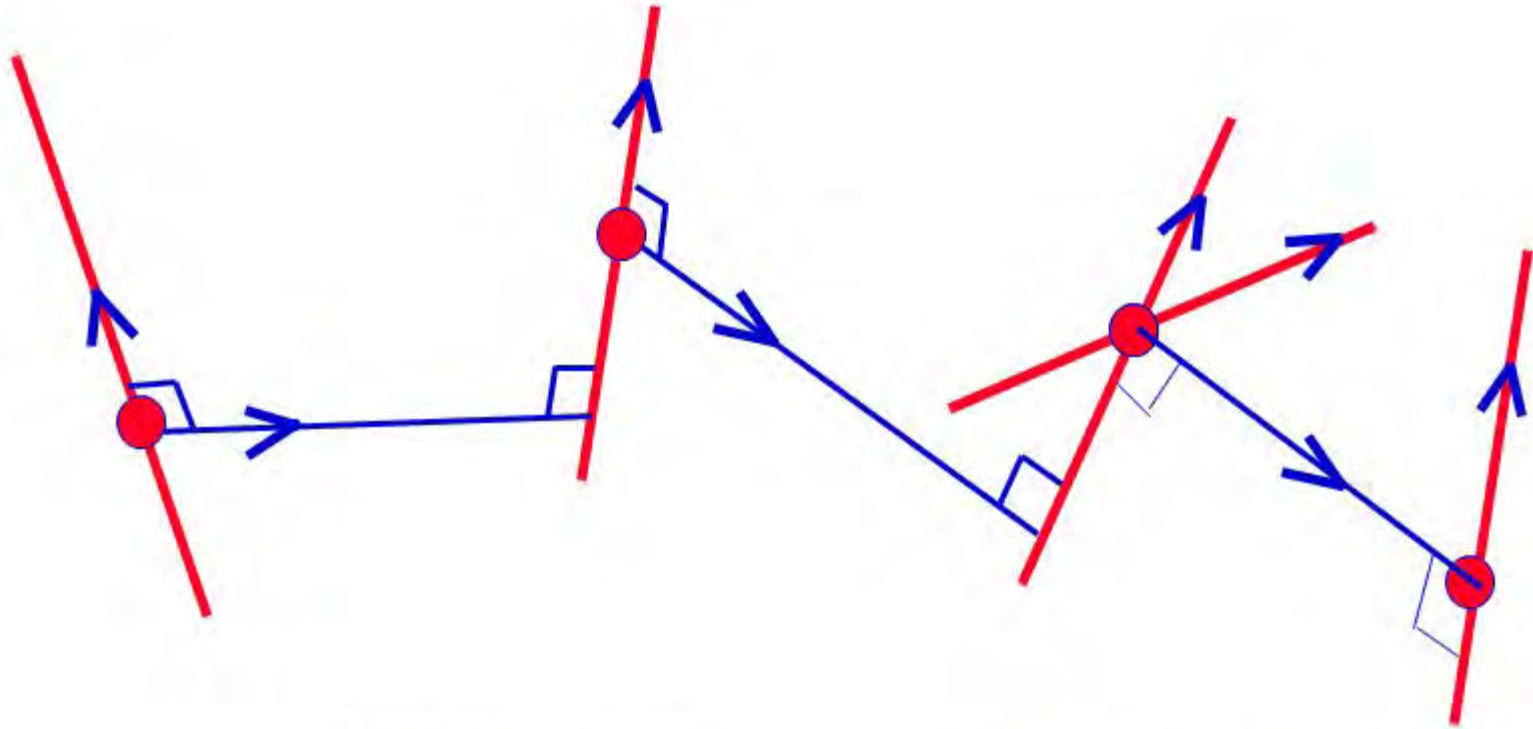
a_i : distance (z_i, z_{i+1}) along x_i

α_i : angle (z_i, z_{i+1}) about x_i

d_i : distance (x_{i-1}, x_i) along z_i

θ_i : angle (x_{i-1}, x_i) about z_i

Summary – Frame Attachment



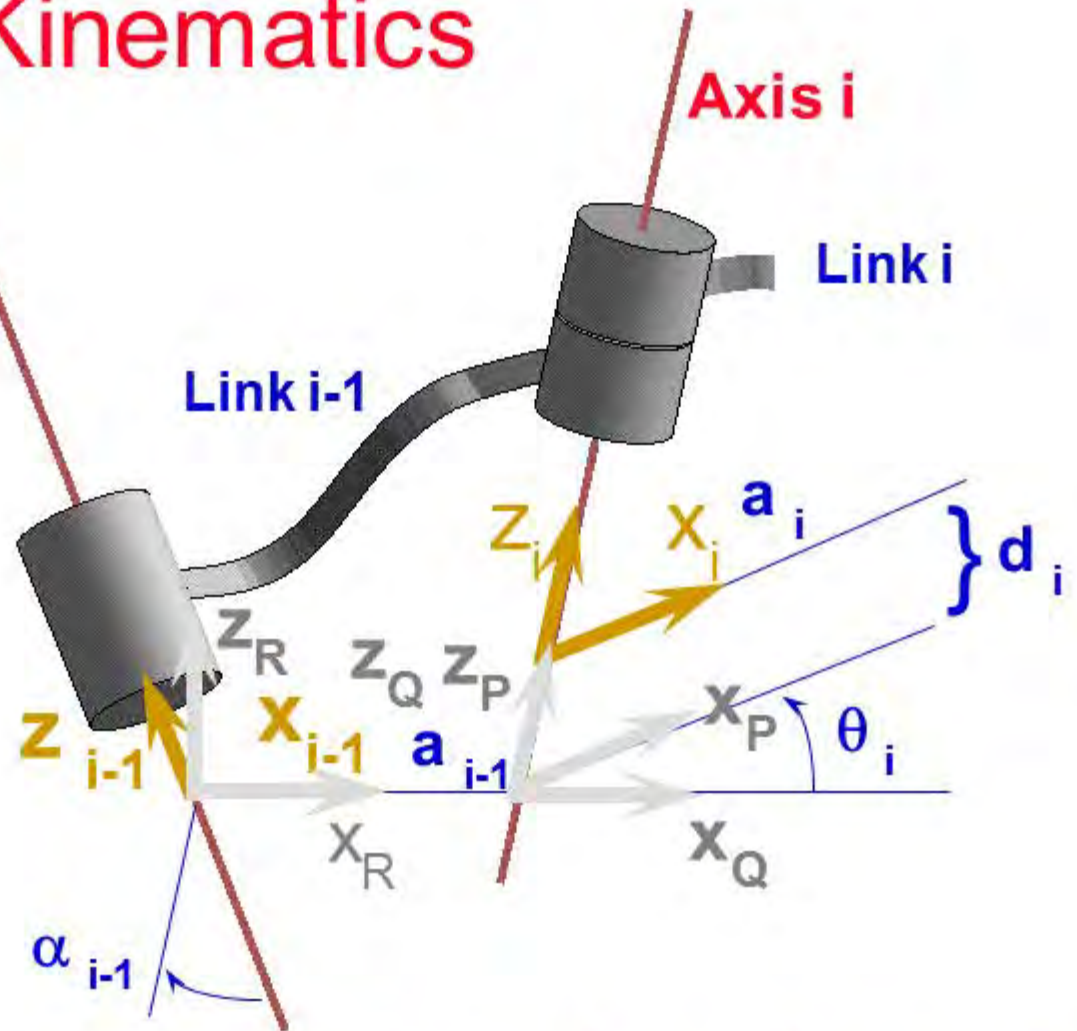
1. Normals
2. Origins

3. Z-axes
4. X-axes

Forward Kinematics

Axis (i-1)

