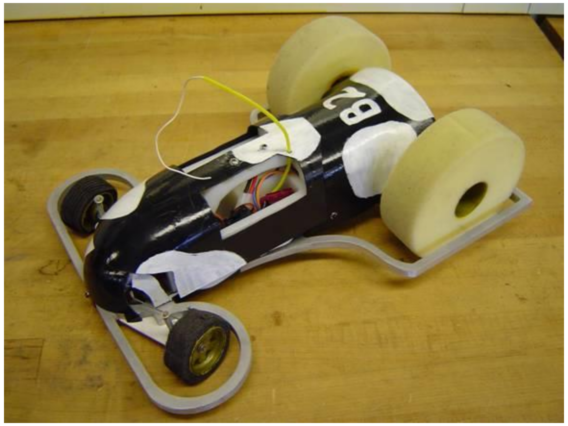
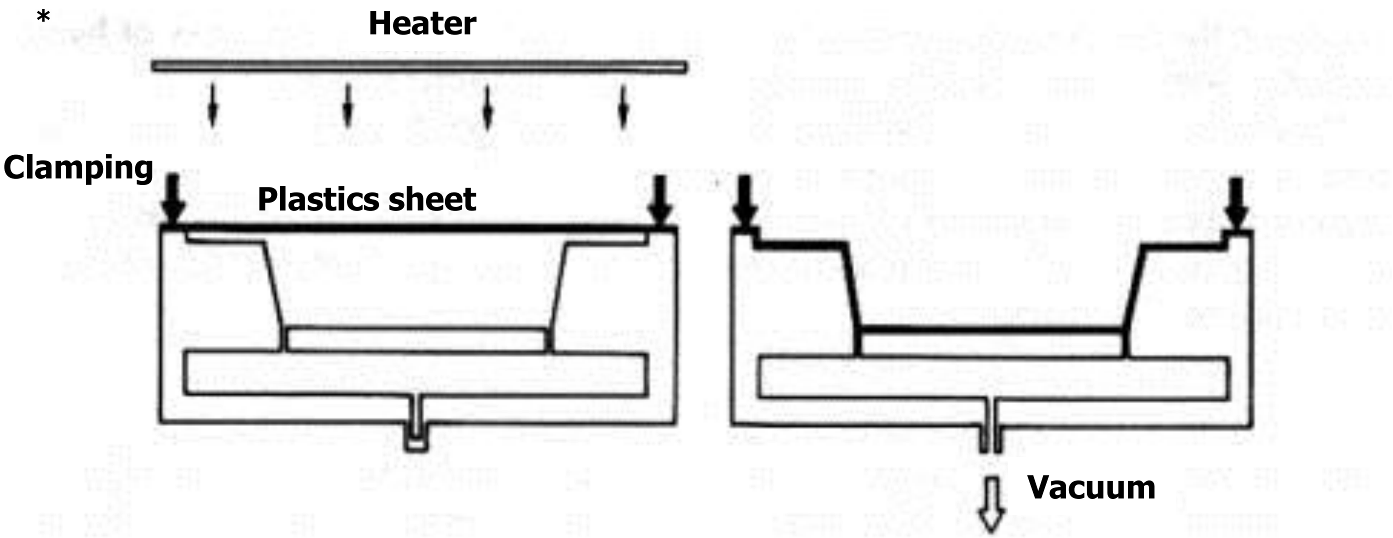


