

introduction to
Robotics



Lecture Notes, CS223A, Winter 2013-2014

O. Khatib and K. Kolarov

Movie Segment

Pet-Proto Robot Navigates
Obstacles, Boston Dynamics,
2012

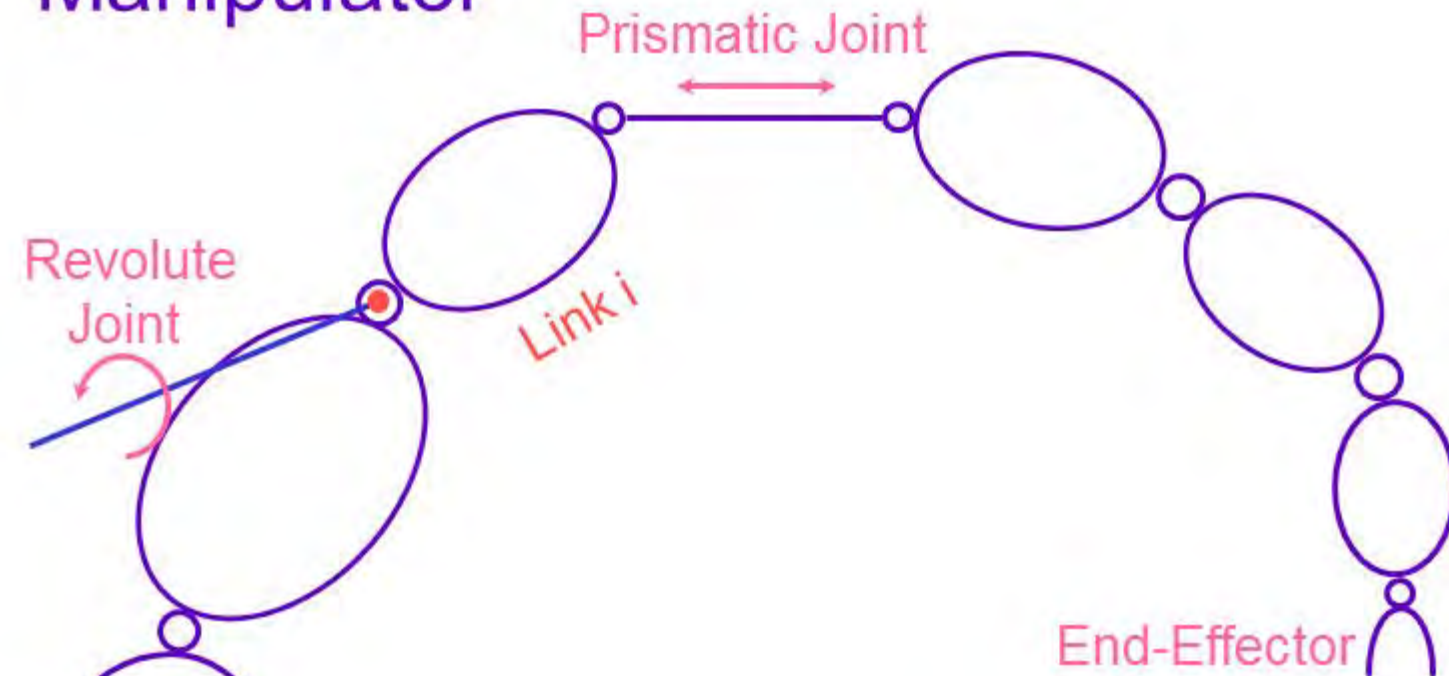
Kinematics

Spatial Descriptions

- Task Description
- Transformations
- Representations



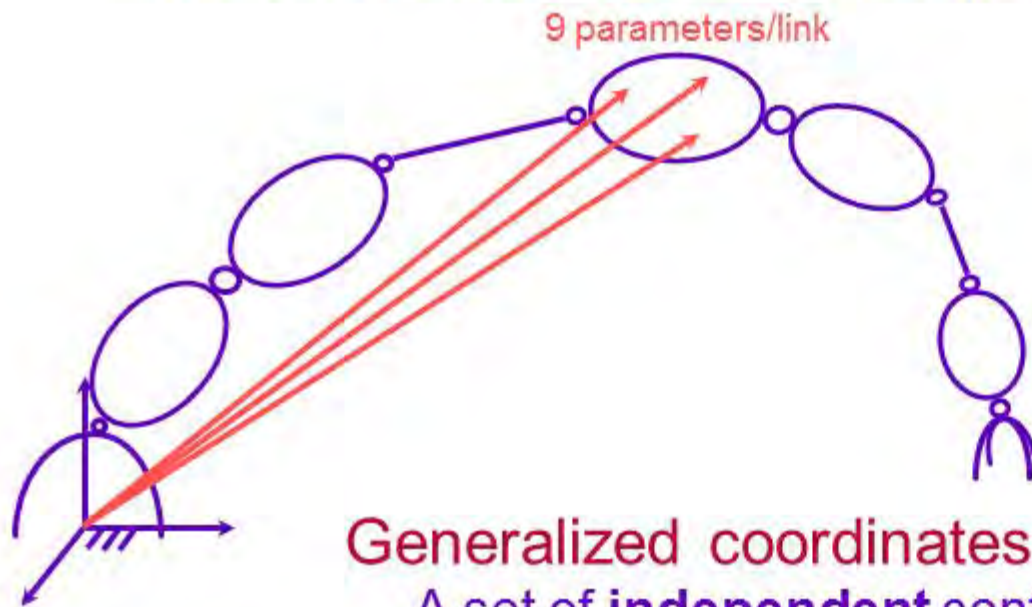
Manipulator



- Links:** n moving link
1 fixed link
- Joints:** Revolute (1 DOF)
Prismatic (1 DOF)

Configuration Parameters

A set of position parameters that describes the full configuration of the system.



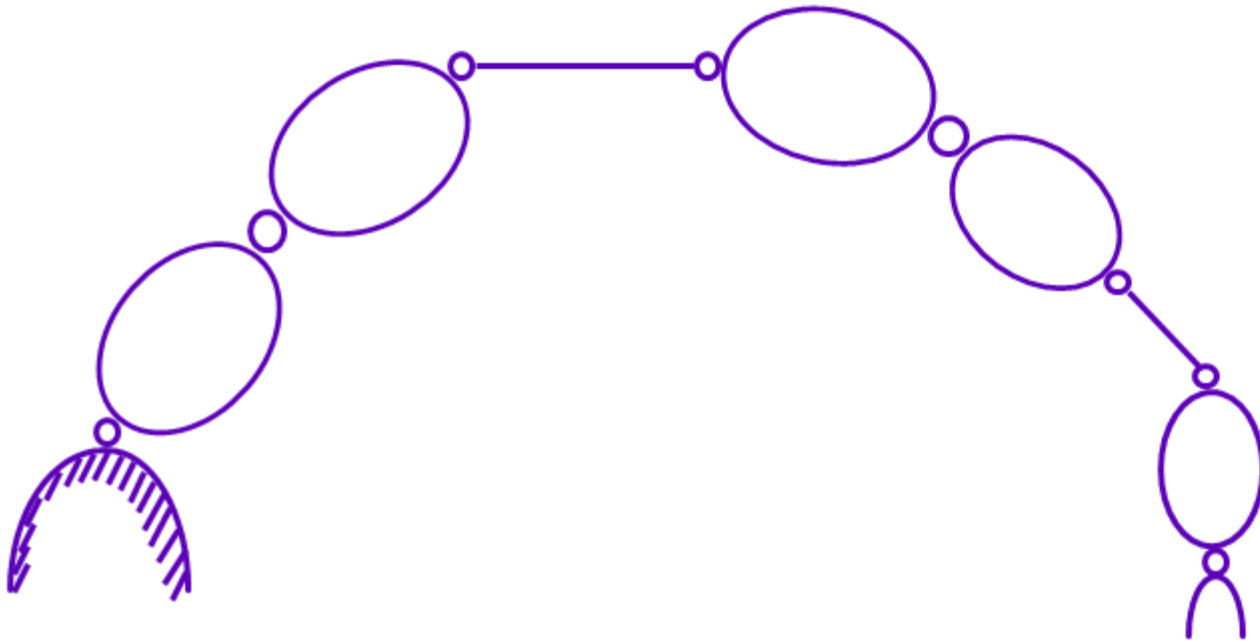
Generalized coordinates

A set of **independent** configuration parameters

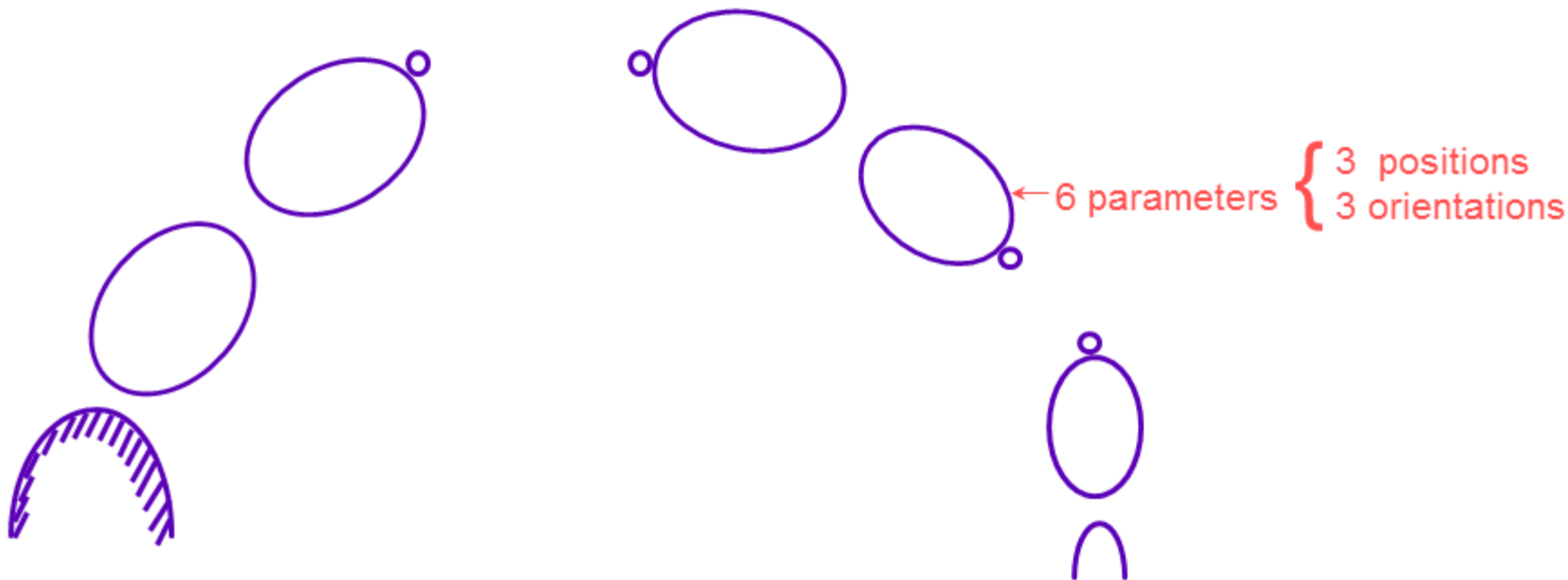
Degrees of Freedom

Number of generalized coordinates

Generalized Coordinates



Generalized Coordinates



n moving links: $6n$ parameters

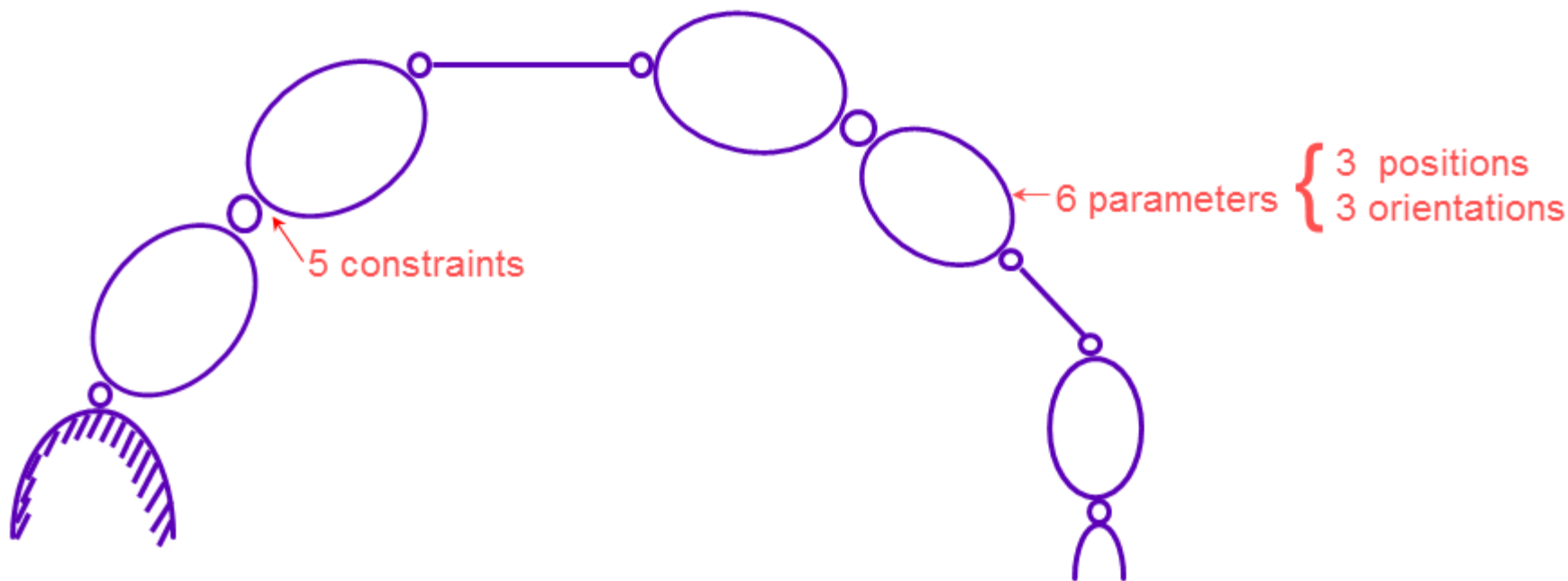
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Generalized Coordinates

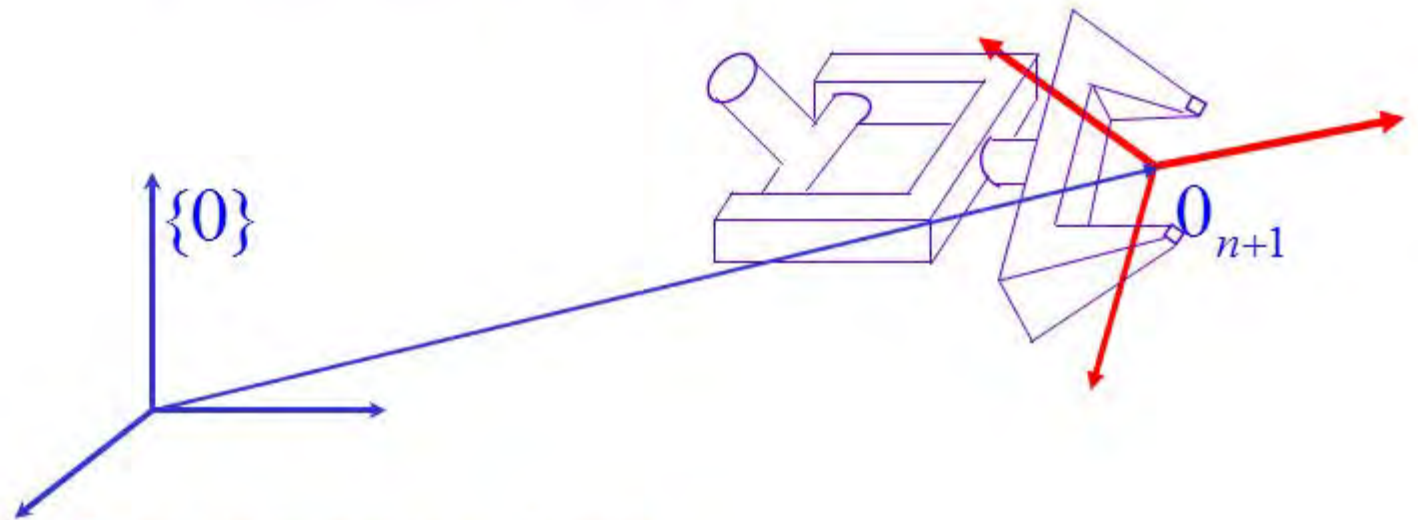


n moving links: $6n$ parameters

n 1 d.o.f. joints: $5n$ constraints

d.o.f. (system): $6n - 5n = n$

End-Effector Configuration Parameters



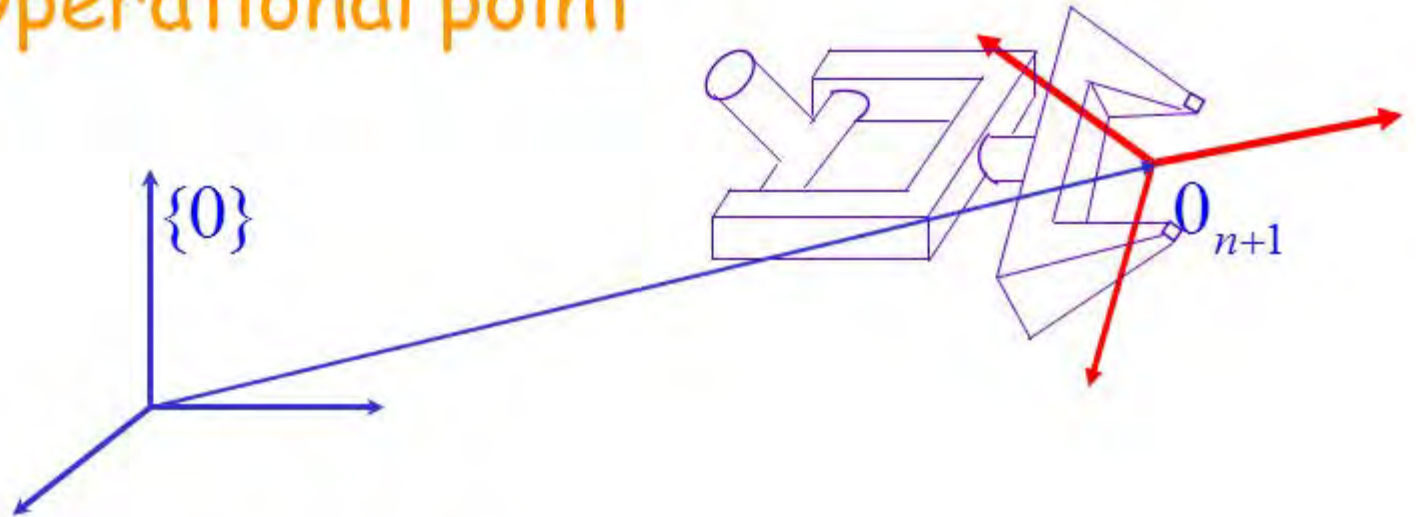
A set of m parameters:

$$(x_1, x_2, x_3, \dots, x_m)$$

that completely specifies the end-effector position and orientation with respect to $\{0\}$