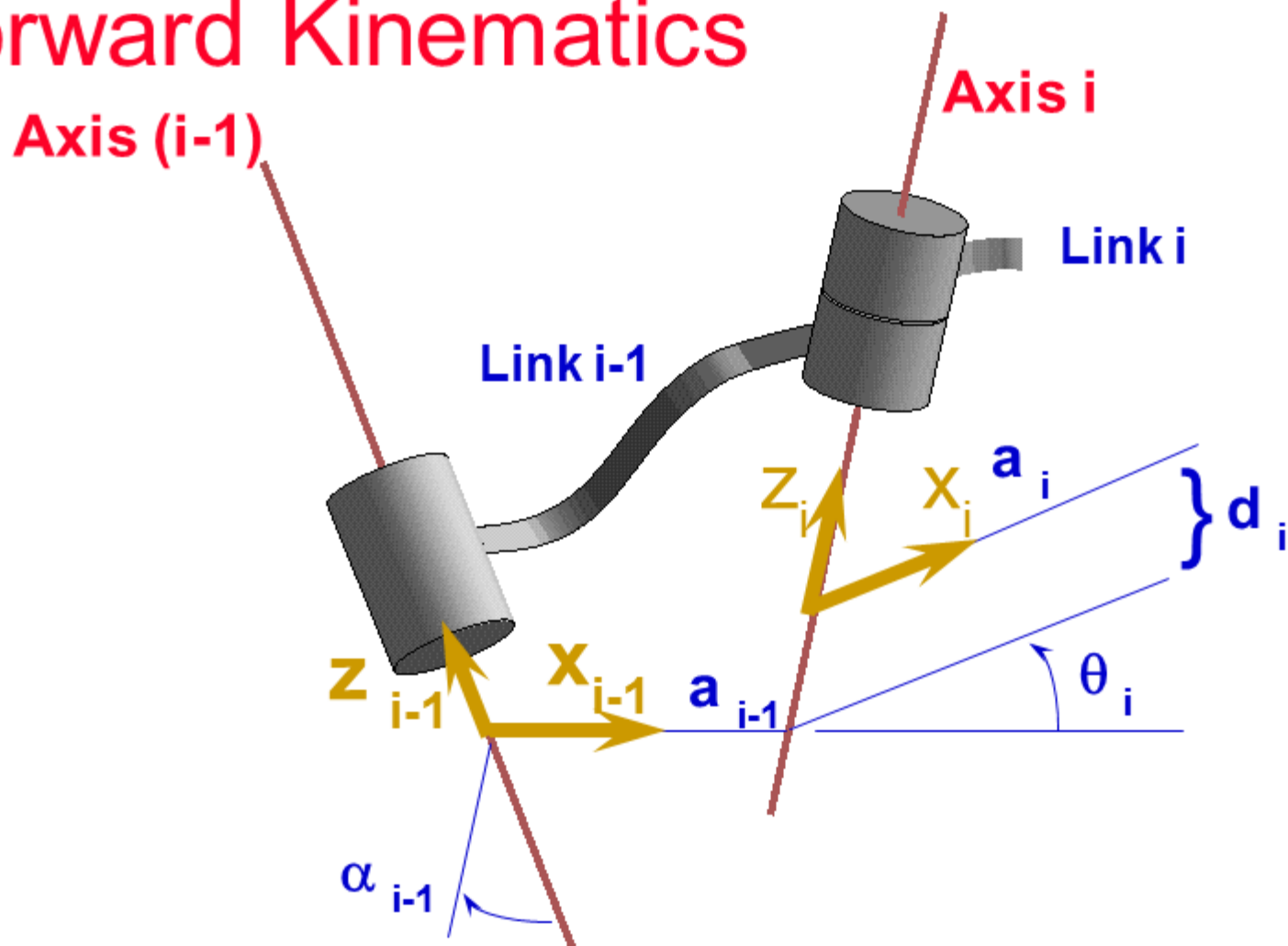
Axis i



$${}^{i-1}_i T = {}^{i-1}_R T \quad {}^R_Q T \quad {}^Q_P T \quad {}^P_i T$$

$${}^{i-1}_i T_{(\alpha_{i-1}, a_{i-1}, \theta_i, d_i)} = R_x(\alpha_{i-1}) D_x(a_{i-1}) R_z(\theta_i) D_z(d_i)$$