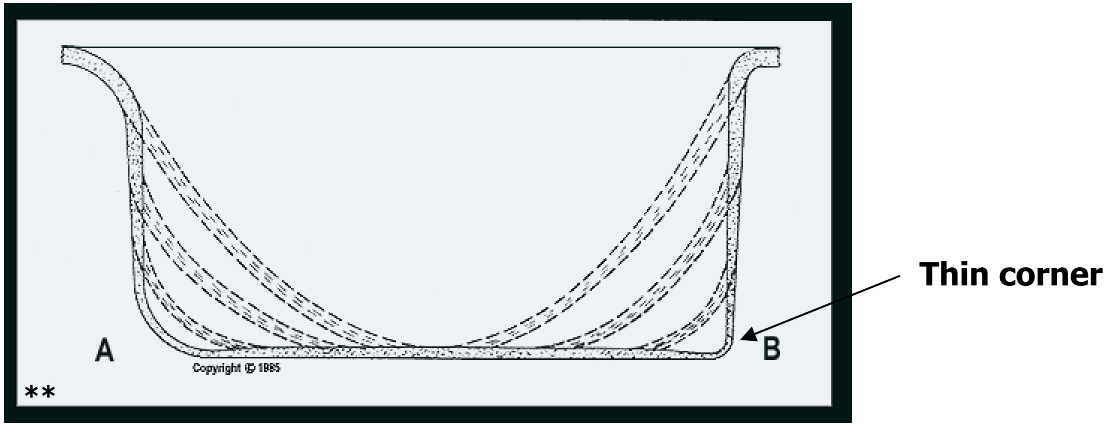
Thermoforming

2.810

T. Gutowski

Vacuum Thermoforming





* Source: R. Ogorkiewicz, “Engineering Properties of Thermoplastics.”; ** http://www.arrem.com/designguide/dgprocesscap.htm

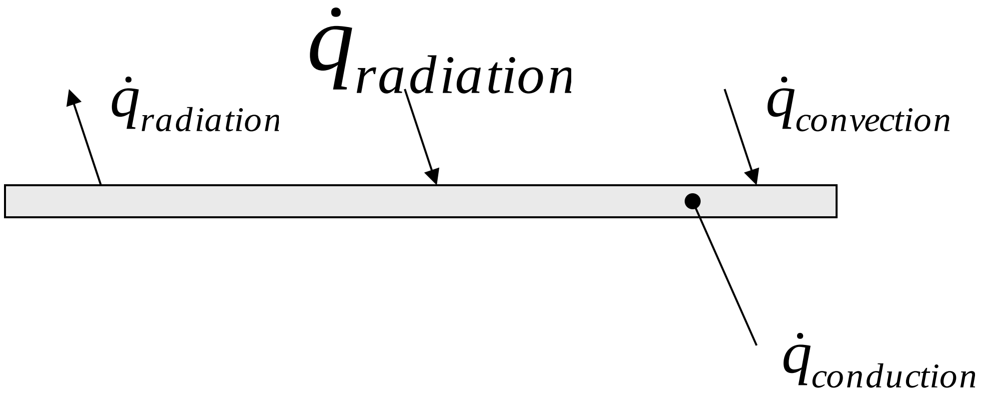
Thermoformed Parts

Some Basics

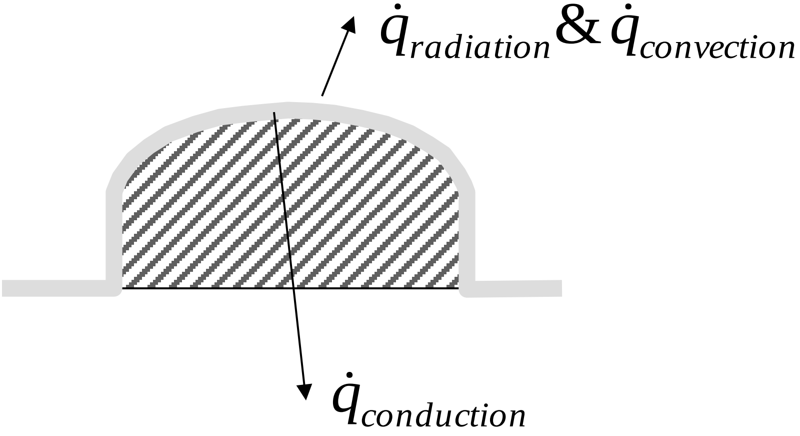
1. Heating and cooling
2. Viscoelastic behavior
   - Rubber elasticity
   - Time-Temperature behavior
3. Deformation patterns
4. Production equipment
5. Double diaphram forming