Operational Coordinates

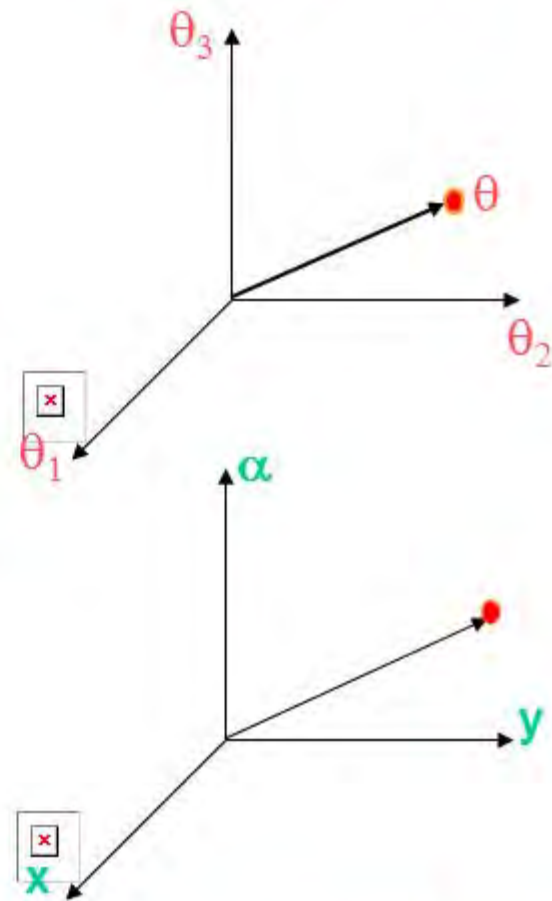
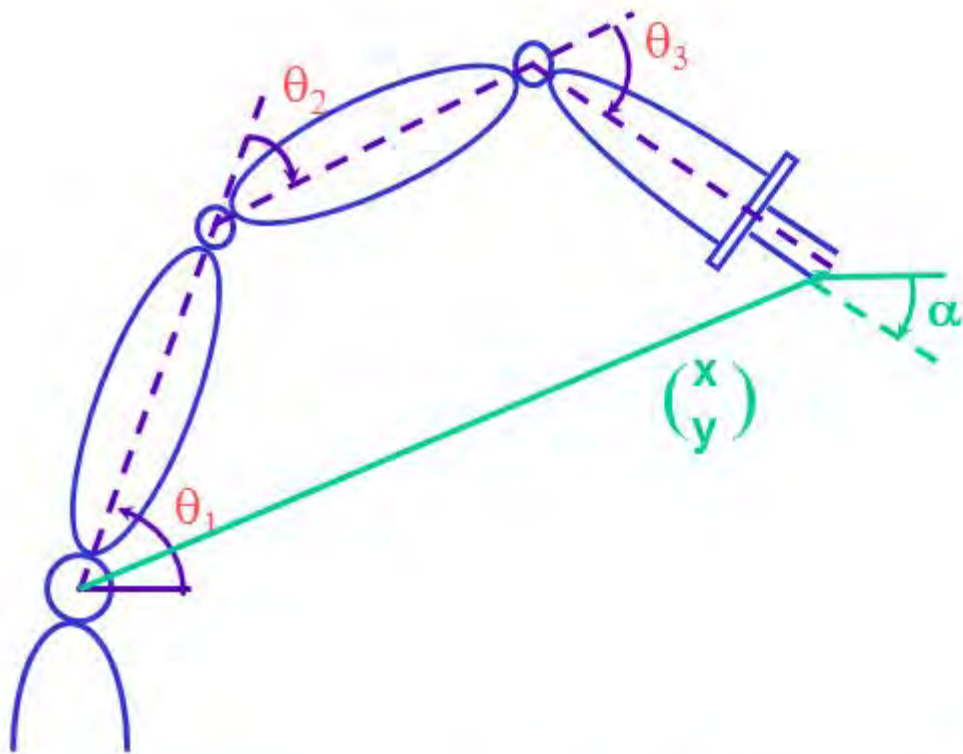
O_{n+1} : Operational point



A set x_1, x_2, \dots, x_{m_0}
of m_0 independent configuration parameters

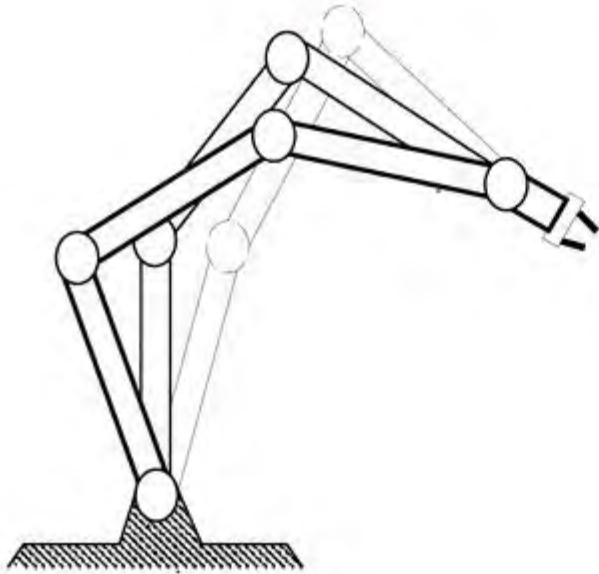
m_0 : number of degrees of freedom
of the end-effector.

Joint Coordinates \longrightarrow Joint Space



Operational Coordinates \longrightarrow Operational Space

Redundancy

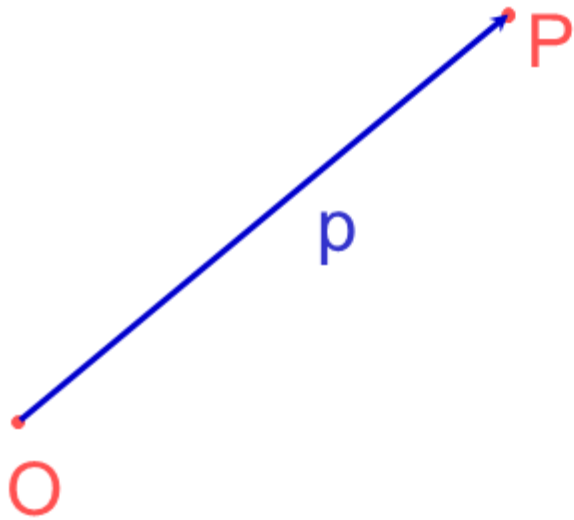


A robot is said to be redundant if

$$n > m_0$$

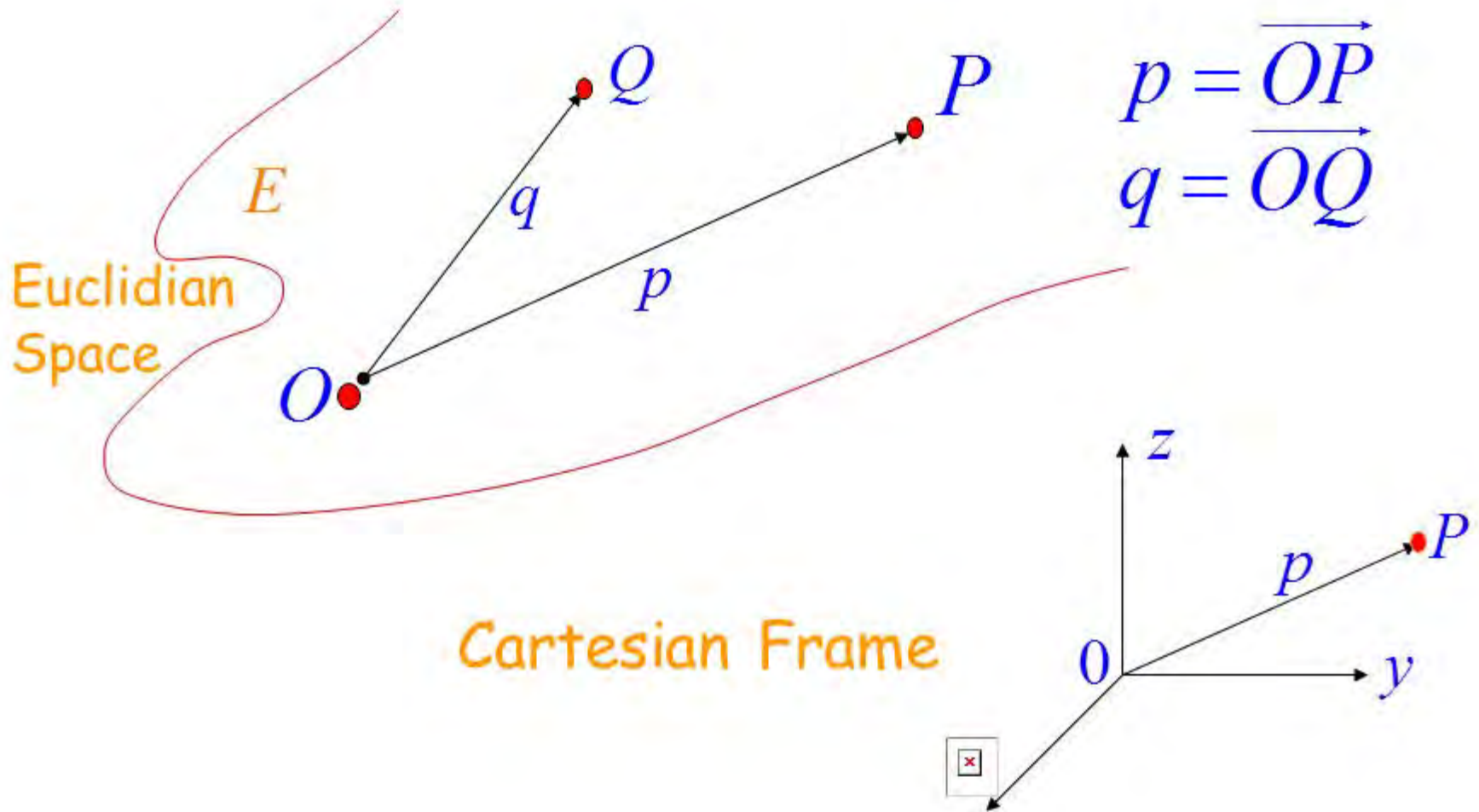
Degrees of redundancy: $n - m_0$

Position of a Point

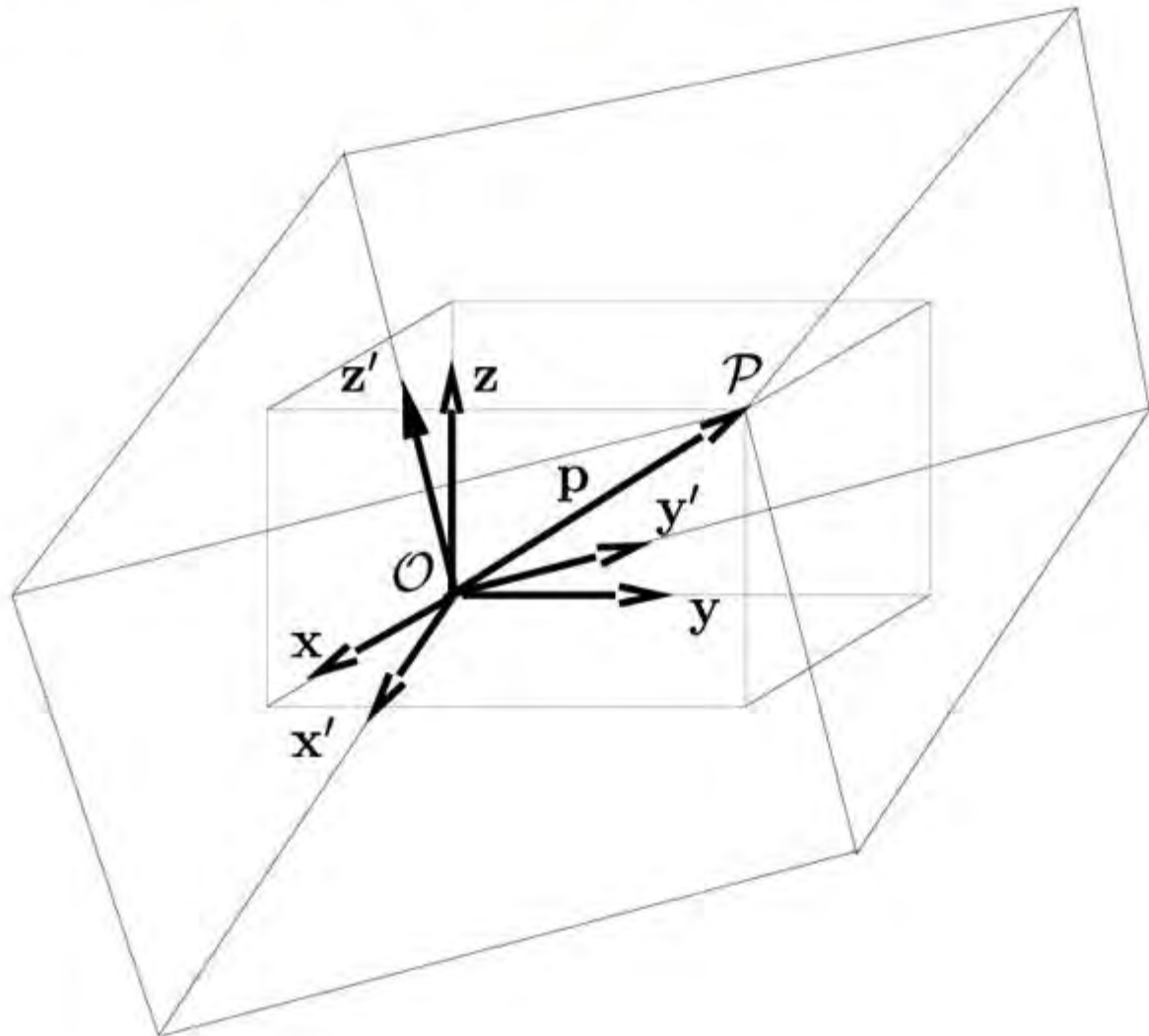


With respect to a fixed origin O , the position of a point P is described by the vector OP or simply by p .

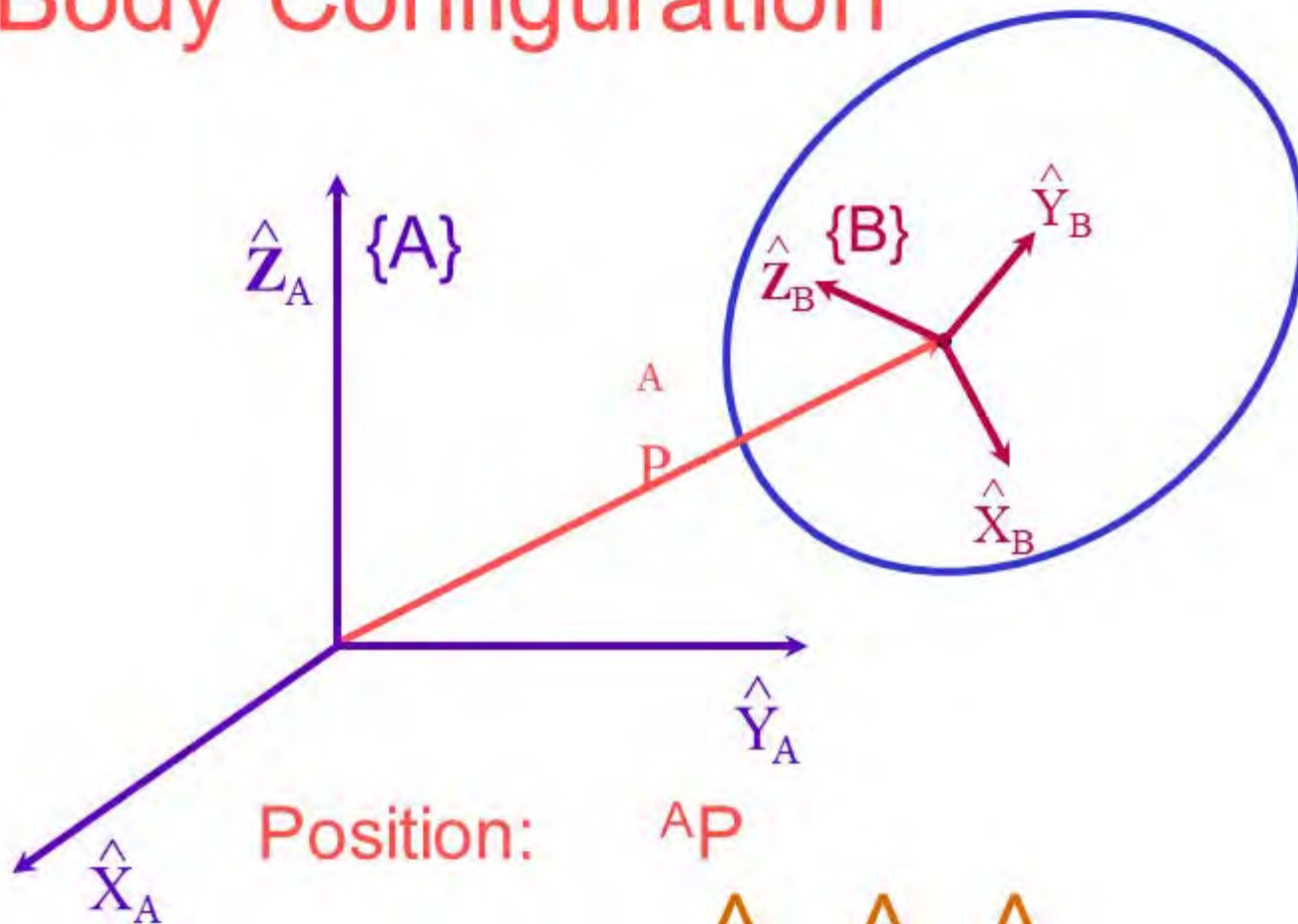
Rigid Body Configuration



Coordinate Frames



Rigid Body Configuration



Position: ${}^A P$

Orientation: $\{ {}^A \hat{X}_B, {}^A \hat{Y}_B, {}^A \hat{Z}_B \}$

describes rotations of {B} with respect to {A}

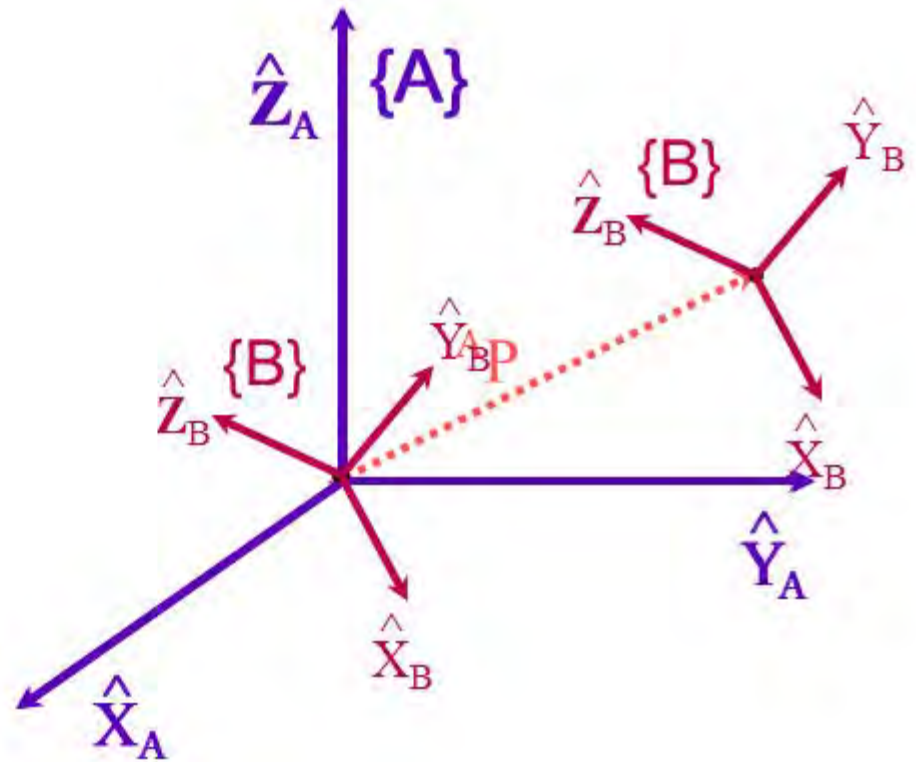


Rotation Matrix

Rotation Matrix

$${}^A_B R = \begin{bmatrix} r_{11} & r_{12} & r_{13} \\ r_{21} & r_{22} & r_{23} \\ r_{31} & r_{32} & r_{33} \end{bmatrix}$$

$${}^A \hat{X}_B = {}^A_B R {}^B \hat{X}_B$$



$${}^A \hat{X}_B = {}^A_B R \begin{bmatrix} 1 \\ 0 \\ 0 \end{bmatrix} \quad {}^A \hat{Y}_B = {}^A_B R \begin{bmatrix} 0 \\ 1 \\ 0 \end{bmatrix} \quad {}^A \hat{Z}_B = {}^A_B R \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix} \quad \longrightarrow \quad {}^A_B R = \begin{bmatrix} {}^A \hat{X}_B & {}^A \hat{Y}_B & {}^A \hat{Z}_B \end{bmatrix}$$