Forward Kinematics

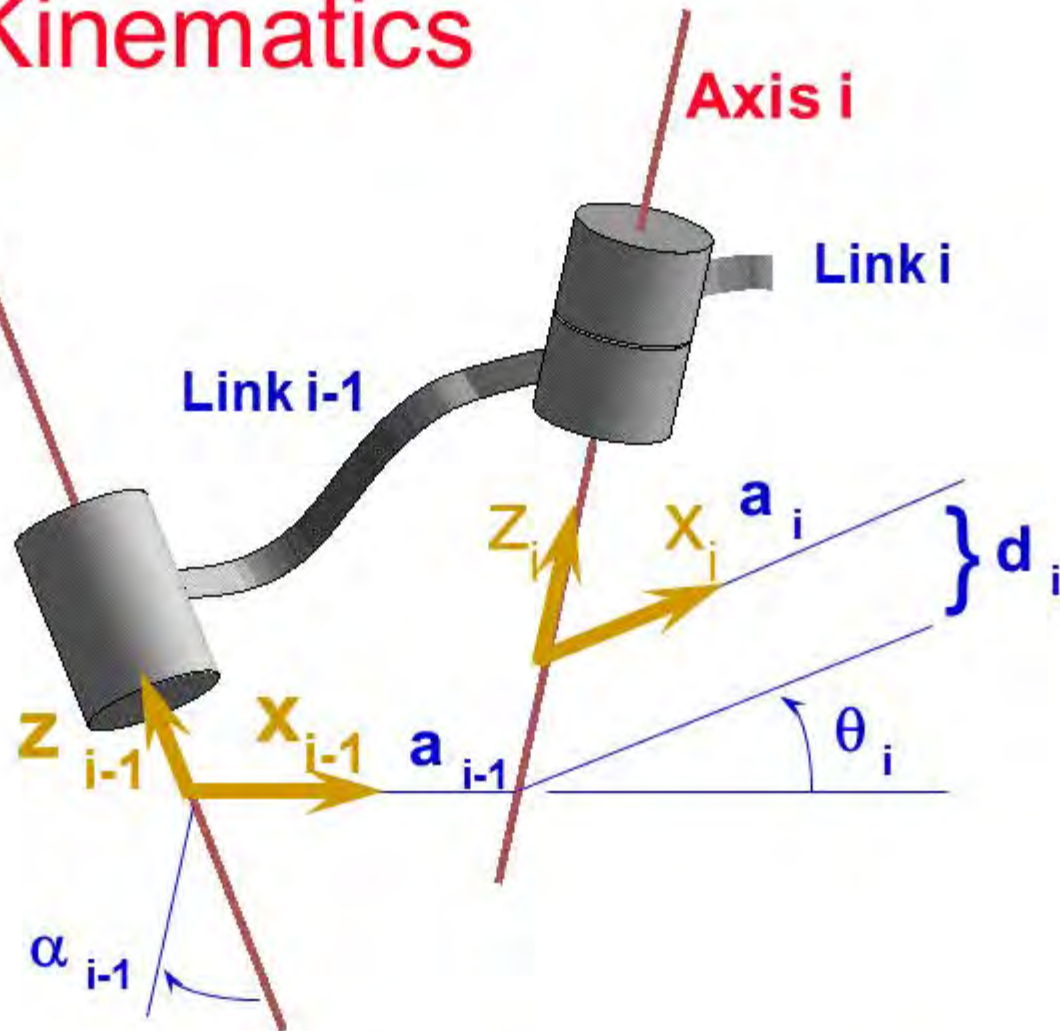


$${}^{i-1}_i \mathbf{T} = \begin{bmatrix} c\theta_i & -s\theta_i & 0 & a_{i-1} \\ s\theta_i c\alpha_{i-1} & c\theta_i c\alpha_{i-1} & -s\alpha_{i-1} & -s\alpha_{i-1} d_i \\ s\theta_i s\alpha_{i-1} & c\theta_i s\alpha_{i-1} & c\alpha_{i-1} & c\alpha_{i-1} d_i \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

Forward Kinematics

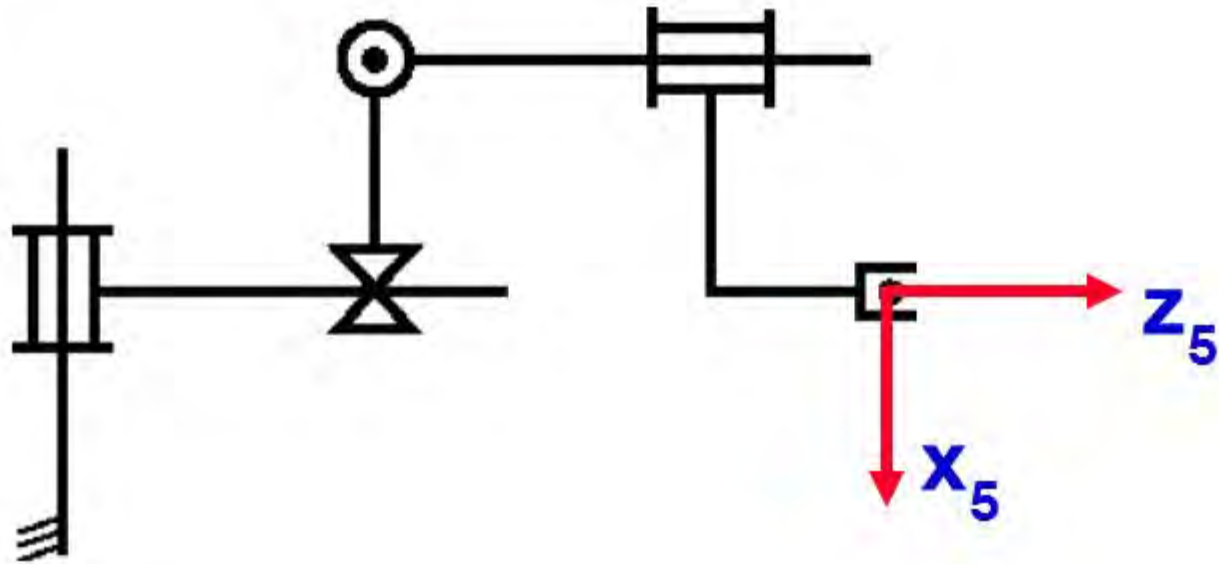
Axis (i-1)