Heat Transfer in Thermoforming

Heating



Cooling



Radiation Heat Transfer between two parallel plates

$$\dot{q} = \frac{1}{\frac{1}{\varepsilon_1} + \frac{1}{\varepsilon_2} - 1} \sigma (T_1^4 - T_2^4)$$

$\sigma = 5.67 \times 10^{-8}$ W/m^{2}K^4

ex. ε_1 ε_2 = 1 (black bodies)

$T_1 = 533^{o}$K (heater)

$T_2 = 293^{o}$K (plastic at room temperature)

q = 4.2kW/m^2

at $T_2 = 180^{o}$C = 453^{o}K (forming temperature)

q = 2.3kW/m^2

See Lienhard Text Ch 10 on Radiation Heat Transfer

Heating Time est. (Kydex sheet)

$$\dot{q} = \rho w c \frac{\Delta T}{\Delta t}$$

ρ = 1.35 g/cm^3

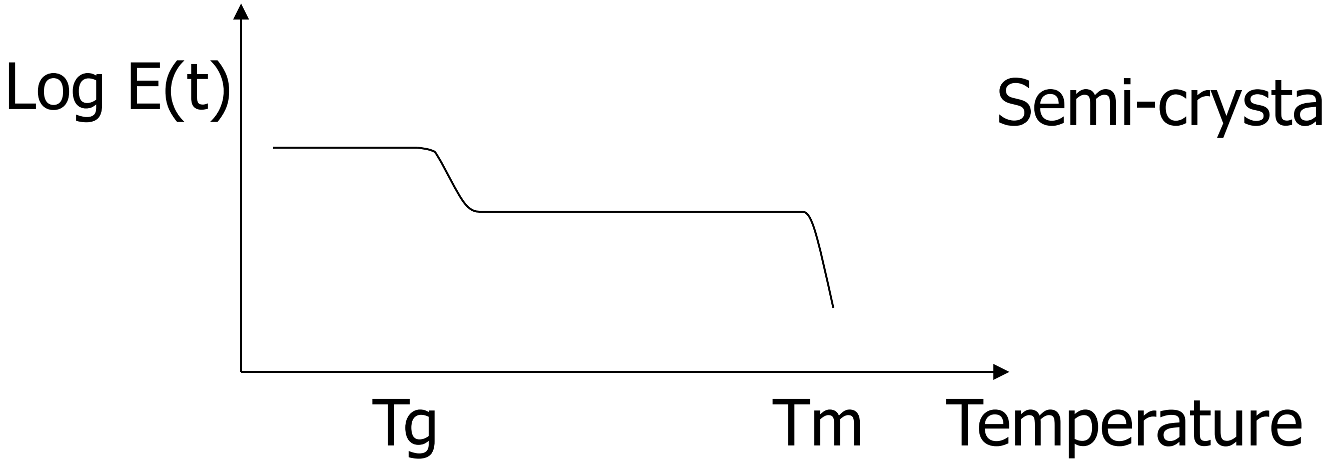
w = 1/16 in or 1.59 mm

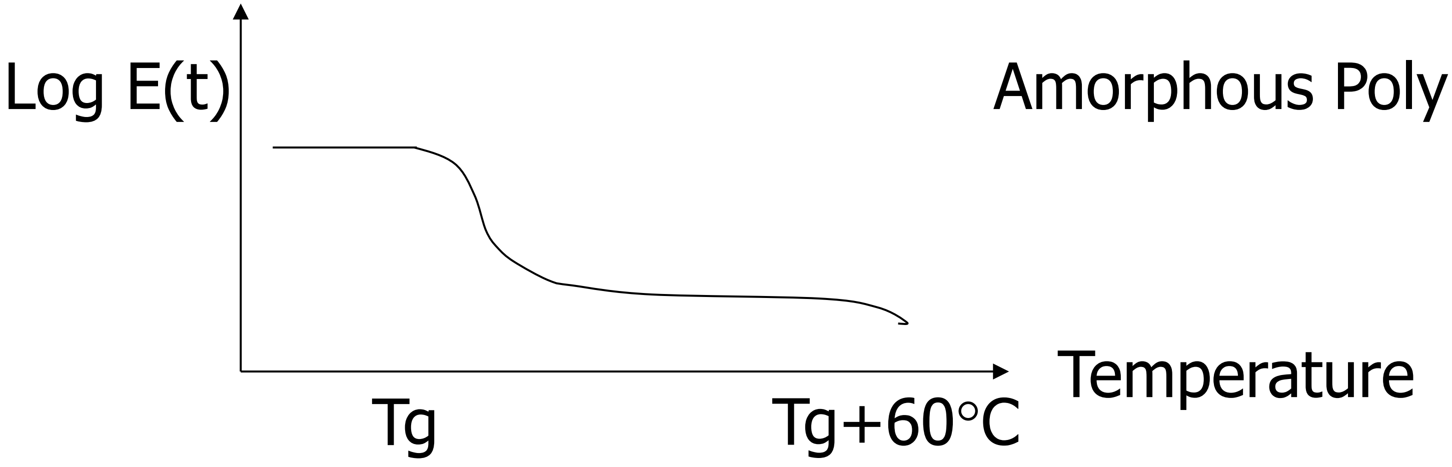
c = 1.21 J/g^{o}K

ΔT = 180 – 20 = 160^{o}K

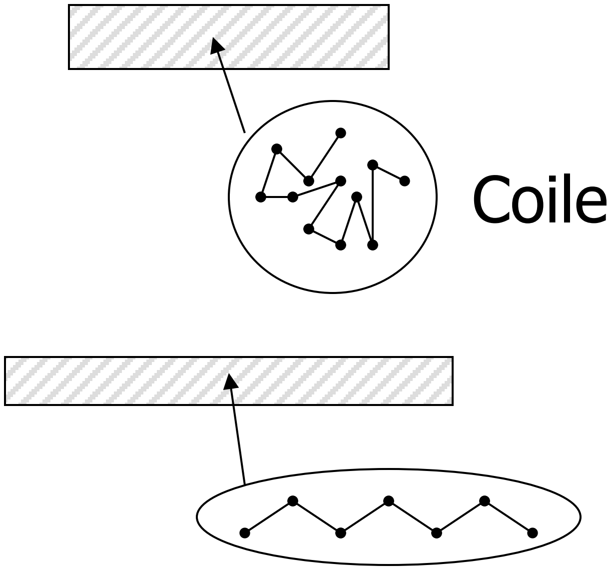