Movie Segment

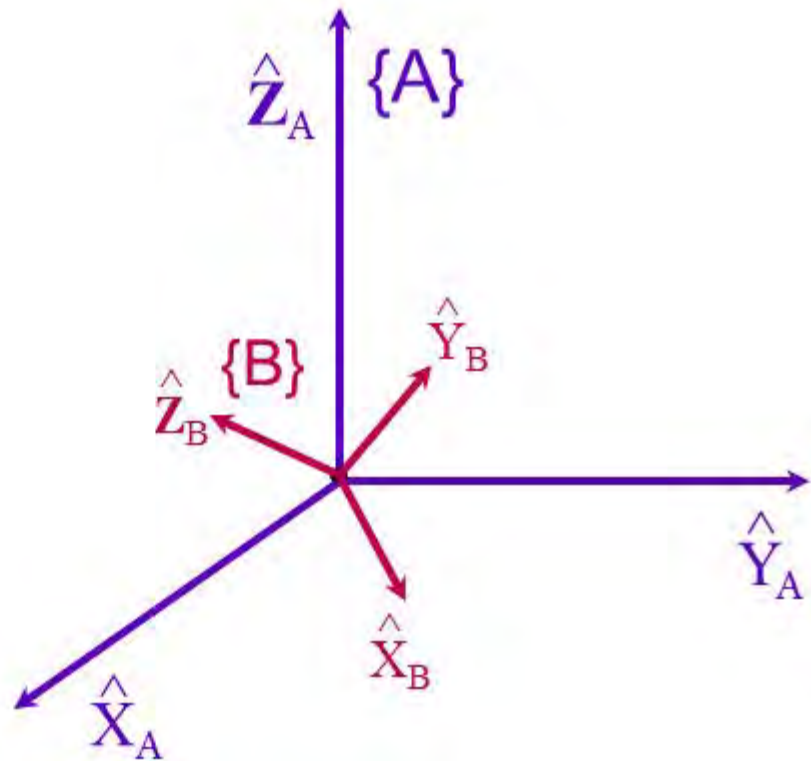
Pet-Proto Robot Navigates
Obstacles, Boston Dynamics,
2012

Rotation Matrix

$${}^A R_B = \begin{bmatrix} {}^A \hat{X}_B & {}^A \hat{Y}_B & {}^A \hat{Z}_B \end{bmatrix}$$

Dot Product

$${}^A \hat{X}_B = \begin{bmatrix} \hat{X}_B \cdot \hat{X}_A \\ \hat{X}_B \cdot \hat{Y}_A \\ \hat{X}_B \cdot \hat{Z}_A \end{bmatrix}$$



$${}^A R_B = \begin{bmatrix} \hat{X}_B \cdot \hat{X}_A & \hat{Y}_B \cdot \hat{X}_A & \hat{Z}_B \cdot \hat{X}_A \\ \hat{X}_B \cdot \hat{Y}_A & \hat{Y}_B \cdot \hat{Y}_A & \hat{Z}_B \cdot \hat{Y}_A \\ \hat{X}_B \cdot \hat{Z}_A & \hat{Y}_B \cdot \hat{Z}_A & \hat{Z}_B \cdot \hat{Z}_A \end{bmatrix} \quad {}^B X_A^T$$

Rotation Matrix

$${}^A_B R = \begin{bmatrix} {}^A \hat{X}_B & {}^A \hat{Y}_B & {}^A \hat{Z}_B \end{bmatrix} = \begin{bmatrix} {}^B \hat{X}_A^T \\ {}^B \hat{Y}_A^T \\ {}^B \hat{Z}_A^T \end{bmatrix} = \begin{bmatrix} {}^B \hat{X}_A & {}^B \hat{Y}_A & {}^B \hat{Z}_A \end{bmatrix}^T = {}^B_A R^T$$

$$\underline{\underline{{}^A_B R = {}^B_A R^T}}$$

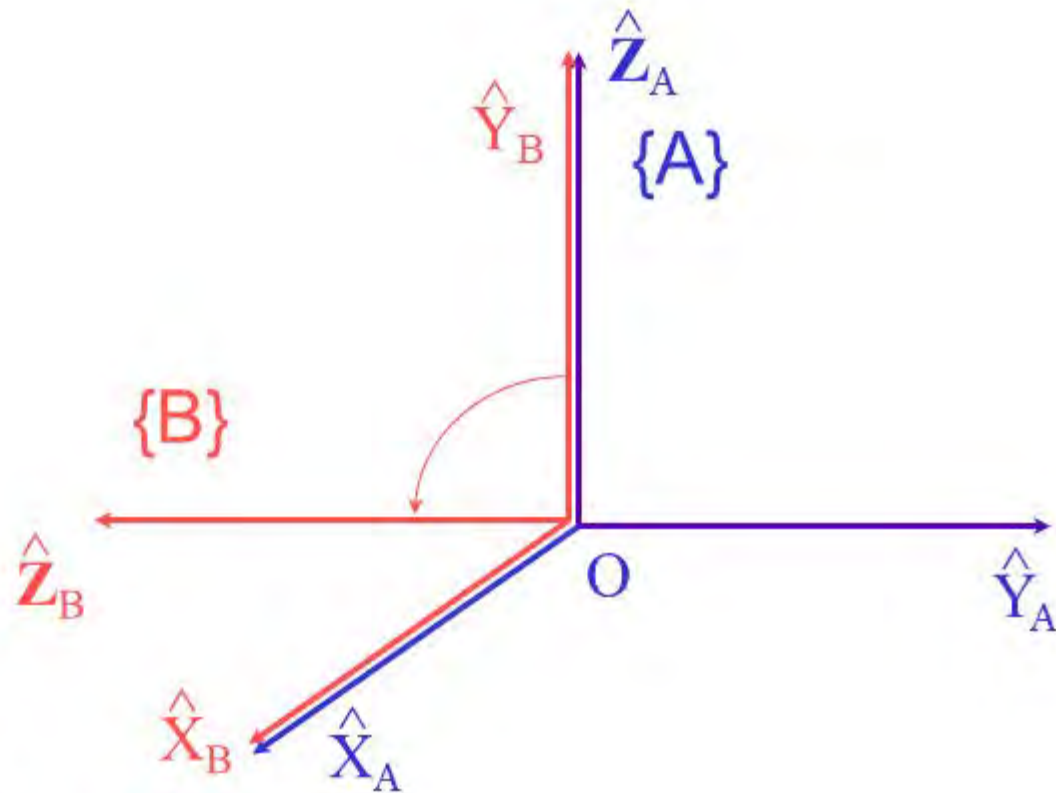
Inverse of Rotation Matrices

$${}^A_B R^{-1} = {}^B_A R = {}^A_B R^T$$

$$\boxed{{}^A_B R^{-1} = {}^A_B R^T}$$

Orthonormal Matrix

Example

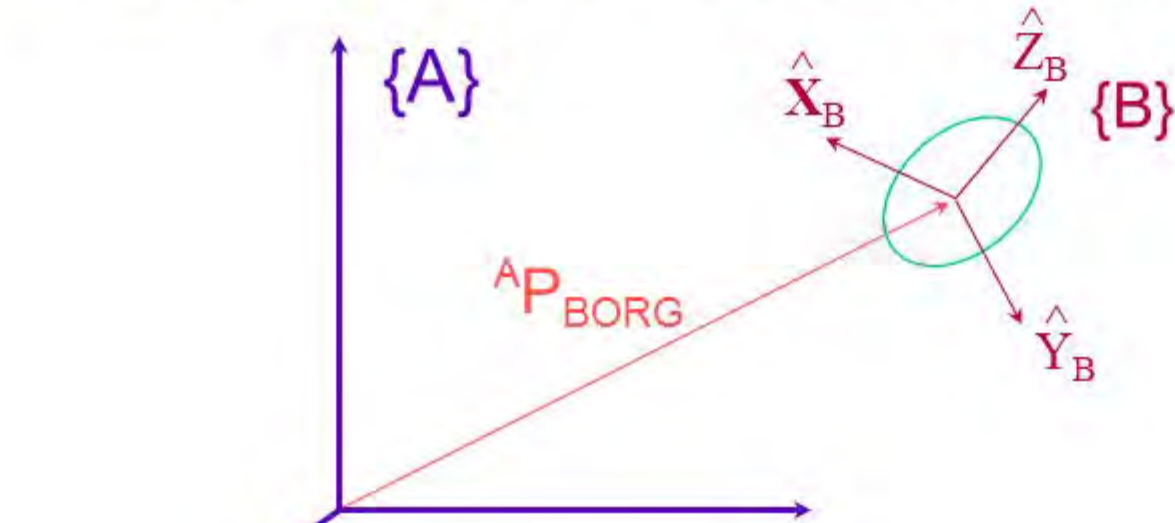


$${}^A_B R = \begin{pmatrix} 1 & 0 & 0 \\ 0 & 0 & -1 \\ 0 & 1 & 0 \end{pmatrix} \begin{matrix} \leftarrow {}^B \hat{X}_A^T \\ \leftarrow {}^B \hat{Y}_A^T \\ \leftarrow {}^B \hat{Z}_A^T \end{matrix}$$

$\uparrow \quad \uparrow \quad \uparrow$
 ${}^A \hat{X}_B \quad {}^A \hat{Y}_B \quad {}^A \hat{Z}_B$

Description of a Frame

with respect to another reference frame



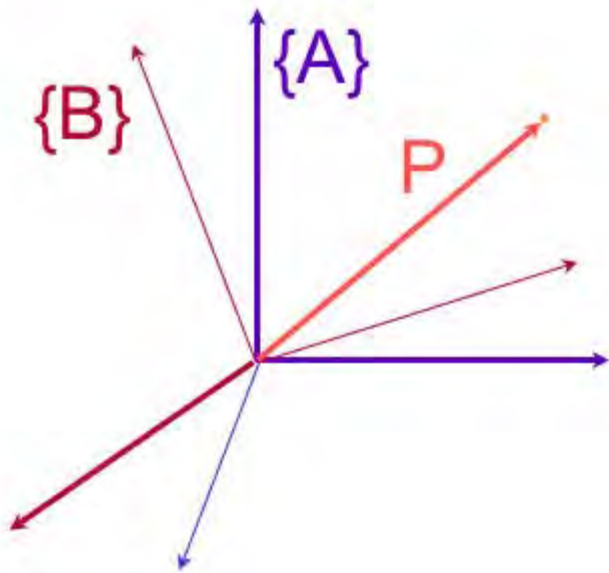
Frame {B}: ${}^A \hat{X}_B, {}^A \hat{Y}_B, {}^A \hat{Z}_B, {}^A P_{Borg}$

$$\{B\} = \left\{ \begin{matrix} {}^A R \\ {}^A P_{Borg} \end{matrix} \right\}$$

Mapping

changing descriptions from frame to frame

Rotations



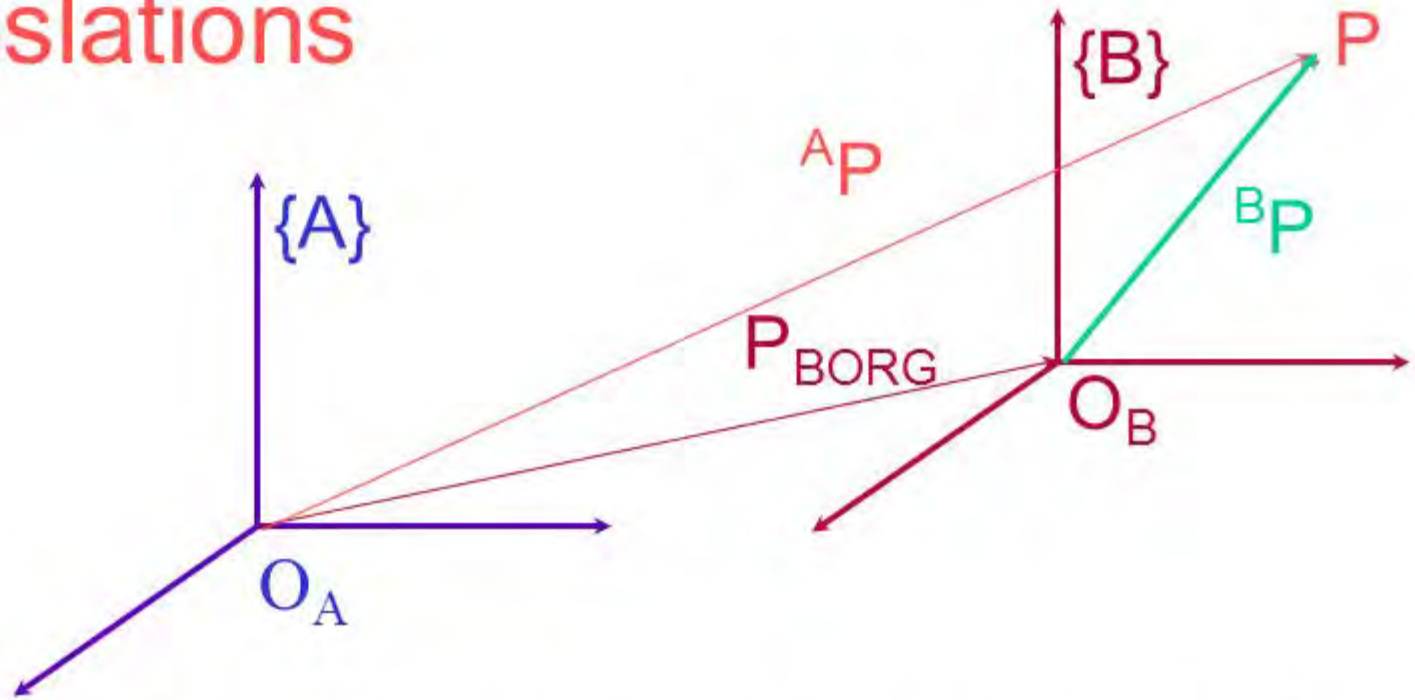
If P is given in $\{B\}$: ${}^B P$

$${}^A P = \begin{pmatrix} {}^B \hat{X}_A \cdot {}^B P \\ {}^B \hat{Y}_A \cdot {}^B P \\ {}^B \hat{Z}_A \cdot {}^B P \end{pmatrix} = \begin{pmatrix} {}^B \hat{X}_A^T \\ {}^B \hat{Y}_A^T \\ {}^B \hat{Z}_A^T \end{pmatrix} \cdot {}^B P$$



$${}^A P = {}^A R_B {}^B P$$

Translations



changing the position description of a point P

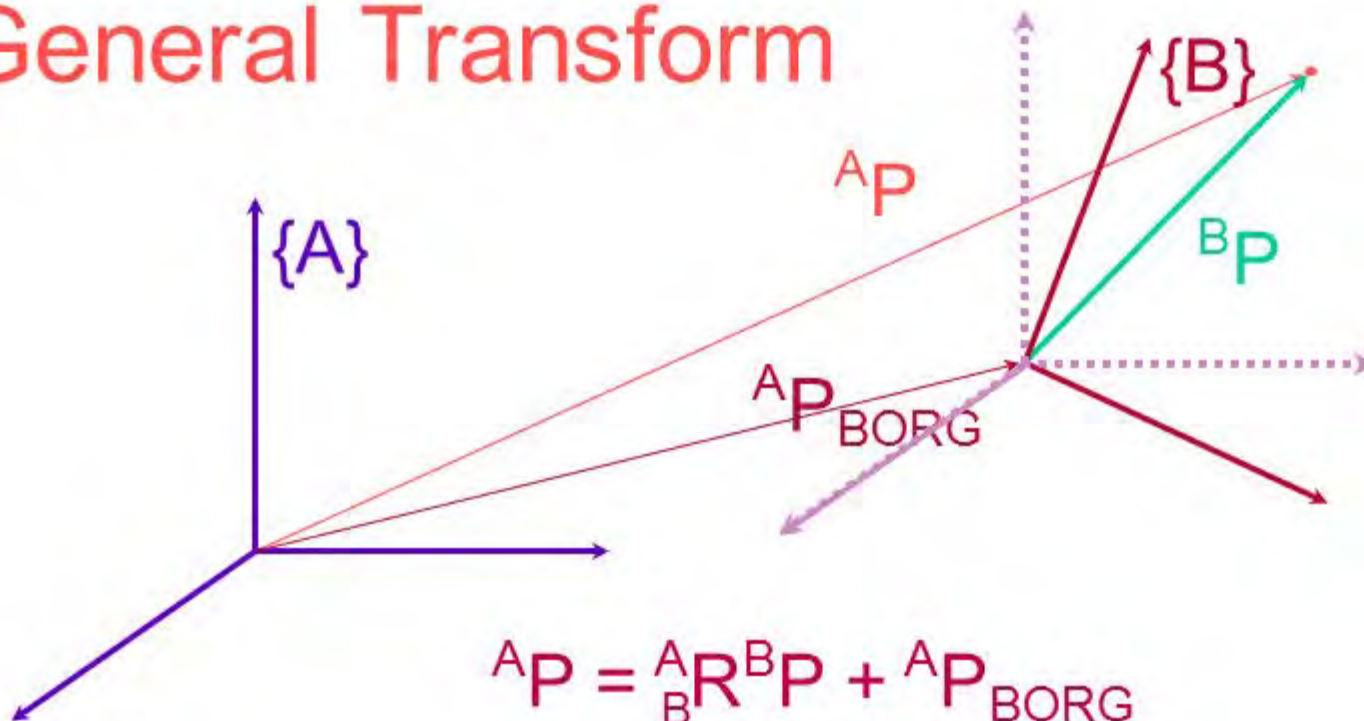
$$\vec{O_B P} \quad \Rightarrow \quad \vec{O_A P}$$

(Two different vectors)