Axis i

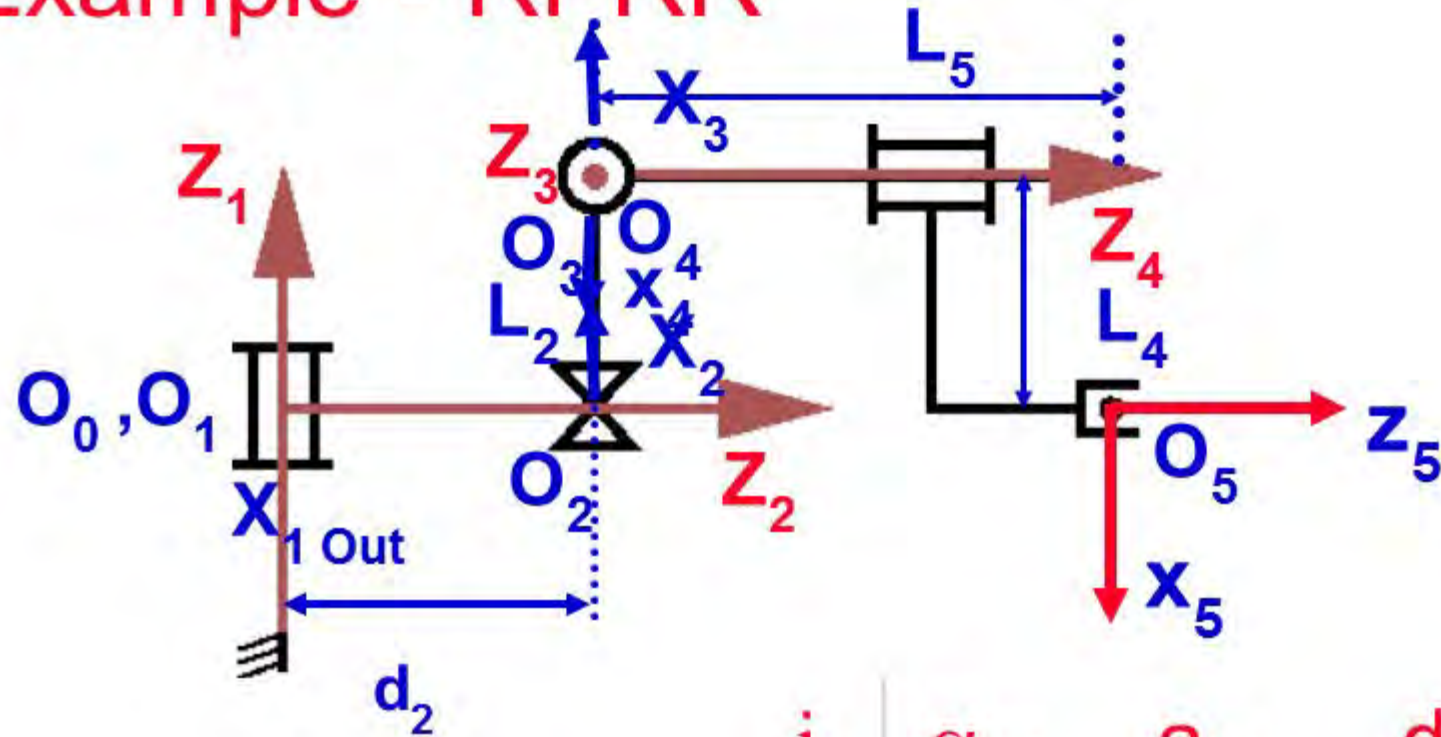


Forward Kinematics: ${}^0_N \mathbf{T} = {}^0_1 \mathbf{T} {}^1_2 \mathbf{T} \dots {}^{N-1}_N \mathbf{T}$

Example - RPRR



Example - RPRR



i	α_{i-1}	a_{i-1}	d_i	θ_i
1	—	—	—	—
2	—	—	—	—
3	—	—	—	—
4	—	—	—	—
5	—	—	—	—

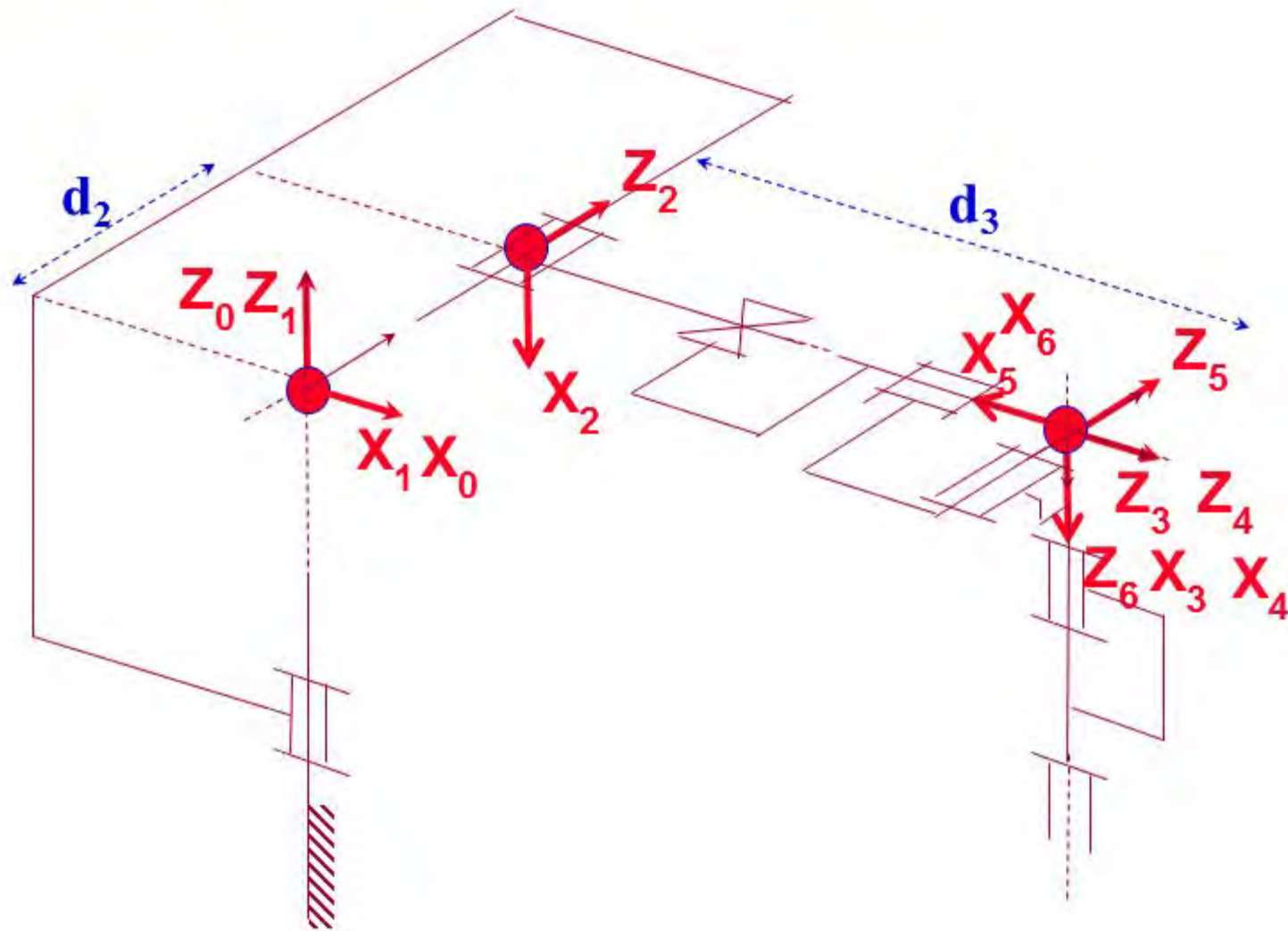
a_i : distance (z_i, z_{i+1}) along x_i
 α_i : angle (z_i, z_{i+1}) about x_i
 d_i : distance (x_{i-1}, x_i) along z_i
 θ_i : angle (x_{i-1}, x_i) about z_i