Δt = 130 sec

Temperature regimes for polymers


Semi-crystalline Polymer


Amorphous Polymer

Viscoelastic Effects During processing



Unloaded sample

Coiled polymer chain

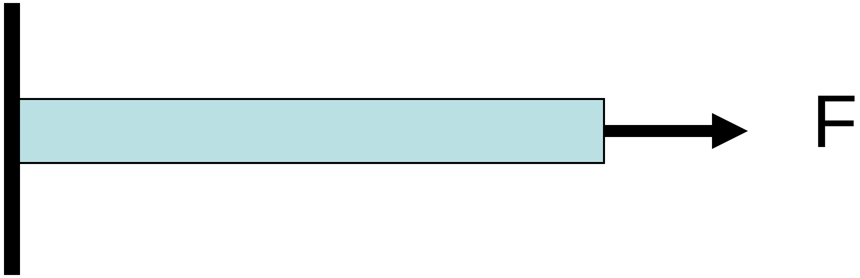
Loaded sample

Extended polymer chain

Polymer chains tend to exist in coiled configurations. Loading the sample can extend the chain and alter the mechanical behavior. Generally, abrupt, high rates of loading will extend the chain and lead to elastic effects. On the other hand, gradual slow rates of loading allow the chain to more or less retain its coiled configuration, with a resulting primarily viscous response

Simplified Rubber Elasticity

(No volume change)



QuickTime™ and a decompressor are needed to see this picture.