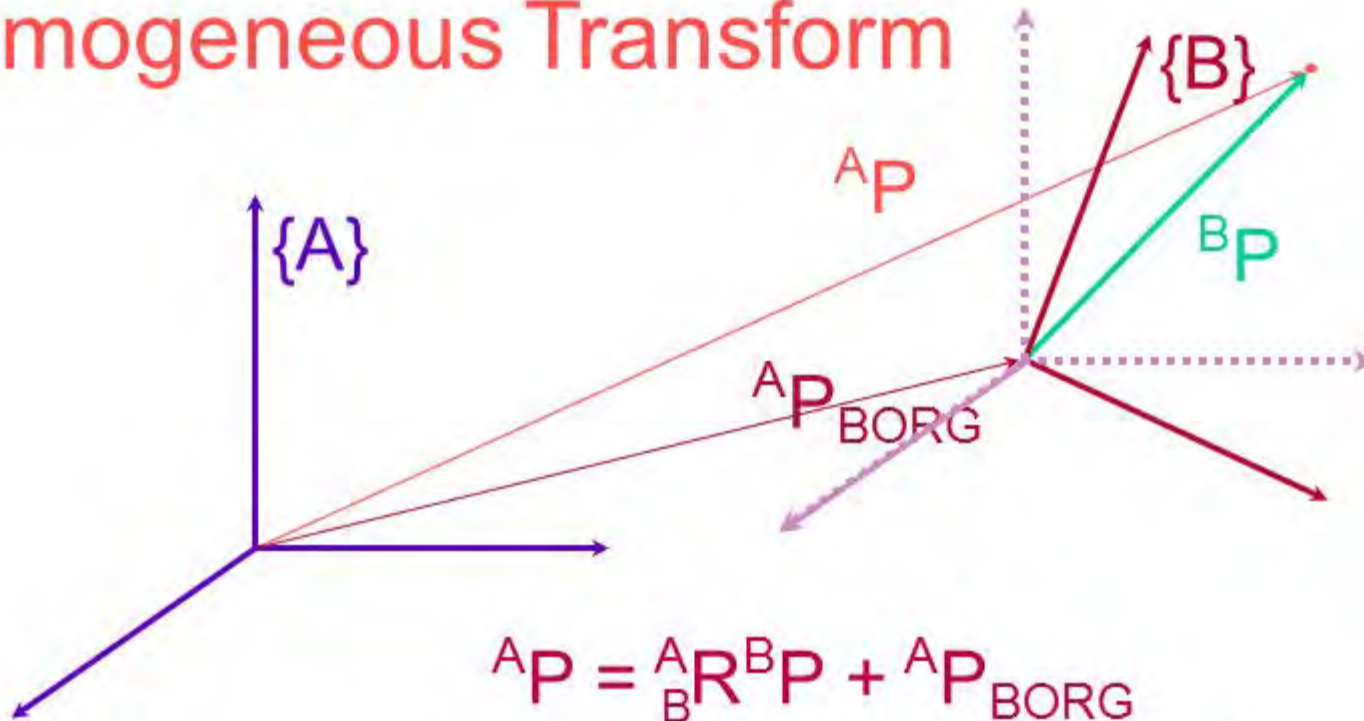
$$P_{BORG} : P_{O_B} \quad \Rightarrow \quad P_{O_A}$$

$$P_{O_A} = P_{O_B} + P_{BORG}$$

General Transform



Homogeneous Transform



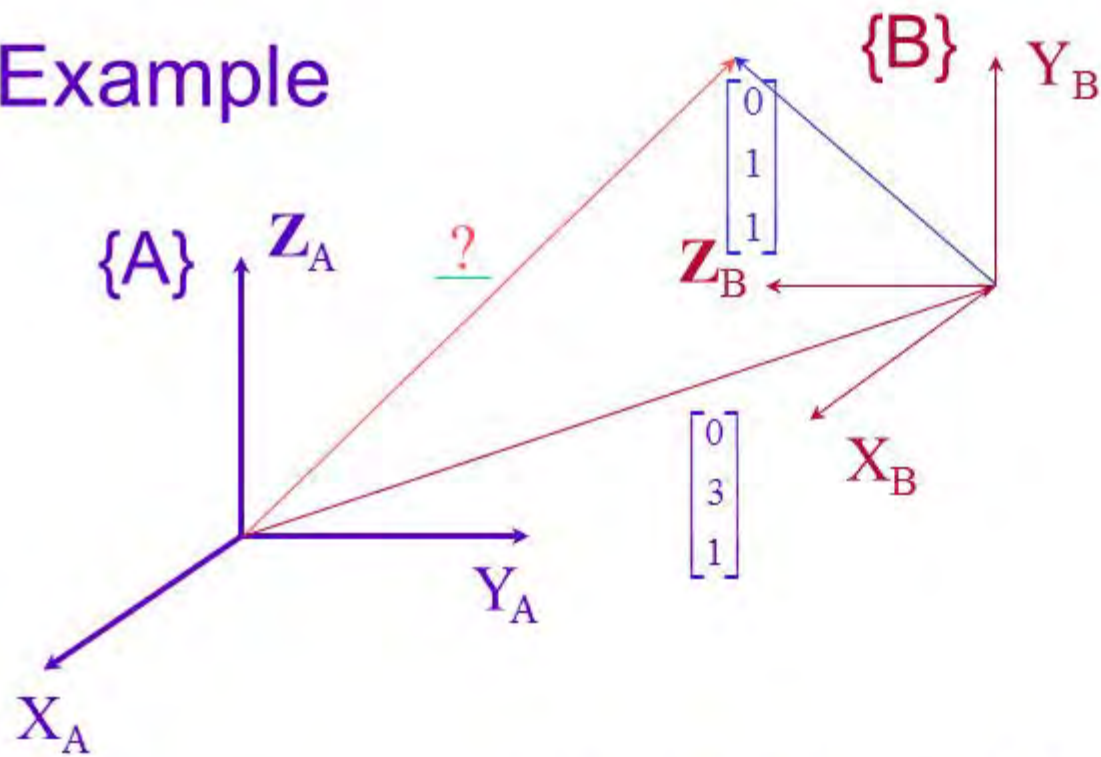
$${}^A P = {}^A R_B {}^B P + {}^A P_{BORG}$$

$$\begin{bmatrix} {}^A P \\ 1 \end{bmatrix} = \begin{bmatrix} {}^A R_B & | & {}^A P_{BORG} \\ \hline 0 & 0 & 0 & | & 1 \end{bmatrix} \begin{bmatrix} {}^B P \\ 1 \end{bmatrix}$$

$$\underline{\underline{{}^A P = \begin{bmatrix} A \\ B \end{bmatrix} {}^B P}}$$

(4×1)
 (4×4)
 (4×1)

Example



Homogeneous Transform

$${}^A_B T = \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 0 & -1 & 3 \\ 0 & 1 & 0 & 1 \\ 0 & 0 & 0 & 1 \end{bmatrix} \quad {}^B P = \begin{bmatrix} 0 \\ 1 \\ 1 \\ 1 \end{bmatrix}$$

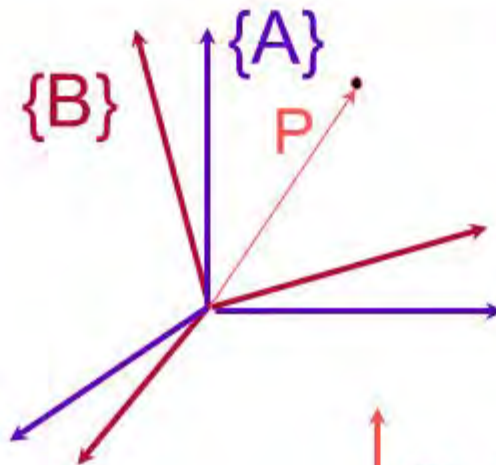
$${}^A P = {}^A_B T \cdot {}^B P \Rightarrow {}^A P = \begin{bmatrix} 0 \\ 2 \\ 2 \\ 1 \end{bmatrix}$$

Operators

Mapping: changing descriptions from frame to frame

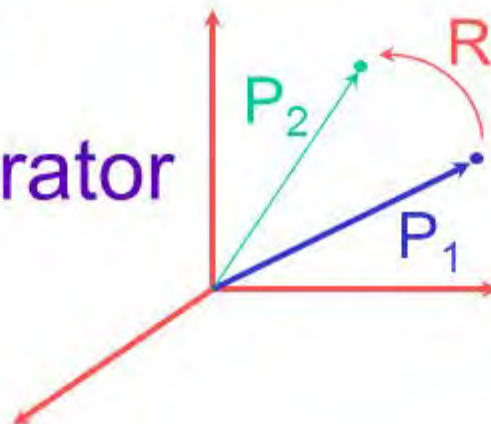
Operators: moving points (within the same frame)

Mapping



$${}^A P = {}^A_B R {}^B P$$

Rotational Operator



$$R: P_1 \longrightarrow P_2$$

$$P_2 = R P_1$$

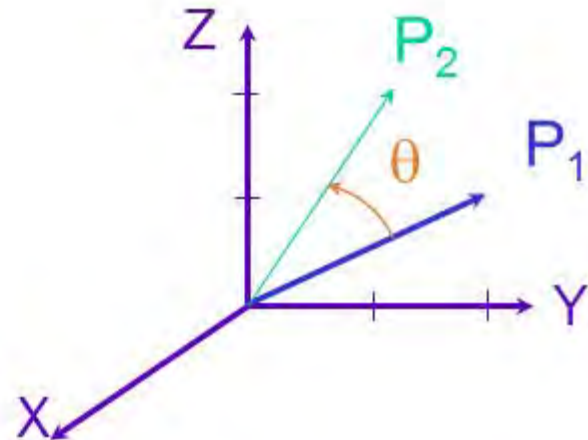
Rotational Operators

$$R_K(\theta): P_1 \longrightarrow P_2$$

$$P_2 = R_K(\theta) P_1$$

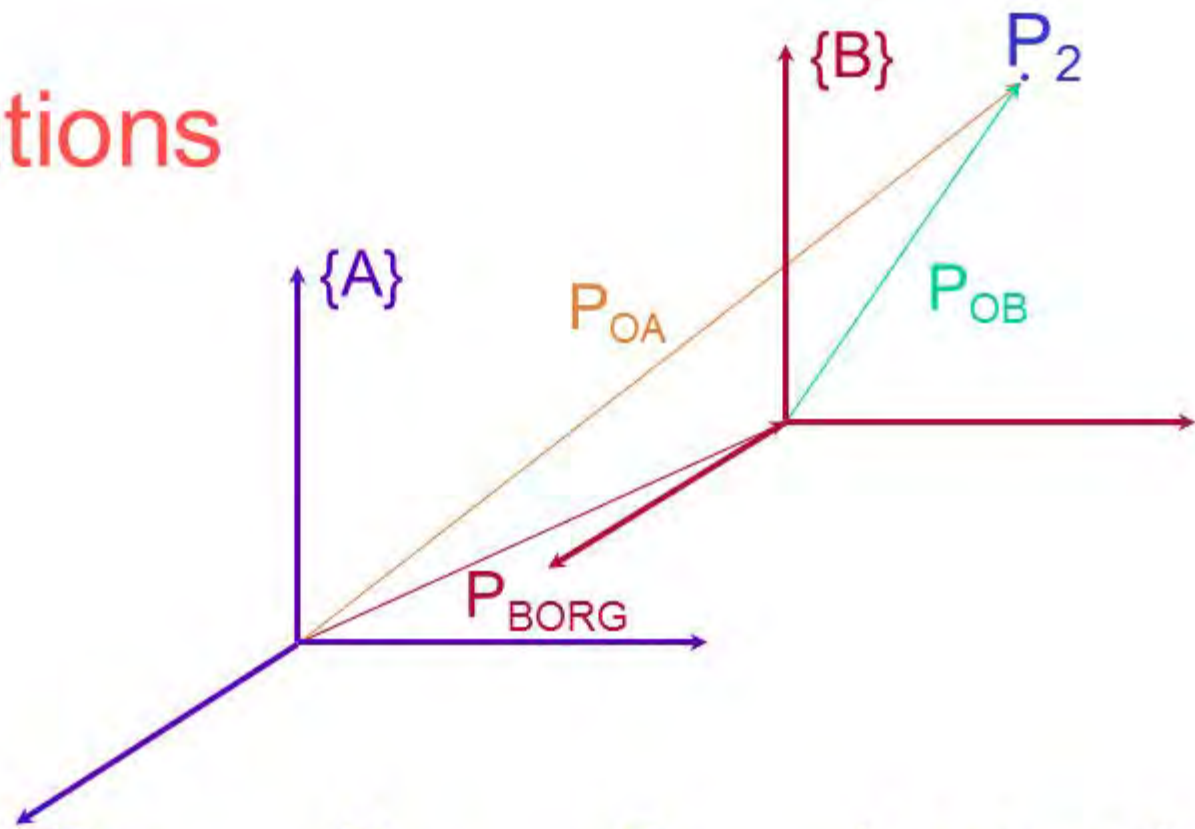
Example

$$R_X(\theta) = \begin{bmatrix} 1 & 0 & 0 \\ 0 & \cos \theta & -\sin \theta \\ 0 & \sin \theta & \cos \theta \end{bmatrix}$$



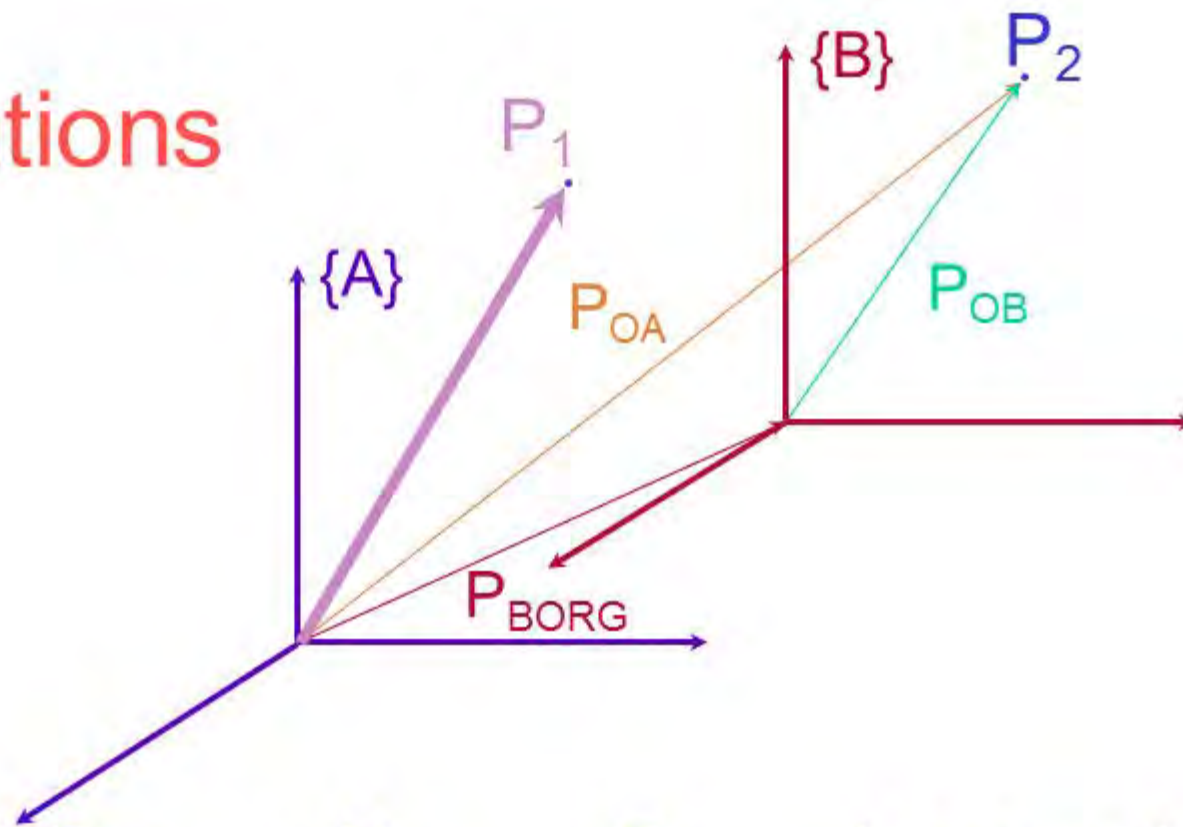
$$P_2 = R_X(\theta)P_1 = \begin{bmatrix} 1 & 0 & 0 \\ 0 & 0.8 & -0.6 \\ 0 & 0.6 & 0.8 \end{bmatrix} \begin{bmatrix} 0 \\ 2 \\ 1 \end{bmatrix} = \begin{bmatrix} 0 \\ 1 \\ 2 \end{bmatrix}$$

Translations



Mapping: $P_{BORG} : P_{OB} \longrightarrow P_{OA}$ (same point)
2 diff. vectors
$$P_{OA} = P_{OB} + P_{BORG}$$

Translations

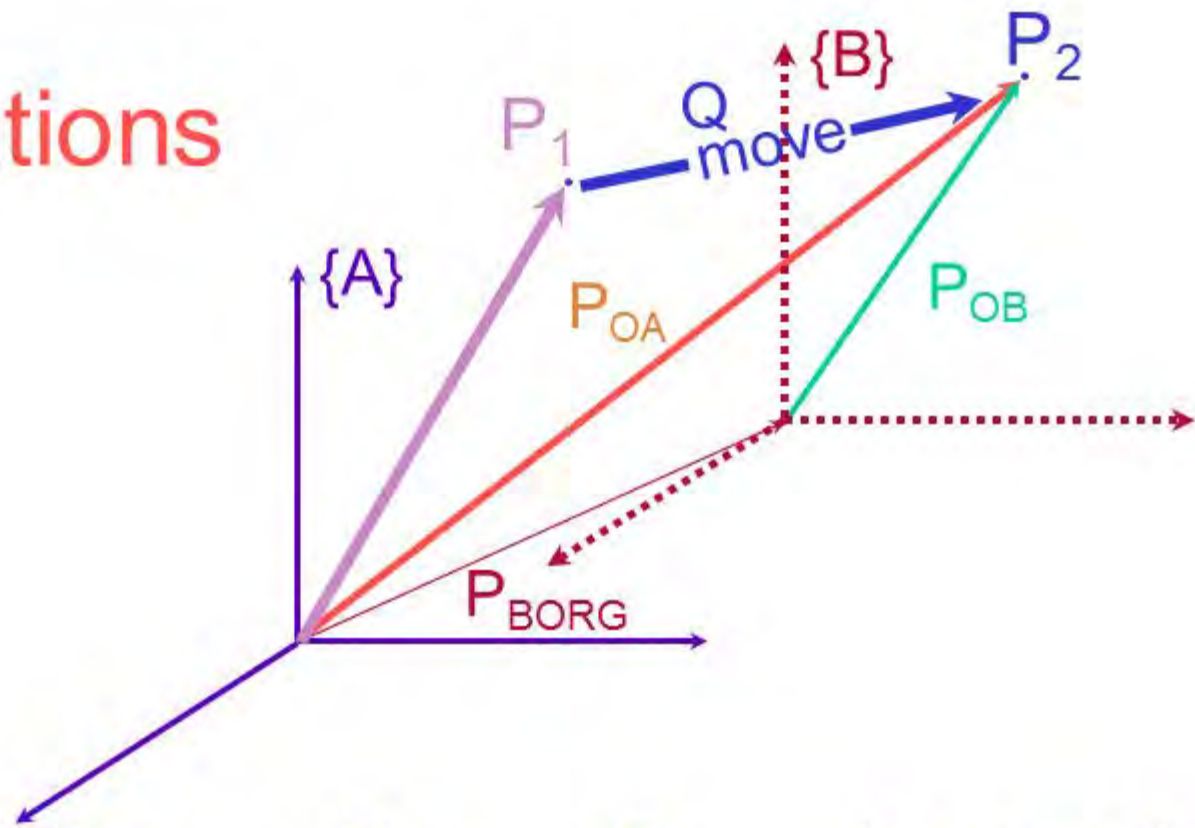


Mapping: $P_{BORG} : P_{OB} \longrightarrow P_{OA}$ (same point)
2 diff. vectors

$$P_{OA} = P_{OB} + P_{BORG}$$

Translational Operator:

Translations



Mapping: $P_{\text{BORG}} : P_{\text{OB}} \longrightarrow P_{\text{OA}}$ (same point)
2 diff. vectors