Stanford Scheinman Arm

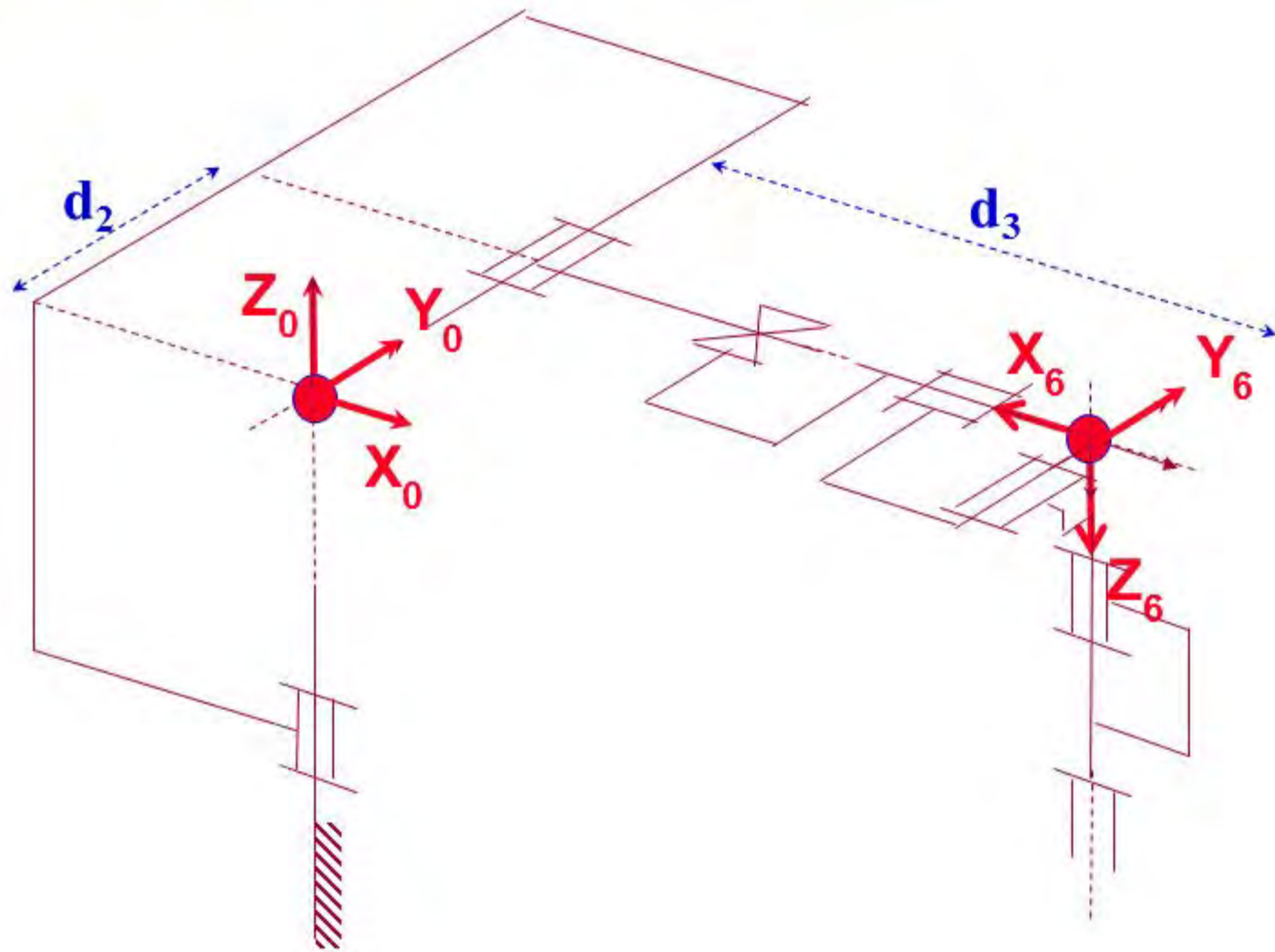


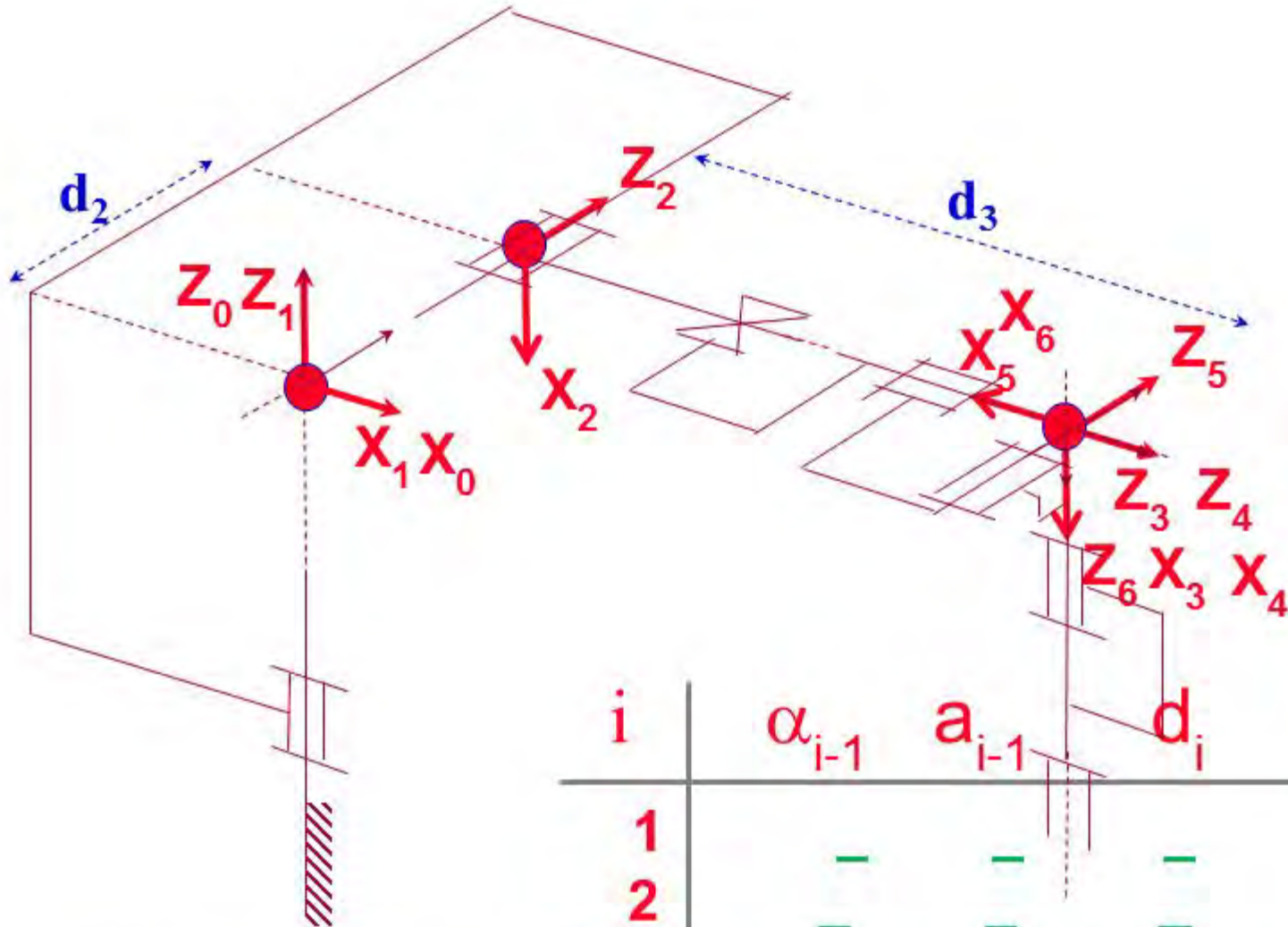
Victor Scheinman (around 1968)