$\Delta W = F\,\Delta L = \Delta A = \Delta E - T\Delta S$

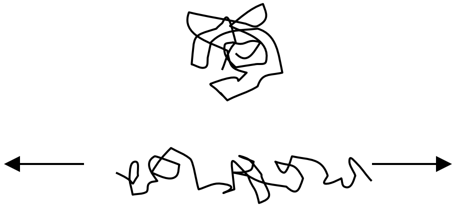
(A = Helmholtz free energy)

- Conventional materials

  $F = \Delta E/\Delta L$

- Rubber

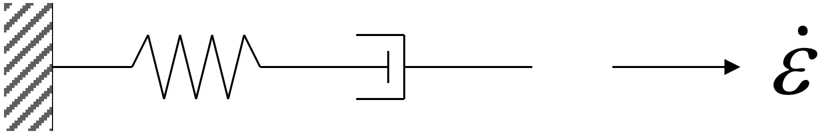
  $F = -T\,(\Delta S/\Delta L)$



Flory

note that upon extension the change in entropy is negative

Simple Viscoelastic System



Force Equilibrium: $\sigma_s = \sigma_d = \sigma$

Kinematic compatibility: $\dot{\varepsilon}_s + \dot{\varepsilon}_d = \dot{\varepsilon}$

Constitutive behavior: $\sigma_s = E\varepsilon_s ; \sigma_d = \mu\dot{\varepsilon}_d$

This gives $\frac{\mu}{E}\dot{\sigma} + \sigma = \mu\dot{\varepsilon}$

The viscoelastic Time constant is :

$$\lambda = \frac{\mu}{E} = \frac{\text{"Newtonian" Viscosity}}{\text{Elastic Modulus}}$$

Solution to : $\lambda\dot{\sigma} + \sigma = \mu\dot{\varepsilon}$ with I.C. $\sigma = 0$ at $t = 0$

$$\sigma = \mu\dot{\varepsilon}(1 - e^{-t/\lambda})$$

Large values of t / λ i.e. $t >> \lambda$

$\sigma \approx \mu\dot{\varepsilon}$ viscous behavior

Small values of t / λ i.e. $t << \lambda$

$$\sigma \approx \mu\dot{\varepsilon}(1 - (1 - t / \lambda)) = \mu\dot{\varepsilon}t/\lambda$$

let $\dot{\varepsilon} \cdot t = \varepsilon$, this gives

$\sigma \approx E\varepsilon$ elastic behavior

"FAST"	$t << \lambda$	Elastic
"SLOW"	$t >> \lambda$	Viscous
"INBETWEN"	$t \sim \lambda$	Viscoelastic