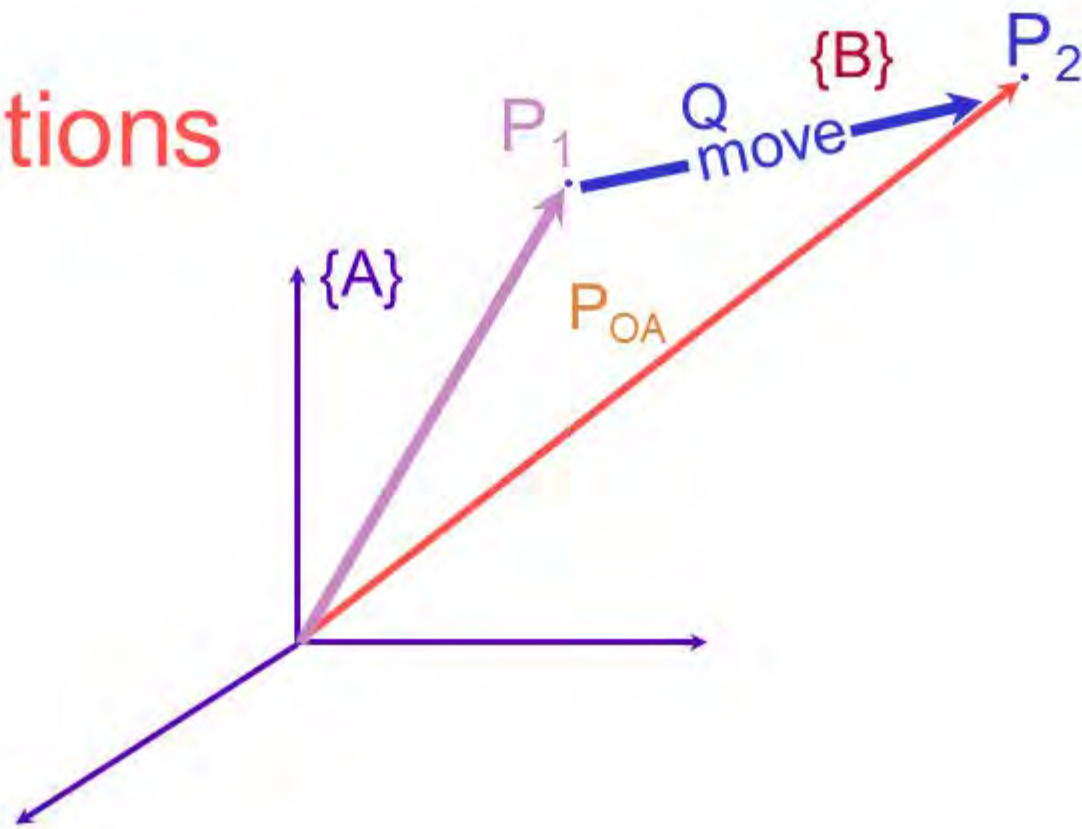
$$P_{\text{OA}} = P_{\text{OB}} + P_{\text{BORG}}$$

Translational Operator:

$Q : P_1 \longrightarrow P_2$ (2 points, 2 diff vectors)

$$P_2 = P_1 + Q$$

Translations



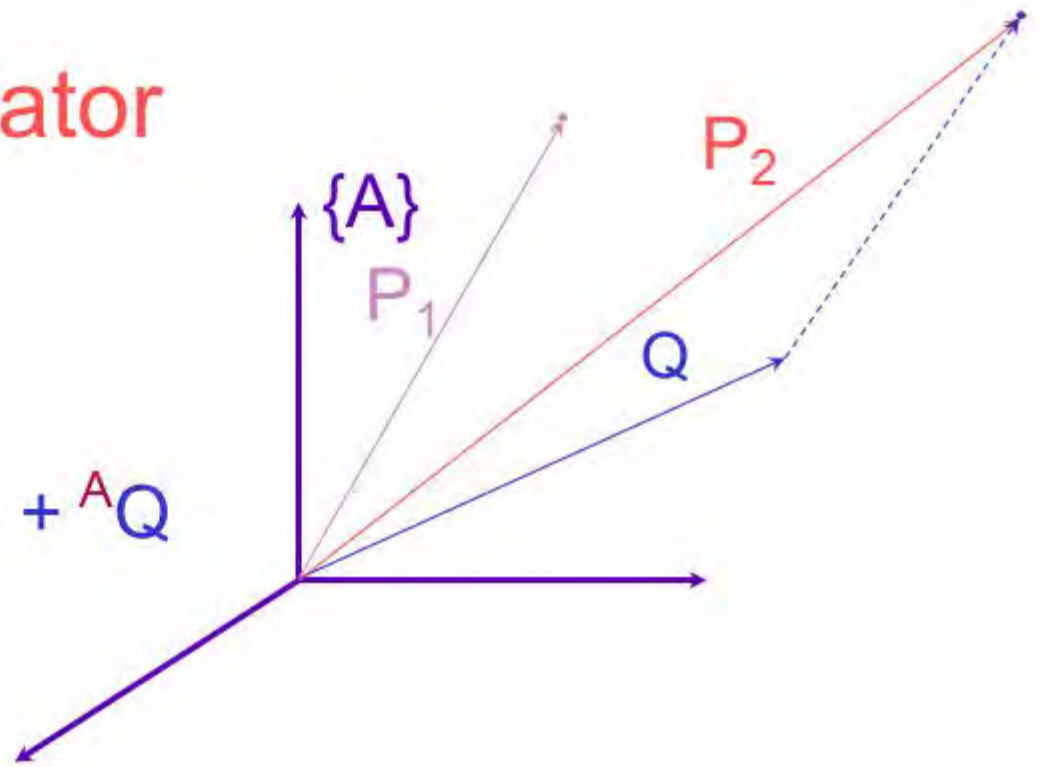
Translational Operator:

$Q : P_1 \longrightarrow P_2$ (2 points, 2 diff vectors)

$$P_2 = P_1 + Q$$

Translation Operator

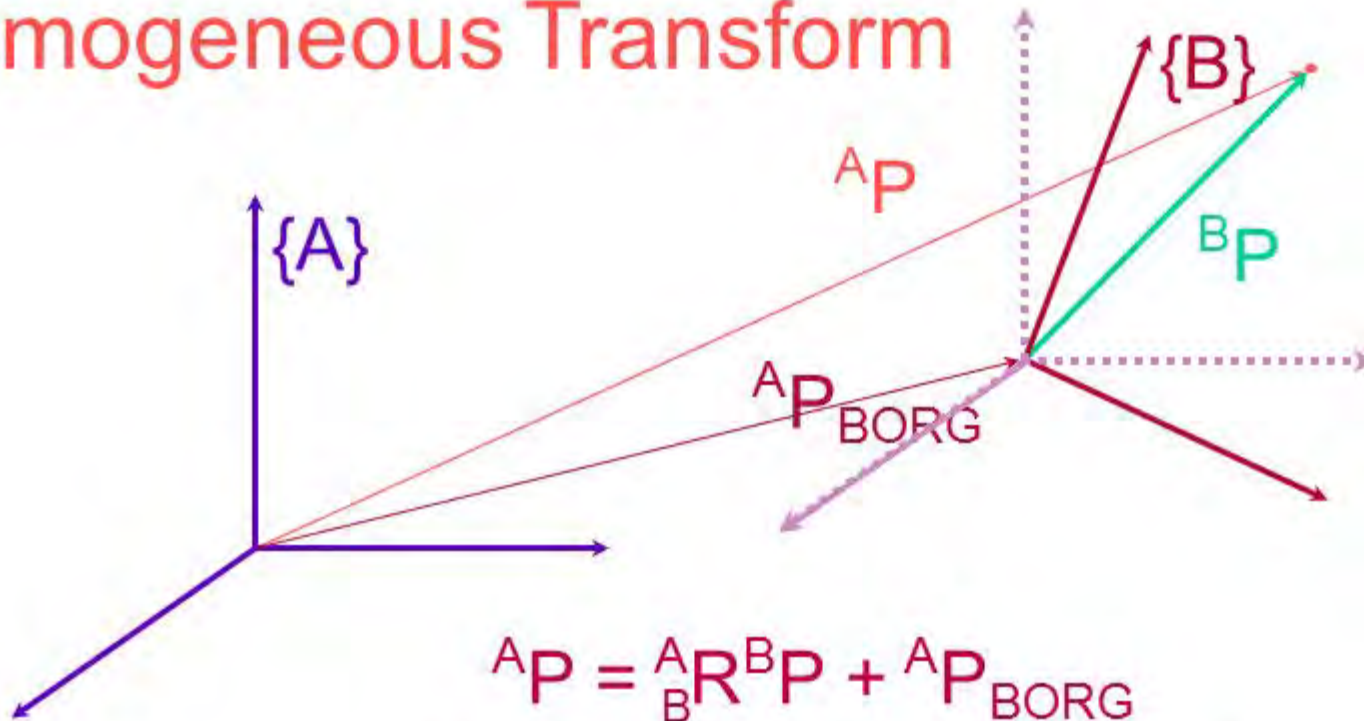
Operator: ${}^A P_2 = {}^A P_1 + {}^A Q$



Homogeneous Transform:

$$D_Q = \begin{bmatrix} 1 & 0 & 0 & q_x \\ 0 & 1 & 0 & q_y \\ 0 & 0 & 1 & q_z \\ 0 & 0 & 0 & 1 \end{bmatrix} \Rightarrow {}^A P_2 = {}^A D_Q {}^A P_1$$

Homogeneous Transform



$${}^A P = {}^A_B R^B P + {}^A P_{BORG}$$

$$\begin{bmatrix} {}^A P \\ 1 \end{bmatrix} = \begin{bmatrix} {}^A_B R & | & {}^A P_{BORG} \\ \hline 0 & 0 & 0 & | & 1 \end{bmatrix} \begin{bmatrix} {}^B P \\ 1 \end{bmatrix}$$

$$\underline{\underline{{}^A P = \begin{bmatrix} A \\ B \end{bmatrix}^T P}}$$

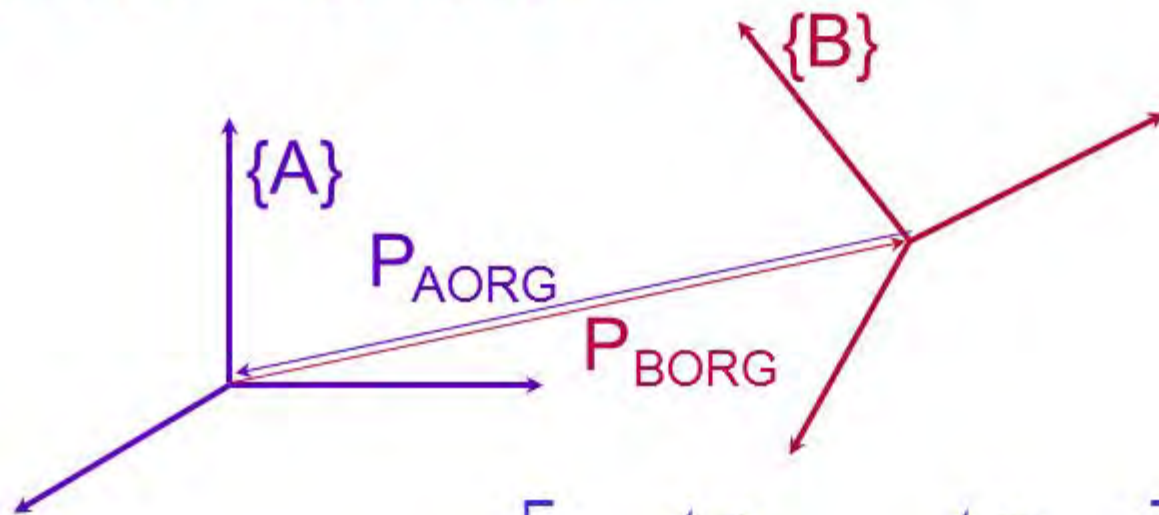
(4×1)
 (4×4)
 (4×1)

General Operators

$$P_2 = \left(\begin{array}{ccc|c} R_K(\theta) & & & Q \\ \hline 0 & 0 & 0 & 1 \end{array} \right) P_1$$

$$P_2 = T P_1$$

Inverse Transform



$${}^A T_B = \begin{bmatrix} {}^A R_B & {}^A P_{Borg} \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$R^{-1} = R^T \quad (T^{-1} \neq T^T)$$

$${}^A T_B^{-1} = {}^B T_A = \begin{bmatrix} {}^A R_B^T & -{}^A R_B^T \cdot {}^A P_{Borg} \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

${}^B P_{AORG}$

Announcement: Computer Forum Career Fair

Wednesday, Jan. 15

Computer Forum Career Fair

11am - 4pm

Lawn behind Gates & Mudd Chemistry Buildings

a9	Cisco	IBM	Quantcast	Texas Instruments
Accel Partners	Counsyl	Intuit	Rocket Fuel	Tower Research
Adap.tv	Coursera	IXL	Salesforce	Turn
Addepar	Cutler Group	Juniper Networks	Samsung	Twitter
Adobe	D.E. Shaw	Lab 126	SAP Americas	Two Sigma
Amazon Web Services	Dropbox	Lenovo	Sequoia Capital	VMware
Andreessen Horowitz	eBay	Lightspeed	Serendipity	WhatsApp
Apple	EMC	LinkedIn	Shape Security	Workday
Apportable	Ericsson	LiveRamp	Snapchat	Yahoo!
Arista Networks	Evernote	Marin Software	Splunk	Yelp
Bloomberg	Facebook	Microsoft	Spokeo	Zazzle
Box	GE	Mobile Iron	Square	Zynga
Brightroll	Google	Nissan	Storm8	
Broadcom	Groupon	Nvidia	Symantec	
Cash Dynamics	HealthTap	Oracle	Tableau Software	
C3 Energy	Hewlett Packard	Palantir Technologies	Technicolor	
Chopper Trading		Pocket Gems	Teradata	

Kinematics

Movie Segment

LittleDog

Learning Locomotion with LittleDog

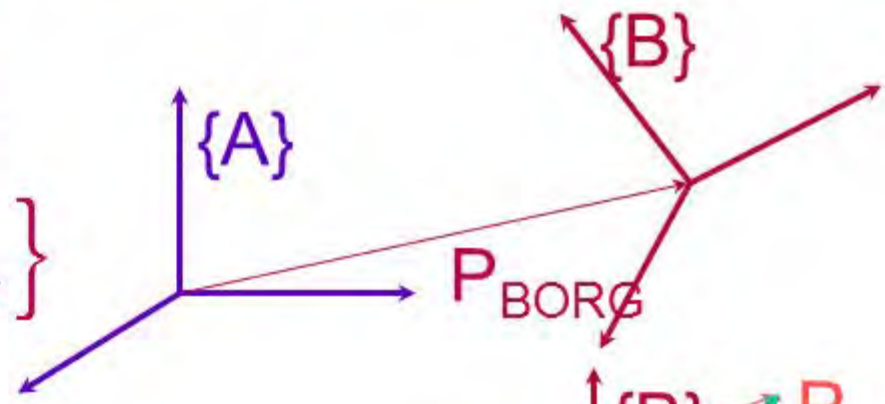
<http://www-clmc.usc.edu>

Mrinal Kalakrishnan, Jonas Buchli,
Peter Pastor, Michael Mistry, and
Stefan Schaal

Homogeneous Transform Interpretations

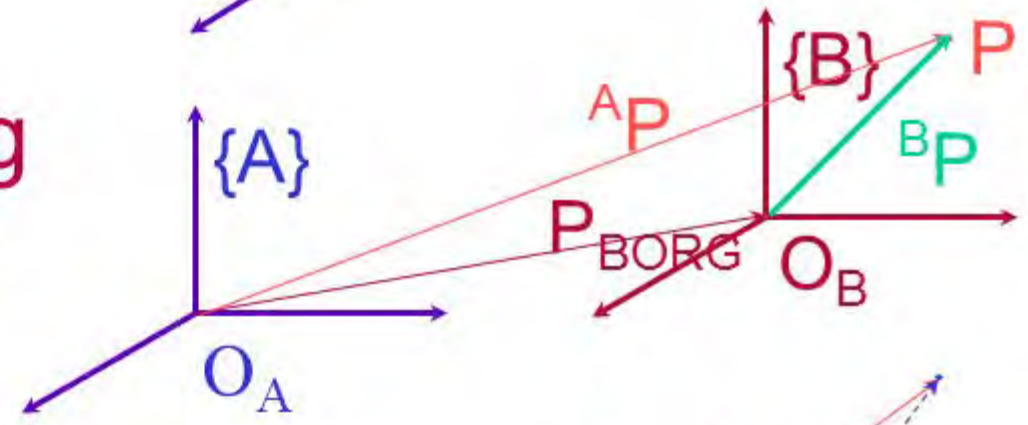
Description of a frame

$${}^A_B T: \{B\} = \left\{ {}^A_B R \quad {}^A P_{Borg} \right\}$$



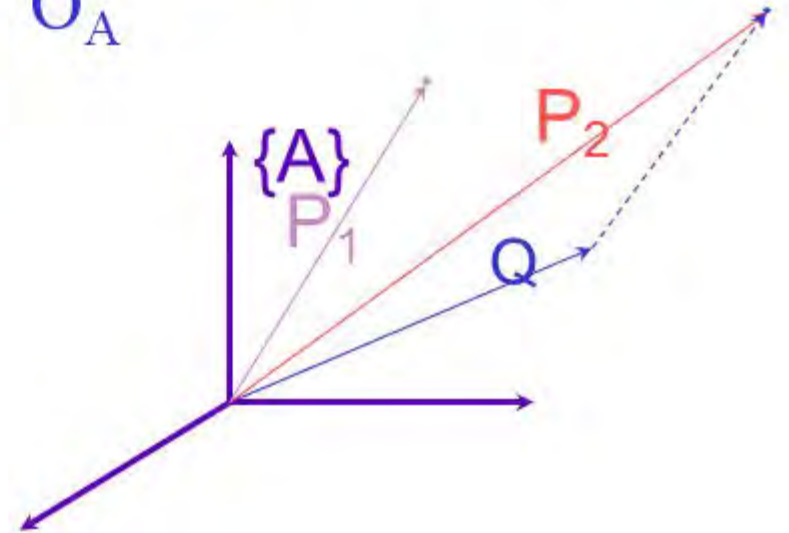
Transform mapping

$${}^A_B T: {}^B P \rightarrow {}^A P$$

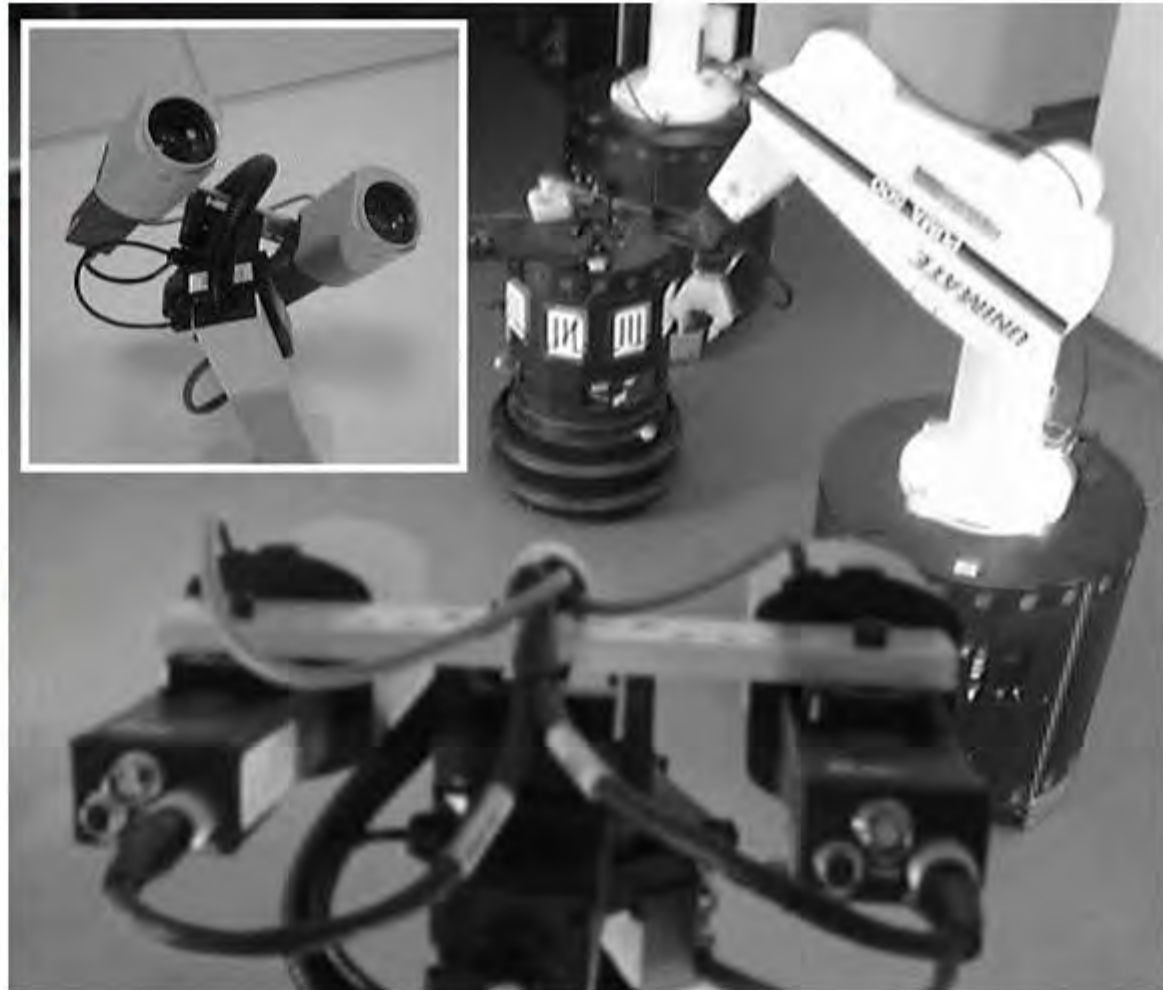
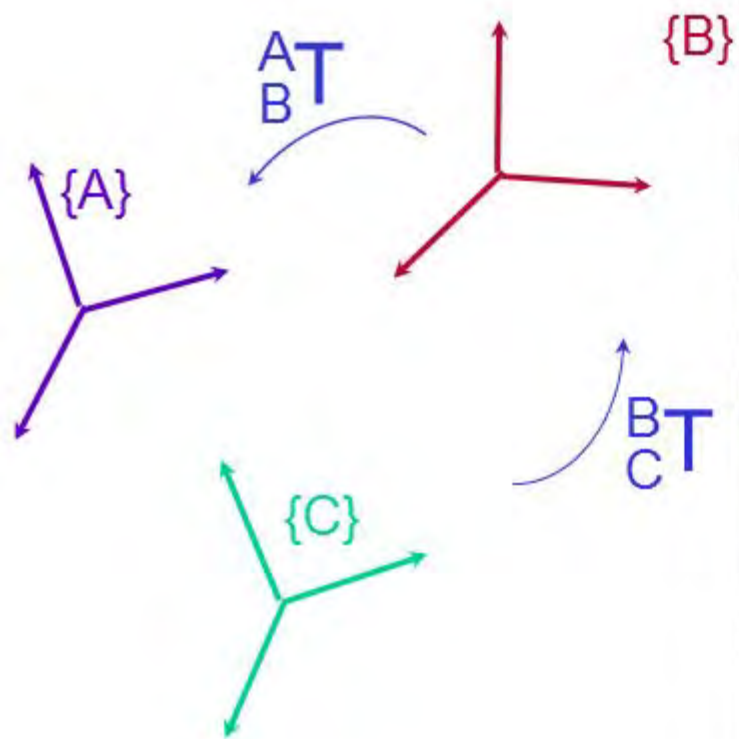