Stanford Scheinman Arm



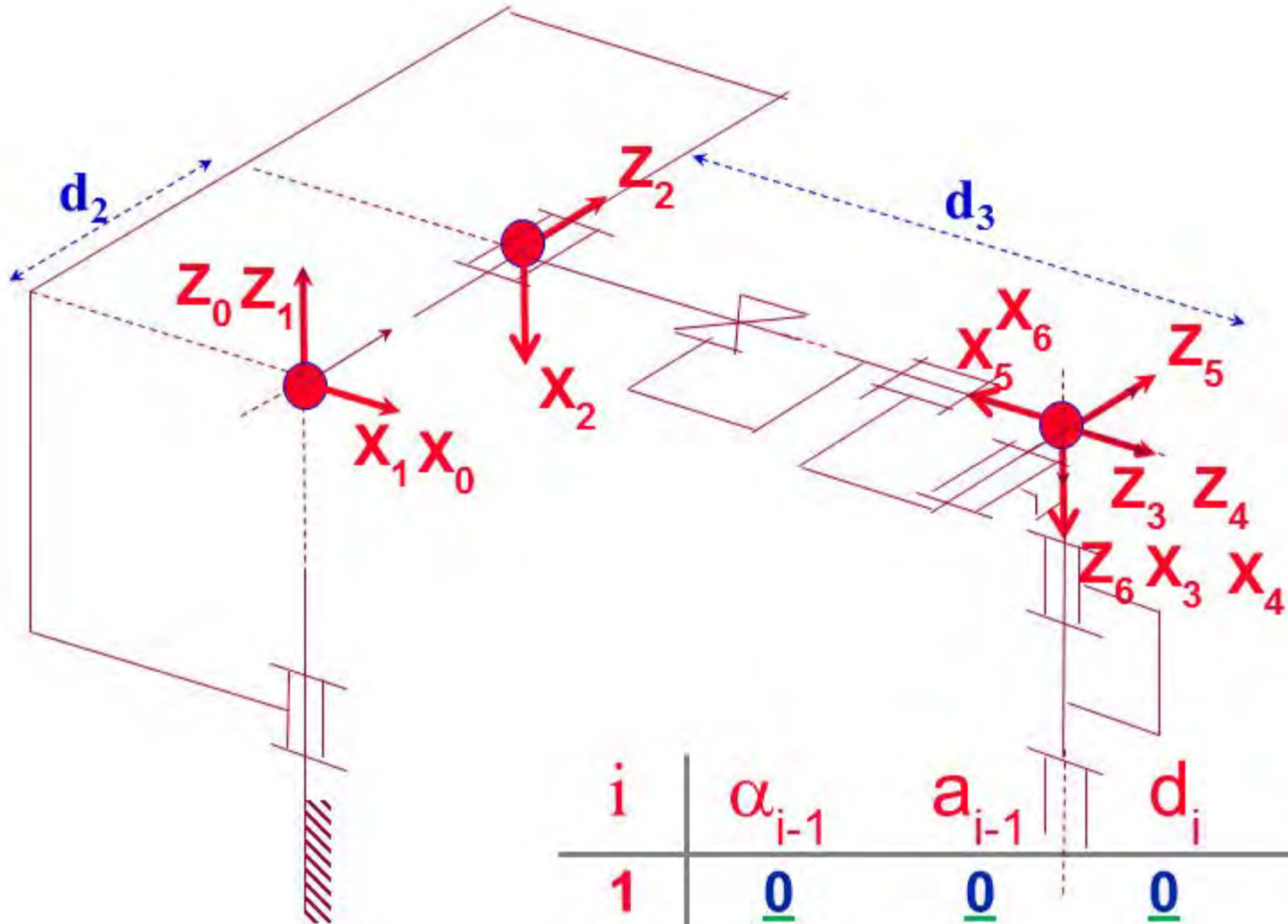
Stanford Scheinman Arm





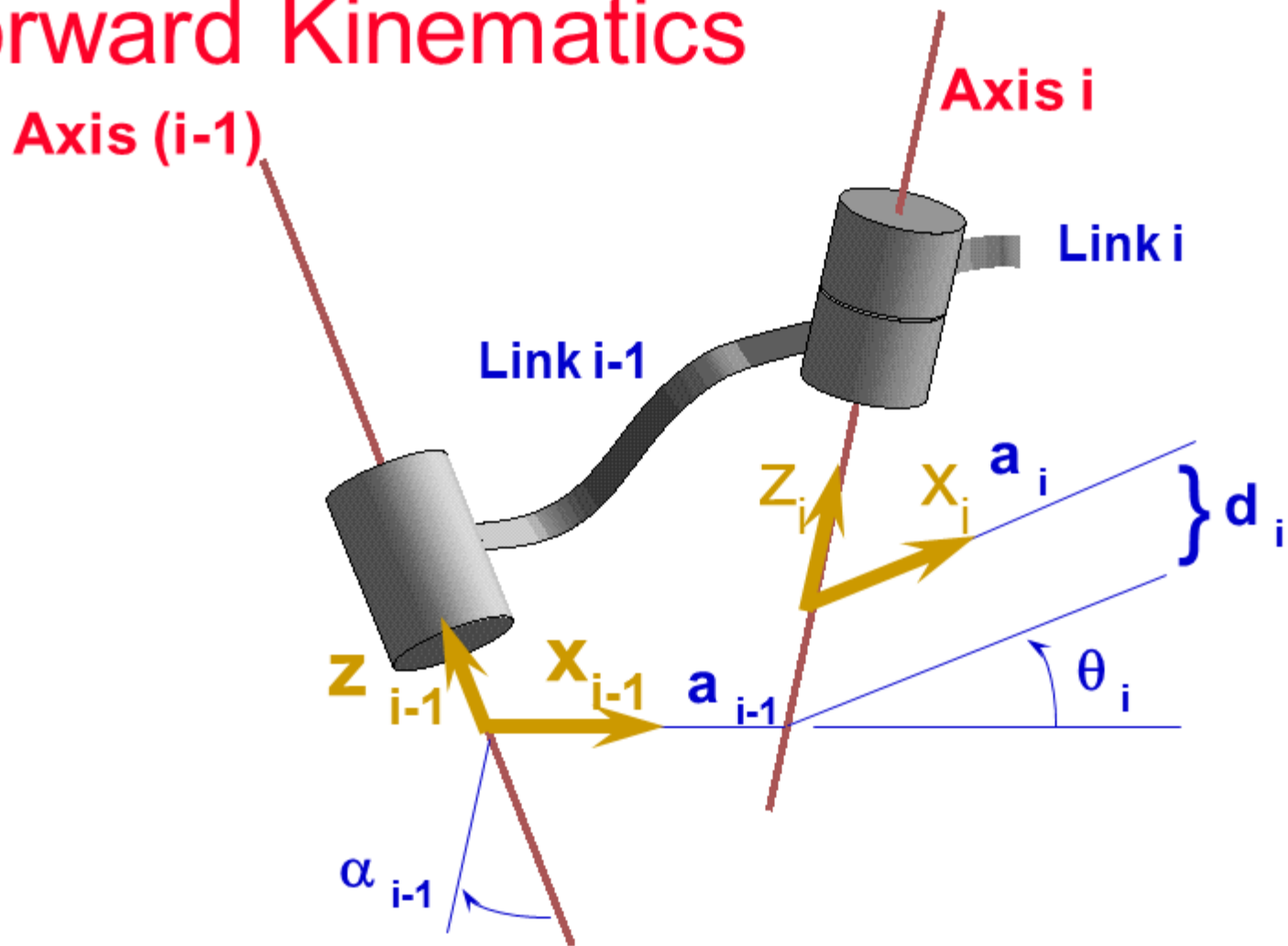
i	α_{i-1}	a_{i-1}	d_i	θ_i
1	—	—	—	—
2	—	—	—	—
3	—	—	—	—
4	—	—	—	—
5	—	—	—	—
6	—	—	—	—