Transform operator

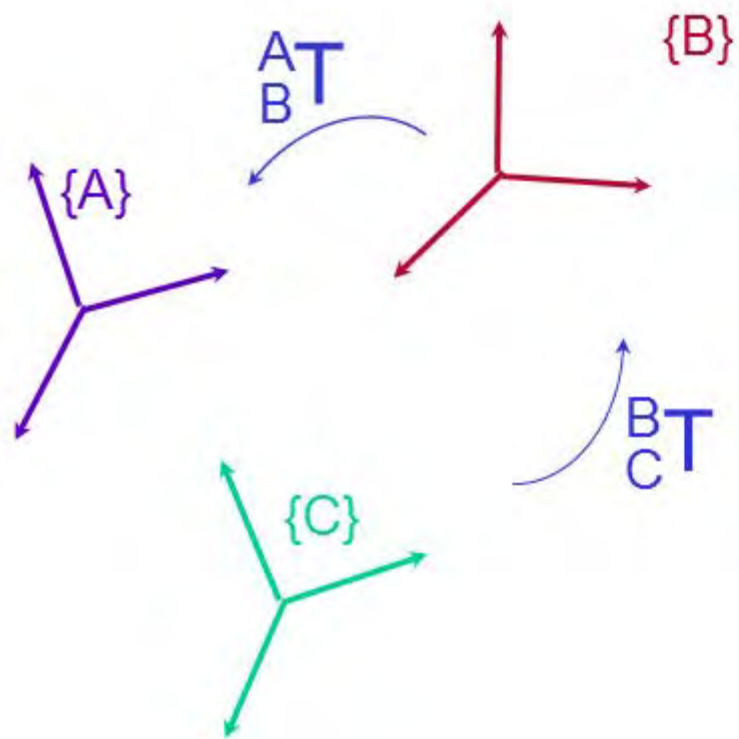
$$T: P_1 \rightarrow P_2$$



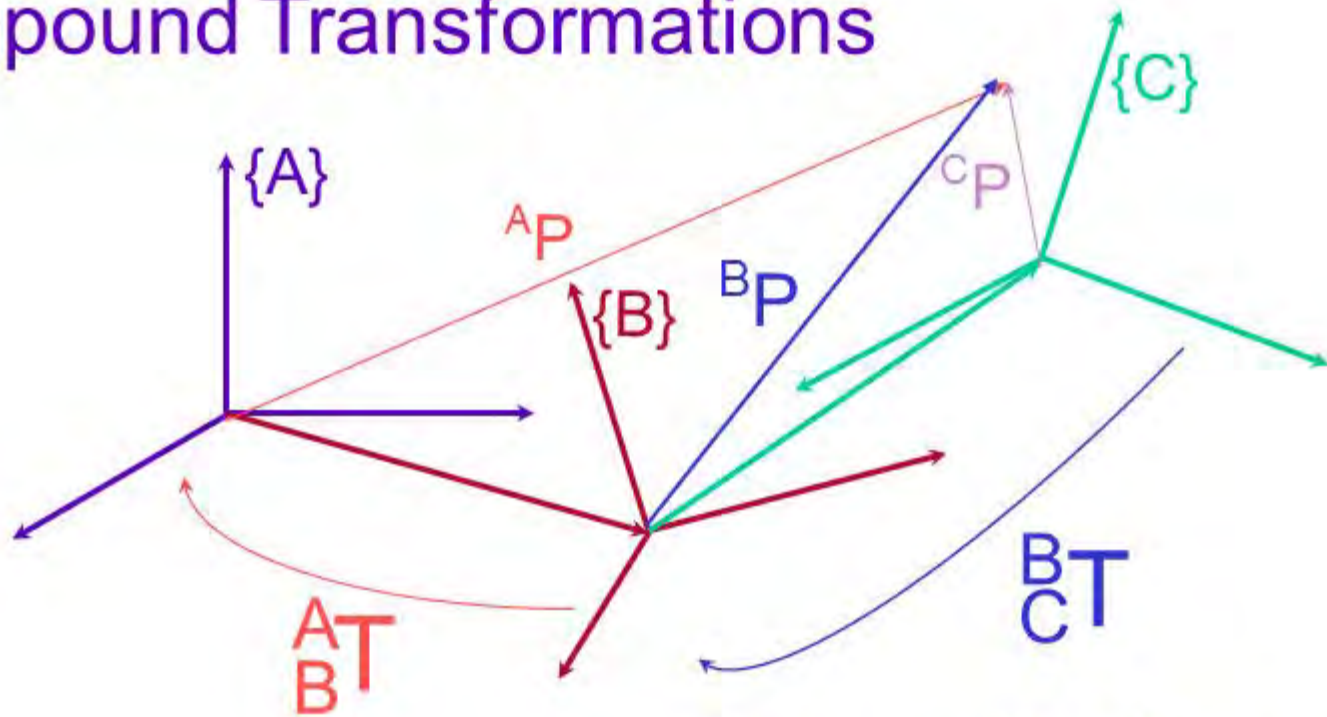
Transform Equation



Transform Equation



Compound Transformations



$$B_P = B_C^T C_P$$

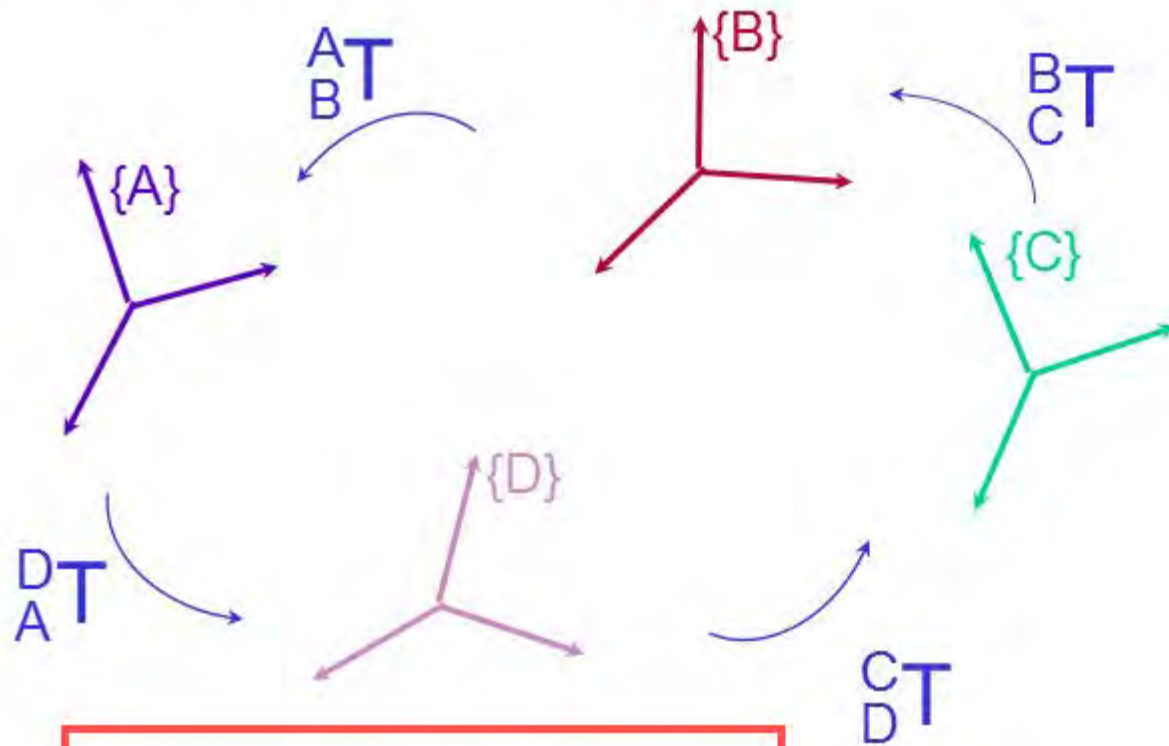
$$A_P = A_B^T B_P$$

$$A_P = A_B^T B_C^T C_P \quad \Rightarrow \quad A_C^T = A_B^T B_C^T$$

$${}^A T_C = {}^A T_B {}^B T_C$$

$${}^A T_C = \begin{bmatrix} {}^A R_B {}^B R_C & {}^A R_B {}^B P_{Corg} + {}^A P_{Borg} \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

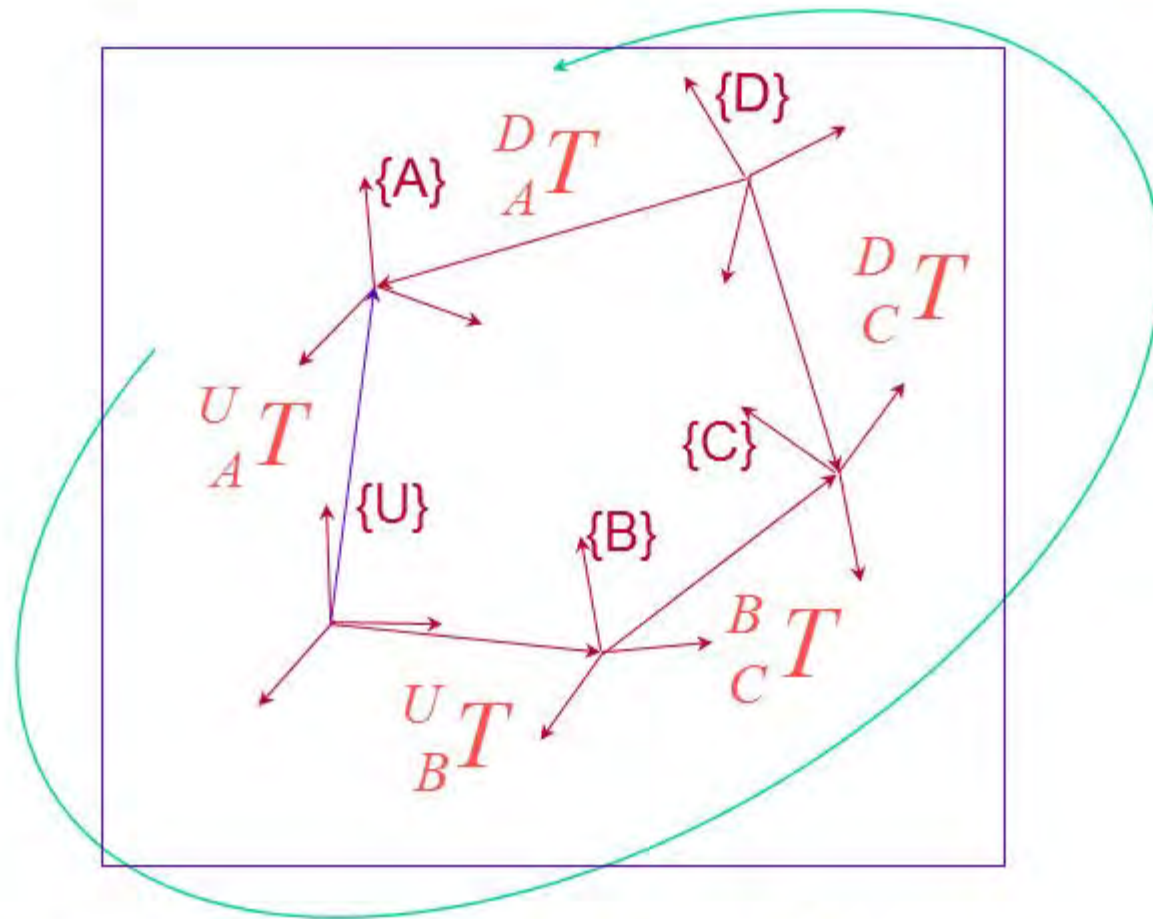
Transform Equation



$$\begin{bmatrix} A^T & B^T & C^T & D^T \\ B^T & C^T & D^T & A^T \end{bmatrix} = I$$



$$\begin{bmatrix} B^T \\ A^T \end{bmatrix} = \begin{bmatrix} B^T & C^T & D^T \\ C^T & D^T & A^T \end{bmatrix}$$



$$D_A T^{-1} \cdot D_C T \cdot B_C T^{-1} \cdot U_B T^{-1} \cdot U_A T \equiv I$$

$$U_A T = U_B T \cdot B_C T \cdot D_C T^{-1} \cdot D_A T$$

Spatial Descriptions

- Task Description
- Transformations
- Representations

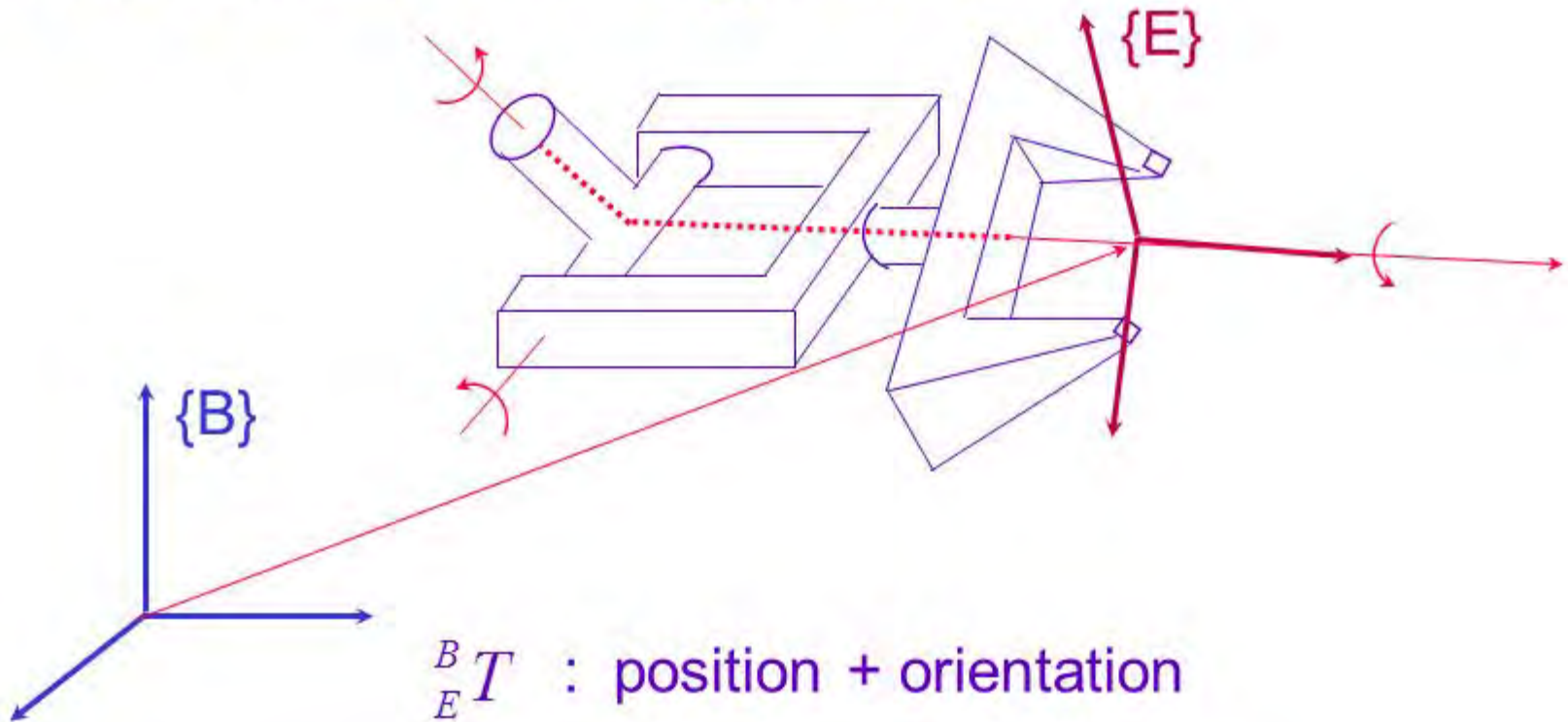


Spatial Descriptions

- Task Description
- Transformations
- Representations



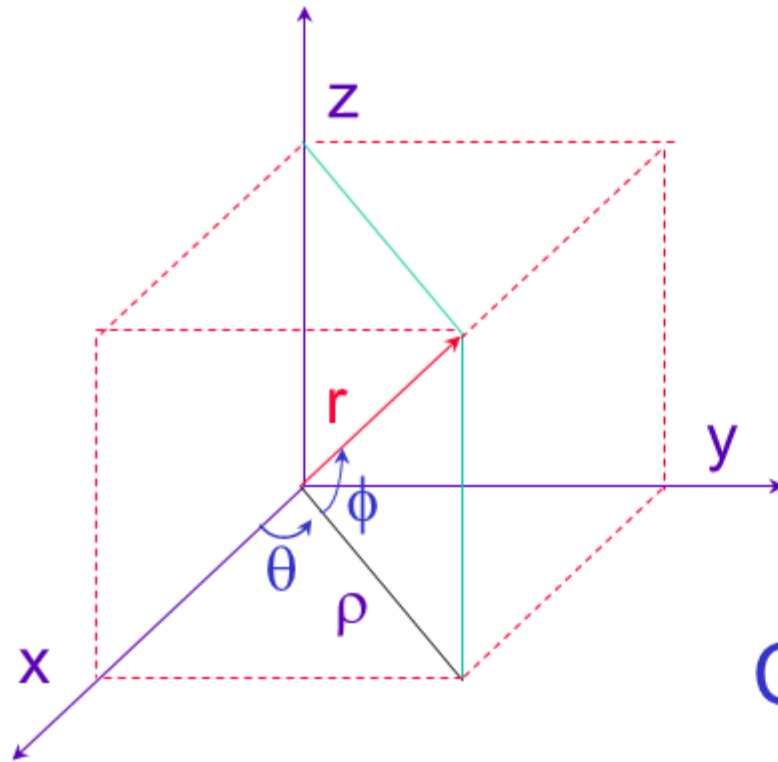
End-Effector Configuration



End-Effector Configuration Parameters

$$X = \begin{bmatrix} X_P \\ X_R \end{bmatrix} \begin{array}{l} \leftarrow \text{position} \\ \leftarrow \text{orientation} \end{array}$$

Position Representations



Cartesian: (x, y, z)

Cylindrical: (ρ, θ, z)

Spherical: (r, θ, ϕ)

Rotation Representations

Rotation Matrix

$$R = \begin{bmatrix} r_{11} & r_{12} & r_{13} \\ r_{21} & r_{22} & r_{23} \\ r_{31} & r_{32} & r_{33} \end{bmatrix} = [\mathbf{r}_1 \quad \mathbf{r}_2 \quad \mathbf{r}_3]$$

Direction Cosines

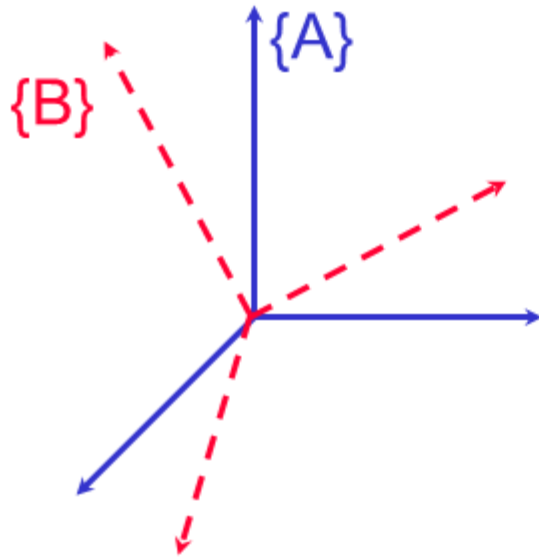
$$x_r = \begin{bmatrix} \mathbf{r}_1 \\ \mathbf{r}_2 \\ \mathbf{r}_3 \end{bmatrix}_{(9 \times 1)}$$

Constraints

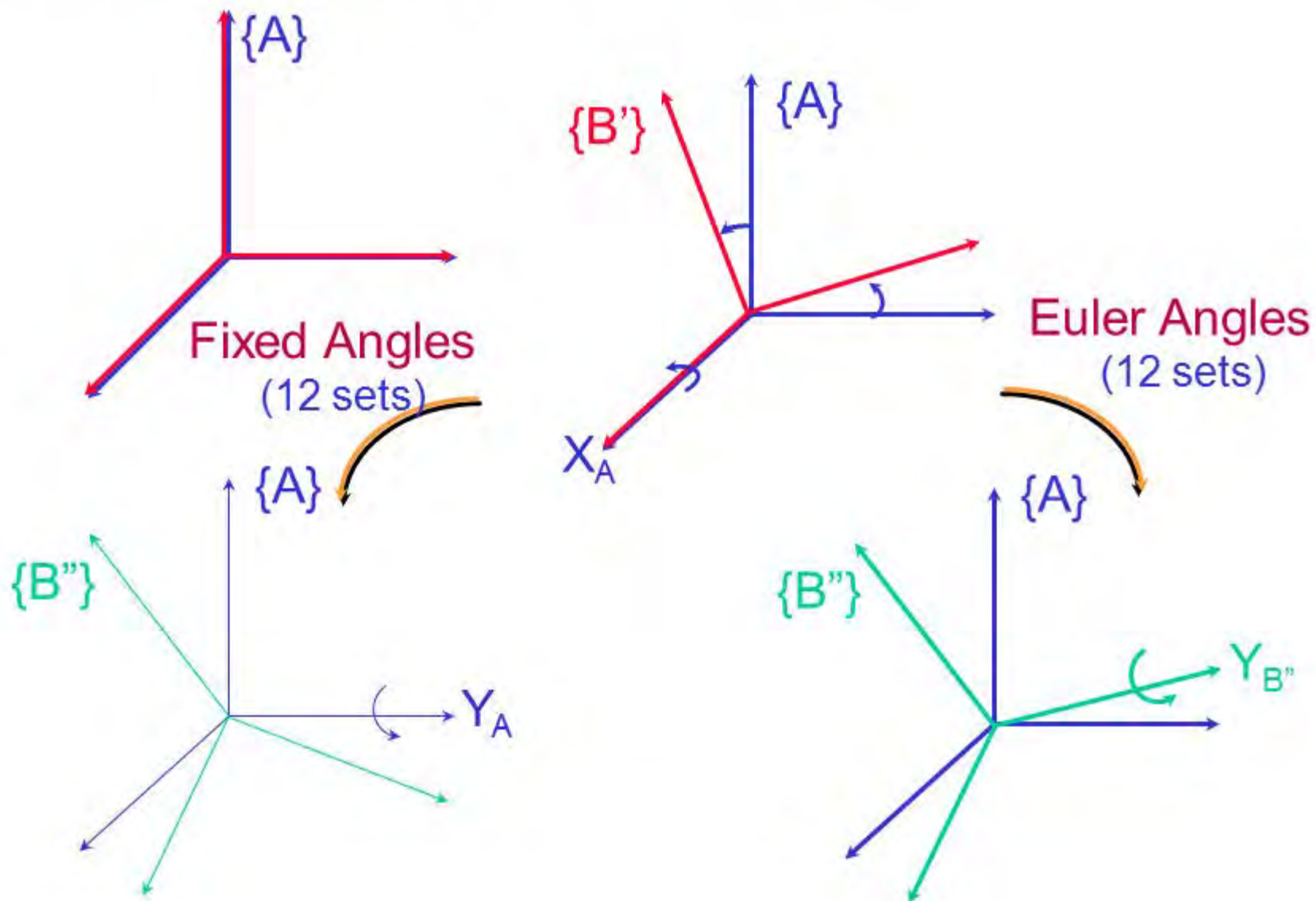
$$|\mathbf{r}_1| = |\mathbf{r}_2| = |\mathbf{r}_3| = 1$$

$$\mathbf{r}_1 \cdot \mathbf{r}_2 = \mathbf{r}_1 \cdot \mathbf{r}_3 = \mathbf{r}_2 \cdot \mathbf{r}_3 = 0$$

Three Angle Representations

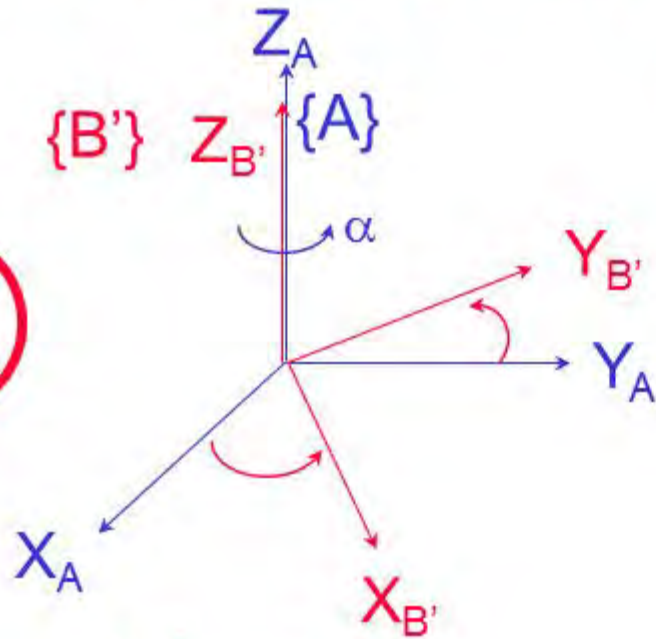


Three Angle Representations

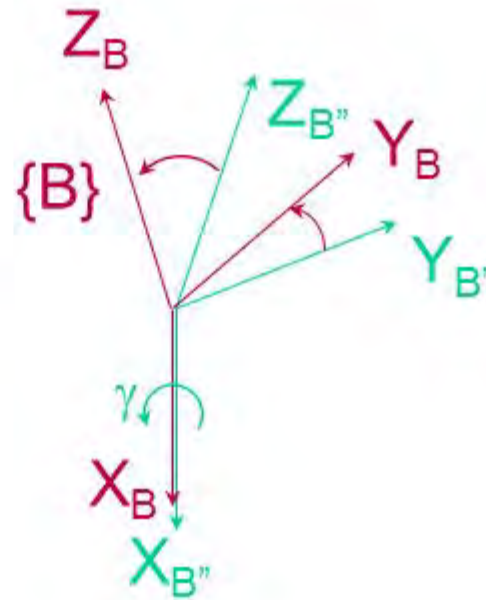
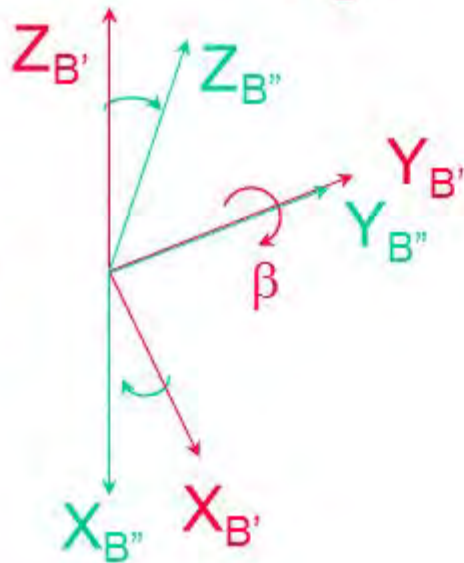


Euler Angles (Z-Y-X)

$${}^A_{B'} R$$



$${}^{B'}_{B''} R$$

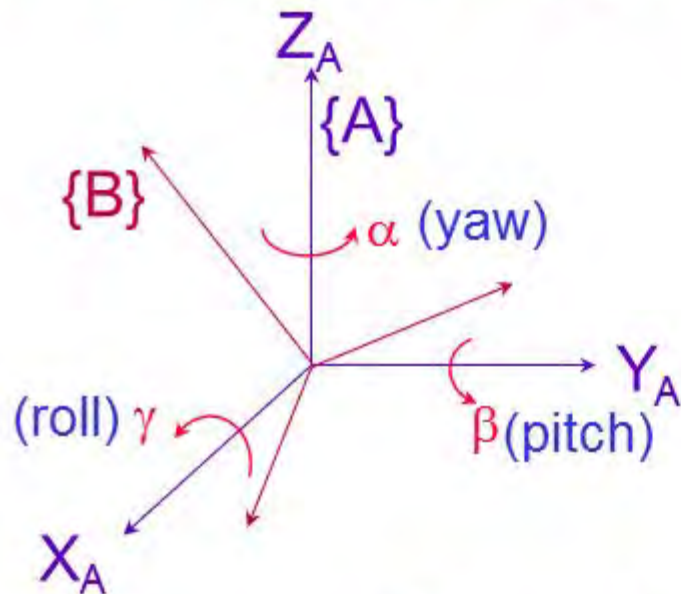


$${}^{B''}_B R$$

$${}^A_B R = {}^A_{B'} R \cdot {}^{B'}_{B''} R \cdot {}^{B''}_B R$$

$${}^A_B R = R_Z(\alpha) \cdot R_Y(\beta) \cdot R_X(\gamma)$$

X-Y-Z Fixed Angles



$$R_X(\gamma): v \rightarrow R_X(\gamma).v$$

$$R_Y(\beta): (R_X(\gamma).v) \rightarrow R_Y(\beta).(R_X(\gamma).v)$$

$$R_Z(\alpha): (R_Y(\beta).R_X(\gamma).v) \rightarrow R_Z(\alpha).(R_Y(\beta).R_X(\gamma).v)$$

$$\boxed{{}^A_B R = {}^A_B R_{XYZ}(\gamma, \beta, \alpha) = R_Z(\alpha).R_Y(\beta).R_X(\gamma)}$$

Z-Y-X Euler Angles

$${}^A_B R = R_{Z'}(\alpha) \cdot R_{Y'}(\beta) \cdot R_{X'}(\gamma)$$

$$\begin{bmatrix} c\alpha & -s\alpha & 0 \\ s\alpha & c\alpha & 0 \\ 0 & 0 & 1 \end{bmatrix} \cdot \begin{bmatrix} c\beta & 0 & s\beta \\ 0 & 1 & 0 \\ -s\beta & 0 & c\beta \end{bmatrix} \cdot \begin{bmatrix} 1 & 0 & 0 \\ 0 & c\gamma & -s\gamma \\ 0 & s\gamma & c\gamma \end{bmatrix}$$

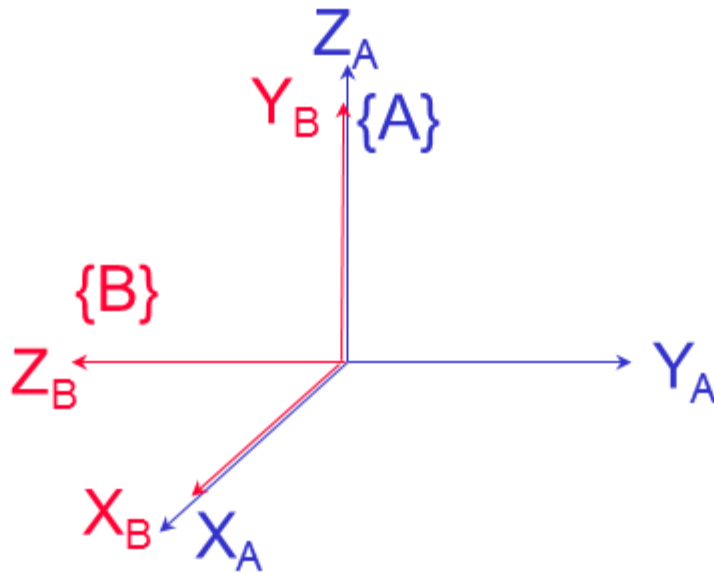
$${}^A_B R = {}^A_B R_{Z'Y'X'}(\alpha, \beta, \gamma) = \begin{bmatrix} c\alpha \cdot c\beta & X & X \\ s\alpha \cdot c\beta & X & X \\ -s\beta & c\beta \cdot s\gamma & c\beta \cdot c\gamma \end{bmatrix}$$

Z-Y-Z Euler Angles

$${}^A_B R = R_{Z'}(\alpha) \cdot R_{Y'}(\beta) \cdot R_{Z'}(\gamma)$$

$${}^A_B R = {}^A_B R_{Z'Y'Z'}(\alpha, \beta, \gamma) = \begin{bmatrix} X & X & c\alpha \cdot s\beta \\ X & X & s\alpha \cdot s\beta \\ -s\beta \cdot c\gamma & s\beta \cdot s\gamma & c\beta \end{bmatrix}$$

Example



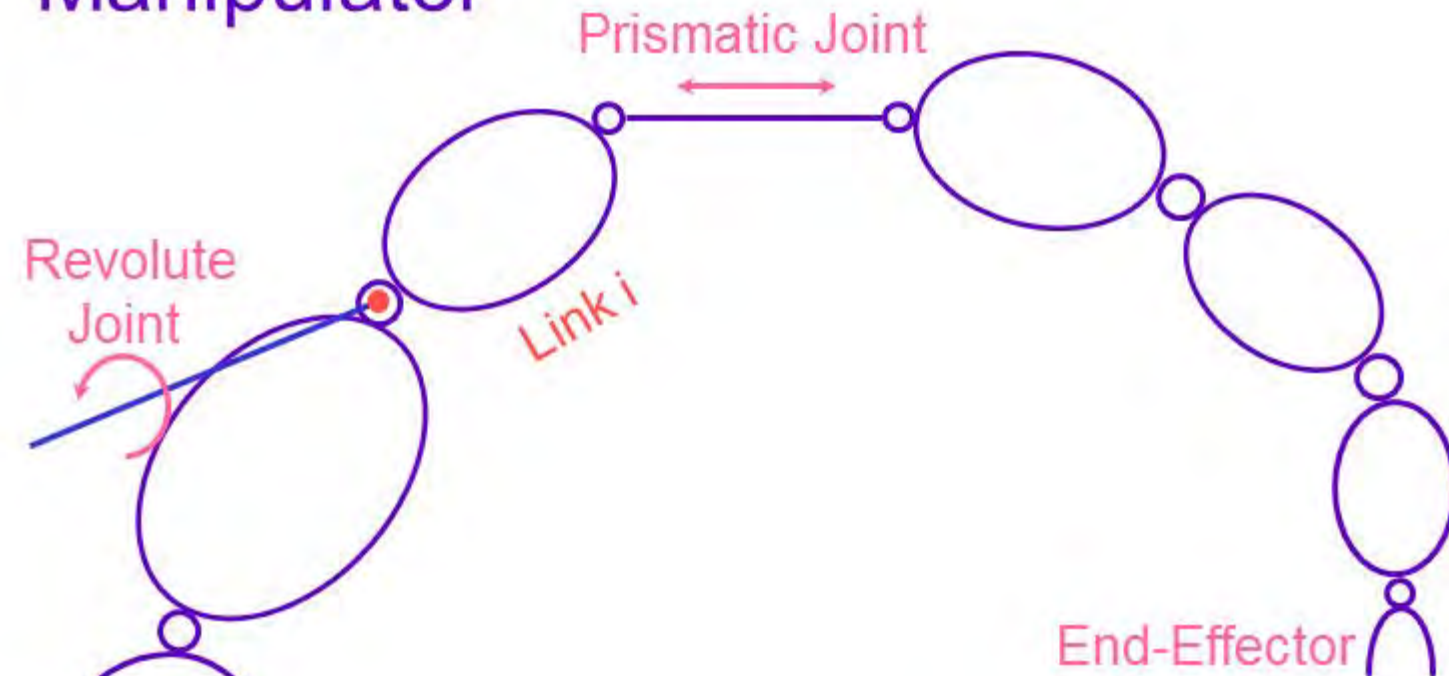
$$R_{Z'Y'X'}(\alpha, \beta, \gamma):$$

$$\alpha = 0$$

$$\beta = 0$$

$$\gamma = 90^\circ$$

Manipulator



- Links:** n moving link
1 fixed link
- Joints:** Revolute (1 DOF)
Prismatic (1 DOF)

Fixed & Euler Angles

X-Y-Z Fixed Angles

$$R_{XYZ}(\gamma, \beta, \alpha) = R_Z(\alpha) \cdot R_Y(\beta) \cdot R_X(\gamma)$$

Z-Y-X Euler Angles

$$R_{Z'Y'X'}(\alpha, \beta, \gamma) = R_Z(\alpha) \cdot R_Y(\beta) \cdot R_X(\gamma)$$

$$R_{Z'Y'X'}(\alpha, \beta, \gamma) = R_{XYZ}(\gamma, \beta, \alpha)$$

Inverse Problem

Given ${}^A_B R$ find (α, β, γ)

$${}^A_B R = \begin{bmatrix} r_{11} & r_{12} & r_{13} \\ r_{21} & r_{22} & r_{23} \\ r_{31} & r_{32} & r_{33} \end{bmatrix} = \begin{bmatrix} c\alpha \cdot c\beta & c\alpha \cdot s\beta \cdot s\gamma - s\alpha \cdot c\gamma & c\alpha \cdot s\beta \cdot c\gamma + s\alpha \cdot s\gamma \\ s\alpha \cdot c\beta & s\alpha \cdot s\beta \cdot s\gamma + c\alpha \cdot c\gamma & s\alpha \cdot s\beta \cdot c\gamma - c\alpha \cdot s\gamma \\ -s\beta & c\beta \cdot s\gamma & c\beta \cdot c\gamma \end{bmatrix} \quad \begin{matrix} \curvearrowright \\ R_{Z'Y'X'} \end{matrix}$$

$$\left. \begin{array}{l} \cos \beta = c\beta = \sqrt{r_{11}^2 + r_{21}^2} \\ \sin \beta = s\beta = -r_{31} \end{array} \right\} \rightarrow \beta = \text{Atan2}(-r_{31}, \sqrt{r_{11}^2 + r_{21}^2})$$

if $c\beta = 0$ ($\beta = \pm 90^\circ$) \Rightarrow Singularity of the representation