a_i : distance (z_i, z_{i+1}) along x_i
 α_i : angle (z_i, z_{i+1}) about x_i
 d_i : distance (x_{i-1}, x_i) along z_i
 θ_i : angle (x_{i-1}, x_i) about z_i



i	α_{i-1}	a_{i-1}	d_i	θ_i
1	0	0	0	θ_1
2	90	0	d_2	θ_2
3	90	0	d_3	0
4	0	0	0	θ_4
5	-90	0	0	θ_5
6	90	0	0	θ_6

Forward Kinematics



$${}^{i-1}_i \mathbf{T} = \begin{bmatrix} c\theta_i & -s\theta_i & 0 & a_{i-1} \\ s\theta_i c\alpha_{i-1} & c\theta_i c\alpha_{i-1} & -s\alpha_{i-1} & -s\alpha_{i-1} d_i \\ s\theta_i s\alpha_{i-1} & c\theta_i s\alpha_{i-1} & c\alpha_{i-1} & c\alpha_{i-1} d_i \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

Stanford Scheinman Arm

i	α_{i-1}	a_{i-1}	d_i	θ_i
1	0	0	0	θ_1
2	-90	0	d_2	θ_2
3	90	0	d_3	0
4	0	0	0	θ_4
5	-90	0	0	θ_5
6	90	0	0	θ_6

$$\begin{bmatrix} c\theta_i & -s\theta_i & 0 & a_{i-1} \\ s\theta_i c\alpha_{i-1} & c\theta_i c\alpha_{i-1} & -s\alpha_{i-1} & -s\alpha_{i-1} d_i \\ s\theta_i s\alpha_{i-1} & c\theta_i s\alpha_{i-1} & c\alpha_{i-1} & c\alpha_{i-1} d_i \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$${}^0_1T = \begin{bmatrix} c_1 & -s_1 & 0 & 0 \\ s_1 & c_1 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$${}^1_2T = \begin{bmatrix} c_2 & -s_2 & 0 & 0 \\ 0 & 0 & 1 & d_2 \\ -s_2 & -c_2 & 0 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$${}^2_3T = \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 0 & -1 & -d_3 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$${}^3_4T = \begin{bmatrix} c_4 & -s_4 & 0 & 0 \\ s_4 & c_4 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

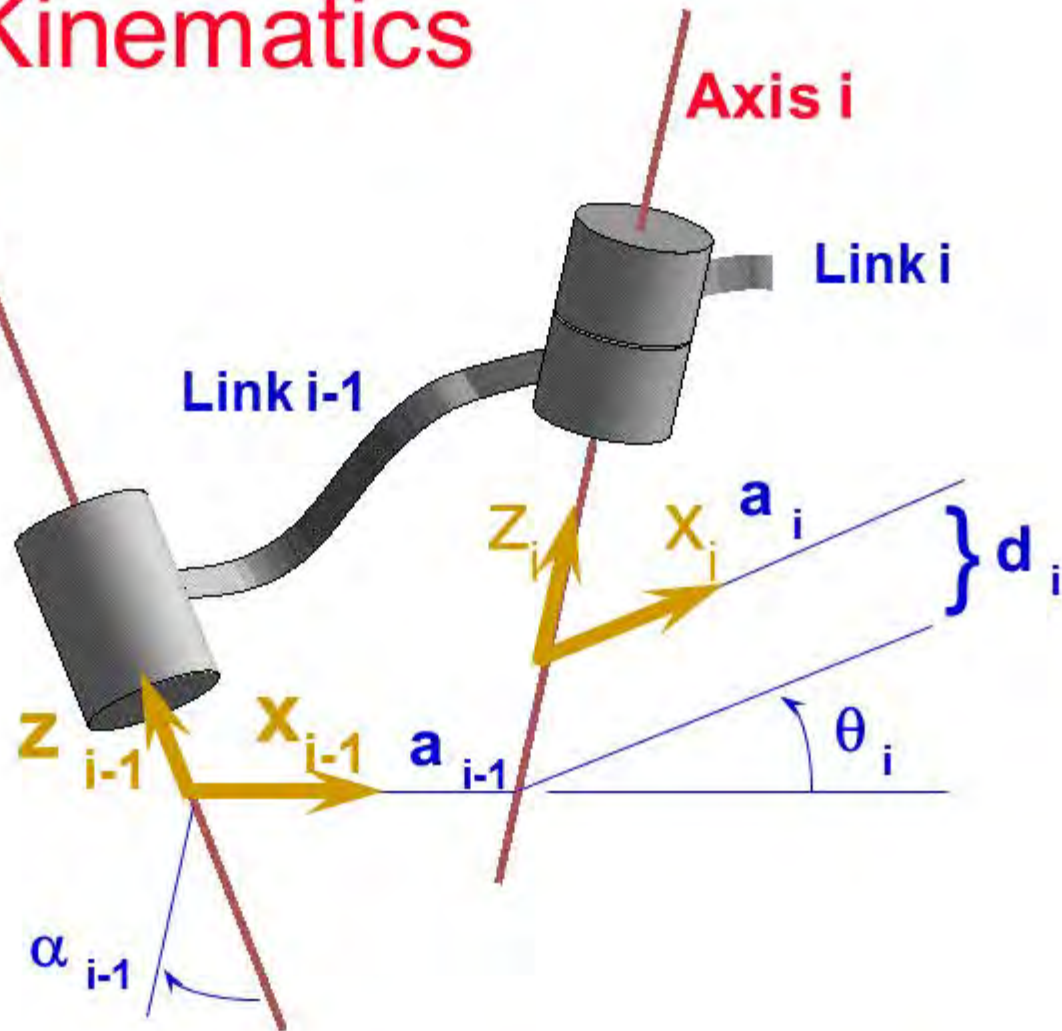
$${}^4_5T = \begin{bmatrix} c_5 & -s_5 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ -s_5 & -c_5 & 0 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$${}^5_6T = \begin{bmatrix} c_6 & -s_6 & 0 & 0 \\ 0 & 0 & -1 & 0 \\ s_6 & c_6 & 0 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