\Rightarrow Only $(\alpha + \gamma)$ or $(\alpha - \gamma)$ is defined

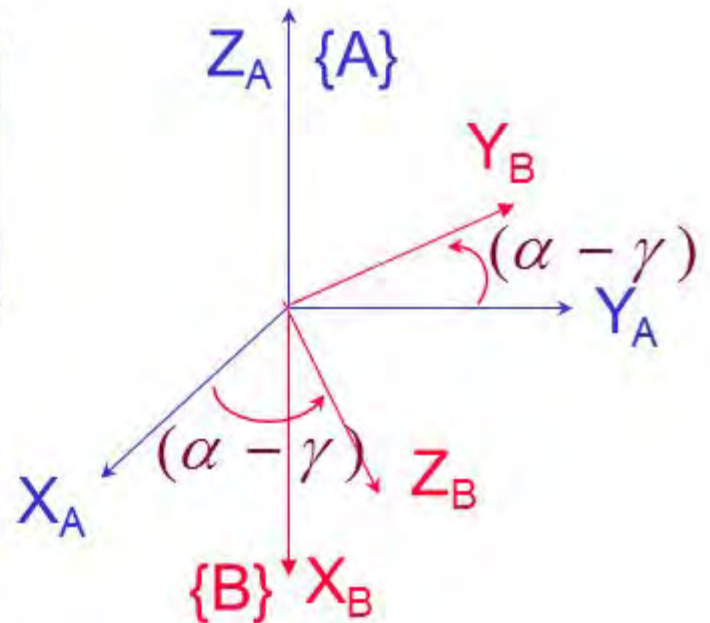
Singularities - Example ($R_{Z'Y'X'}$)

$$\underline{c\beta = 0, s\beta = +1}$$

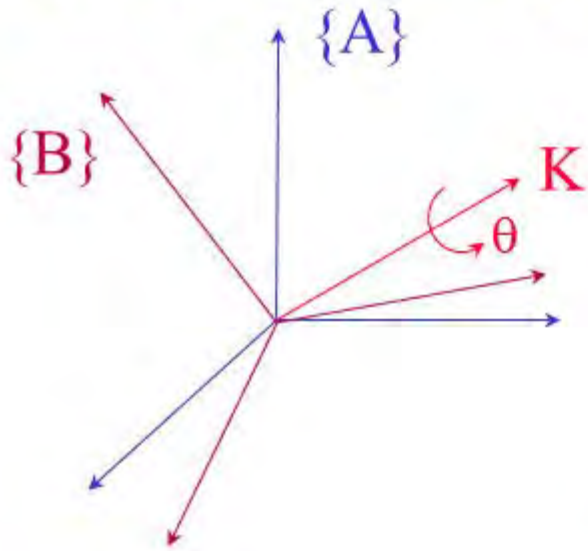
$${}^A_B R = \begin{pmatrix} 0 & -s(\alpha - \gamma) & c(\alpha - \gamma) \\ 0 & c(\alpha - \gamma) & s(\alpha - \gamma) \\ -1 & 0 & 0 \end{pmatrix}$$

$$\underline{c\beta = 0, s\beta = -1}$$

$${}^A_B R = \begin{pmatrix} 0 & -s(\alpha + \gamma) & -c(\alpha + \gamma) \\ 0 & c(\alpha + \gamma) & -s(\alpha + \gamma) \\ 1 & 0 & 0 \end{pmatrix}$$



Equivalent angle-axis representation, $R_K(\theta)$



$$X_r = \theta \cdot K = \begin{bmatrix} \theta \cdot k_x \\ \theta \cdot k_y \\ \theta \cdot k_z \end{bmatrix}$$

$$R_K(\theta) = \begin{bmatrix} k_x \cdot k_x \cdot v\theta + c\theta & k_x \cdot k_y \cdot v\theta - k_z \cdot s\theta & k_x \cdot k_z \cdot v\theta + k_y \cdot s\theta \\ k_x \cdot k_y \cdot v\theta + k_z \cdot s\theta & k_y \cdot k_y \cdot v\theta + c\theta & k_y \cdot k_z \cdot v\theta - k_x \cdot s\theta \\ k_x \cdot k_z \cdot v\theta - k_y \cdot s\theta & k_y \cdot k_z \cdot v\theta + k_x \cdot s\theta & k_z \cdot k_z \cdot v\theta + c\theta \end{bmatrix}$$

with $v\theta = 1 - c\theta$

$$R_K(\theta) = \begin{bmatrix} r_{11} & r_{12} & r_{13} \\ r_{21} & r_{22} & r_{23} \\ r_{31} & r_{32} & r_{33} \end{bmatrix}$$

$$\theta = \text{Ar cos} \left(\frac{r_{11} + r_{22} + r_{33} - 1}{2} \right)$$

$${}^A K = \frac{1}{2 \cdot \sin \theta} \begin{bmatrix} r_{32} - r_{23} \\ r_{13} - r_{31} \\ r_{21} - r_{12} \end{bmatrix}, \quad \text{singularity for } \sin \theta = 0$$

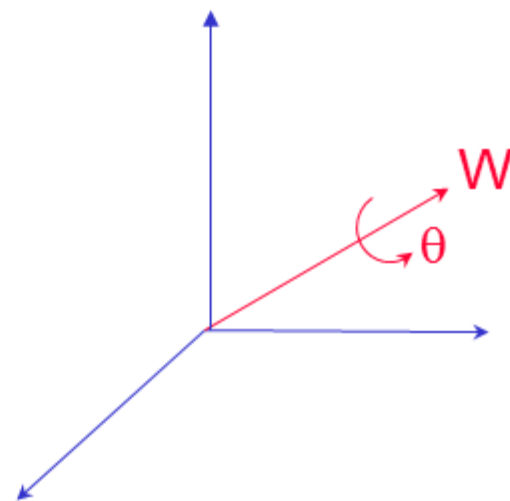
Euler Parameters

$$\varepsilon_1 = W_x \cdot \sin \frac{\theta}{2}$$

$$\varepsilon_2 = W_y \cdot \sin \frac{\theta}{2}$$

$$\varepsilon_3 = W_z \cdot \sin \frac{\theta}{2}$$

$$\varepsilon_4 = \cos \frac{\theta}{2}$$



Normality Condition

$$|W| = 1, \quad \varepsilon_1^2 + \varepsilon_2^2 + \varepsilon_3^2 + \varepsilon_4^2 = 1$$

ε : point on a unit hypersphere
in four-dimensional space

Inverse Problem

Given ${}^A_B R$ find ε

$$\begin{bmatrix} r_{11} & r_{12} & r_{13} \\ r_{21} & r_{22} & r_{23} \\ r_{31} & r_{32} & r_{33} \end{bmatrix} \equiv \begin{bmatrix} 1 - 2\varepsilon_2^2 - 2\varepsilon_3^2 & 2(\varepsilon_1\varepsilon_2 - \varepsilon_3\varepsilon_4) & 2(\varepsilon_1\varepsilon_3 + \varepsilon_2\varepsilon_4) \\ 2(\varepsilon_1\varepsilon_2 + \varepsilon_3\varepsilon_4) & 1 - 2\varepsilon_1^2 - 2\varepsilon_3^2 & 2(\varepsilon_2\varepsilon_3 - \varepsilon_1\varepsilon_4) \\ 2(\varepsilon_1\varepsilon_3 - \varepsilon_2\varepsilon_4) & 2(\varepsilon_2\varepsilon_3 + \varepsilon_1\varepsilon_4) & 1 - 2\varepsilon_1^2 - 2\varepsilon_2^2 \end{bmatrix}$$

$$r_{11} + r_{22} + r_{33} = 3 - 4(\varepsilon_1^2 + \varepsilon_2^2 + \varepsilon_3^2) \\ (1 - \varepsilon_4^2)$$

$$\varepsilon_4 = \frac{1}{2} \sqrt{1 + r_{11} + r_{22} + r_{33}}$$

$$\varepsilon_1 = \frac{r_{32} - r_{23}}{4\varepsilon_4}, \quad \varepsilon_2 = \frac{r_{13} - r_{31}}{4\varepsilon_4}, \quad \varepsilon_3 = \frac{r_{21} - r_{12}}{4\varepsilon_4}$$

$$\underline{\underline{\varepsilon_4 = 0?}}$$

Lemma For all rotations one of the Euler Parameters is greater than or equal to 1/2

$$\left(\sum_1^4 \varepsilon_i^2 = 1 \right)$$

Algorithm Solve with respect to $\max_i \{ \varepsilon_i \}$

- $\varepsilon_1 = \max_i \{ \varepsilon_i \}$

$$\varepsilon_1 = \frac{1}{2} \sqrt{r_{11} - r_{22} - r_{33} + 1}$$

$$\varepsilon_2 = \frac{(r_{21} + r_{12})}{4\varepsilon_1}, \quad \varepsilon_3 = \frac{(r_{31} + r_{13})}{4\varepsilon_1}, \quad \varepsilon_4 = \frac{(r_{32} - r_{23})}{4\varepsilon_1}$$

- $\varepsilon_1 = \max_i \{\varepsilon_i\}$

$$\varepsilon_1 = \frac{1}{2} \sqrt{r_{11} - r_{22} - r_{33} + 1}$$

- $\varepsilon_2 = \max_i \{\varepsilon_i\}$

$$\varepsilon_2 = \frac{1}{2} \sqrt{-r_{11} + r_{22} - r_{33} + 1}$$

- $\varepsilon_3 = \max_i \{\varepsilon_i\}$

$$\varepsilon_3 = \frac{1}{2} \sqrt{-r_{11} - r_{22} + r_{33} + 1}$$

- $\varepsilon_4 = \max_i \{\varepsilon_i\}$

$$\varepsilon_4 = \frac{1}{2} \sqrt{1 + r_{11} + r_{22} + r_{33}}$$

Euler Parameters / Euler Angles

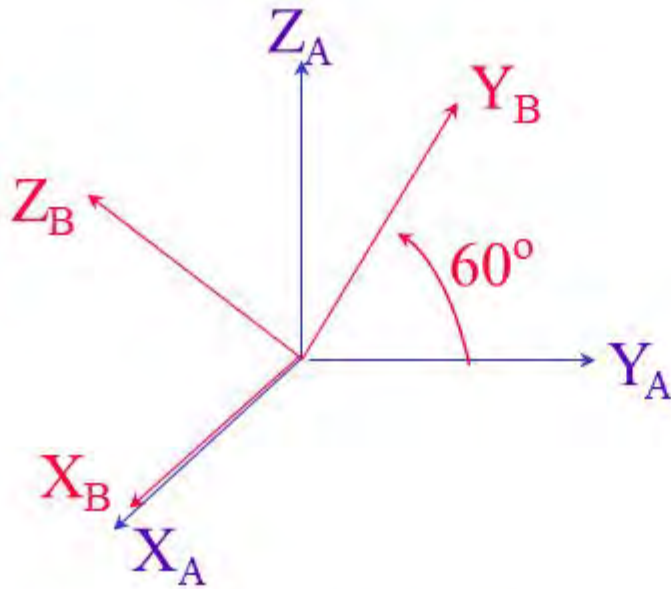
$$\varepsilon_1 = \sin \frac{\beta}{2} \cos \frac{\alpha - \gamma}{2}$$

$$\varepsilon_2 = \sin \frac{\beta}{2} \sin \frac{\alpha - \gamma}{2}$$

$$\varepsilon_3 = \cos \frac{\beta}{2} \sin \frac{\alpha + \gamma}{2}$$

$$\varepsilon_4 = \cos \frac{\beta}{2} \cos \frac{\alpha + \gamma}{2}$$

Quiz



Euler Parameters

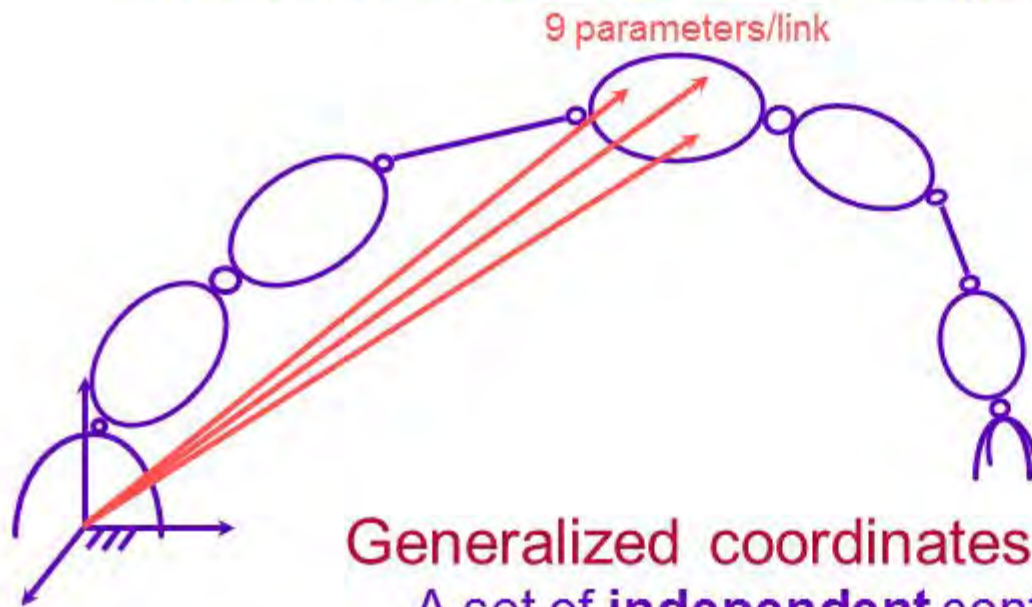
$$x_r = \begin{bmatrix} 1/2 \\ 0 \\ 0 \\ \sqrt{3}/2 \end{bmatrix}$$

Direction Cosines

$$x_r = \begin{bmatrix} 1 \\ 0 \\ 0 \\ 0 \\ 1/2 \\ \sqrt{3}/2 \\ 0 \\ -\sqrt{3}/2 \\ 1/2 \end{bmatrix} \begin{matrix} r_1 \\ r_2 \\ r_3 \end{matrix}$$

Configuration Parameters

A set of position parameters that describes the full configuration of the system.



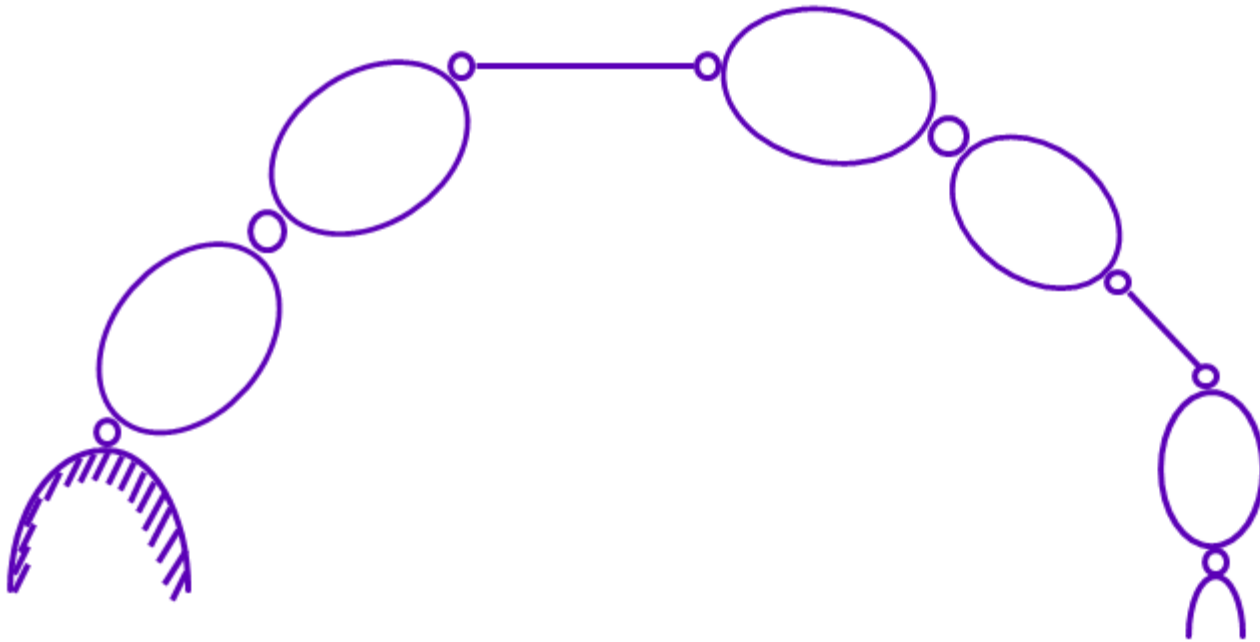
Generalized coordinates

A set of **independent** configuration parameters

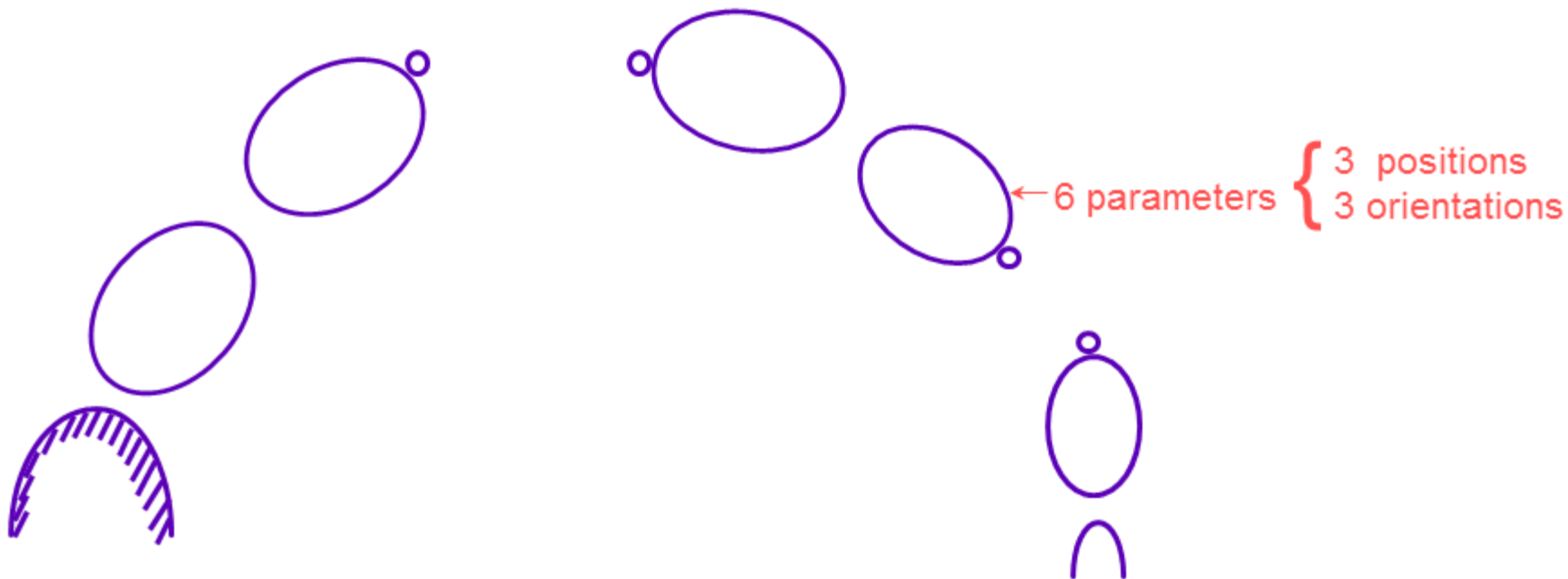
Degrees of Freedom

Number of generalized coordinates

Generalized Coordinates



Generalized Coordinates



n moving links: $6n$ parameters