Forward Kinematics

Axis (i-1)

Axis i



Forward Kinematics: ${}^0_N \mathbf{T} = {}^0_1 \mathbf{T} {}^1_2 \mathbf{T} \dots {}^{N-1}_N \mathbf{T}$

$${}^0_1T = \begin{bmatrix} c_1 & -s_1 & 0 & 0 \\ s_1 & c_1 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$${}^0_2T = \begin{bmatrix} c_1c_2 & -c_1s_2 & -s_1 & -s_1d_2 \\ s_1c_2 & -s_1s_2 & c_1 & c_1d_2 \\ -s_2 & -c_2 & 0 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

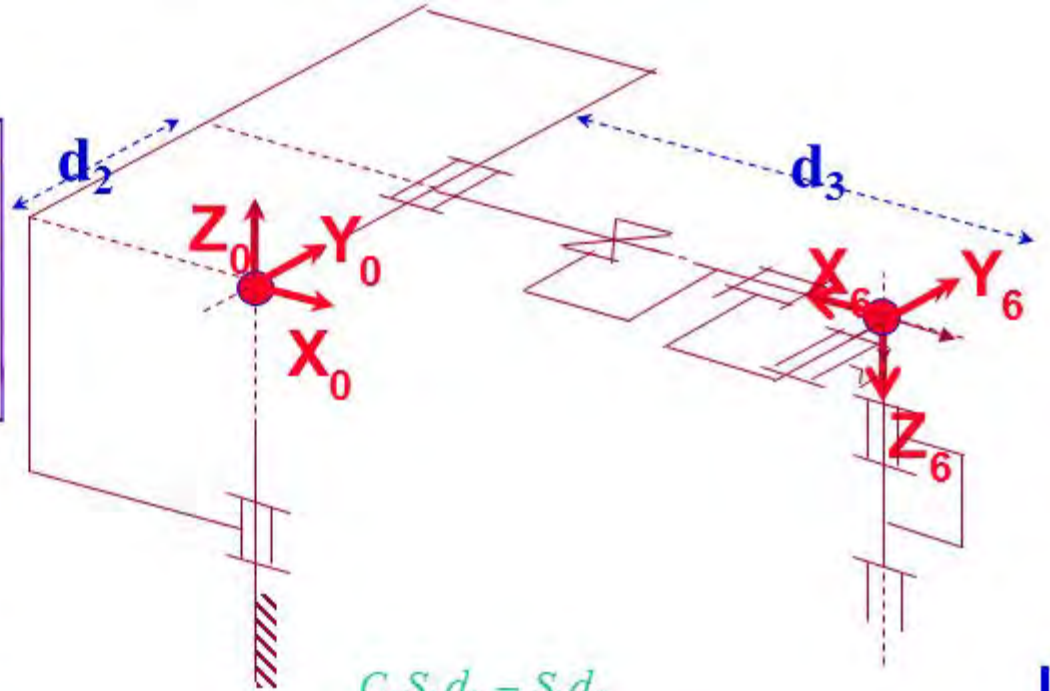
$${}^0_3T = \begin{bmatrix} c_1c_2 & -s_1 & c_1s_2 & c_1d_3s_2 - s_1d_2 \\ s_1c_2 & c_1 & s_1s_2 & s_1d_3s_2 + c_1d_2 \\ -s_2 & 0 & c_2 & d_3c_2 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$${}^0_4T = \begin{bmatrix} c_1c_2c_4 - s_1s_4 & -c_1c_2s_4 - s_1c_4 & c_1s_2 & c_1d_3s_2 - s_1d_2 \\ s_1c_2c_4 + c_1s_4 & -s_1c_2s_4 + c_1c_4 & s_1s_2 & s_1d_3s_2 + c_1d_2 \\ -s_2c_4 & s_2s_4 & c_2 & d_3c_2 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$${}^0_5T = \begin{bmatrix} X & X & -c_1c_2s_4 - s_1c_4 & c_1d_3s_2 - s_1d_2 \\ X & X & -s_1c_2s_4 + c_1c_4 & s_1d_3s_2 + c_1d_2 \\ X & X & s_2s_4 & d_3c_2 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$${}^0_6T = \begin{bmatrix} X & X & c_1c_2c_4s_5 - s_1s_4s_5 + c_1s_2s_5 & c_1d_3s_2 - s_1d_2 \\ X & X & s_1c_2c_4s_5 + c_1s_4s_5 + s_1s_2c_5 & s_1d_3s_2 + c_1d_2 \\ X & X & -s_2c_4s_5 + c_5c_2 & d_3c_2 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$${}^0_6T = \begin{bmatrix} X & X & c_1c_2c_4s_5 - s_1s_4s_5 + c_1s_2s_5 & cds_2 - s_1d_2 \\ X & X & s_1c_2c_4s_5 + c_1s_4s_5 + s_1s_2c_5 & s_1ds_2 + c_1d_2 \\ X & X & -s_2c_4s_5 + c_5c_2 & d_3c_2 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$



$$x = \begin{pmatrix} x_P \\ r_1 \\ r_2 \\ r_3 \end{pmatrix} =$$

$$\begin{aligned} &C_1S_2d_3 - S_1d_2 \\ &S_1S_2d_3 + C_1d_2 \\ &C_2d_3 \end{aligned}$$

$$\begin{aligned} &C_1[C_2(C_4C_5C_6 - S_4S_6) - S_2S_5C_6] - S_1(S_4C_5C_6 + C_4S_6) \\ &S_1[C_2(C_4C_5C_6 - S_4S_6) - S_2S_5C_6] + C_1(S_4C_5C_6 + C_4S_6) \\ &\quad - S_2(C_4C_5C_6 - S_4S_6) - C_2S_5C_6 \\ &C_1[-C_2(C_4C_5S_6 + S_4C_6) + S_2S_5S_6] - S_1(-S_4C_5S_6 + C_4C_6) \\ &S_1[-C_2(C_4C_5S_6 + S_4C_6) + S_2S_5S_6] + C_1(-S_4C_5S_6 + C_4C_6) \\ &\quad S_2(C_4C_5S_6 + S_4C_6) + C_2S_5S_6 \\ &C_1(C_2C_4S_5 + S_2C_5) - S_1S_4S_5 \\ &S_1(C_2C_4S_5 + S_2C_5) + C_1S_4S_5 \\ &\quad - S_2C_4S_5 + C_2C_5 \end{aligned}$$