Temp. Dependence of Time constant, λ

$$\lambda = \frac{\mu}{E} \cong \frac{\mu_0 e^{\Delta E/RT}}{E_0 T}$$

Arrhenius

Rubber elasticity

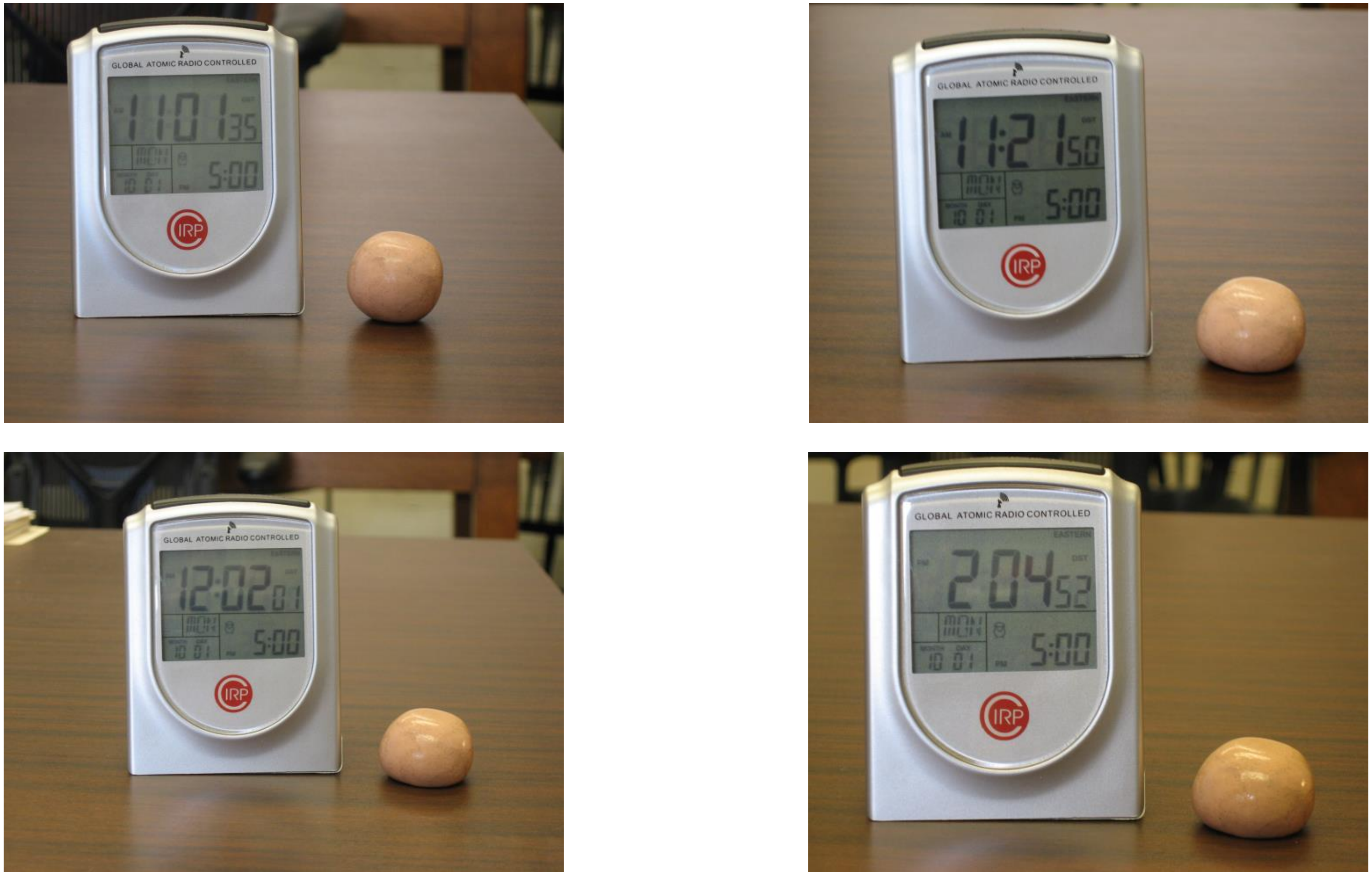
Approximation $$\lambda \cong \lambda_0 e^{\Delta E/RT}$$

(For better accuracy, use Time-Temp shift, WLF eqn.)

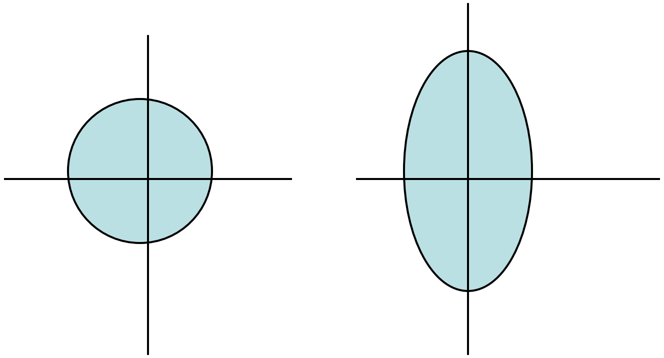
Example: PMMA

Temp	λ
40°C	114 yrs
100°C	T_g
135°C	3.5 millisec

Viscous behavior of “silly putty”



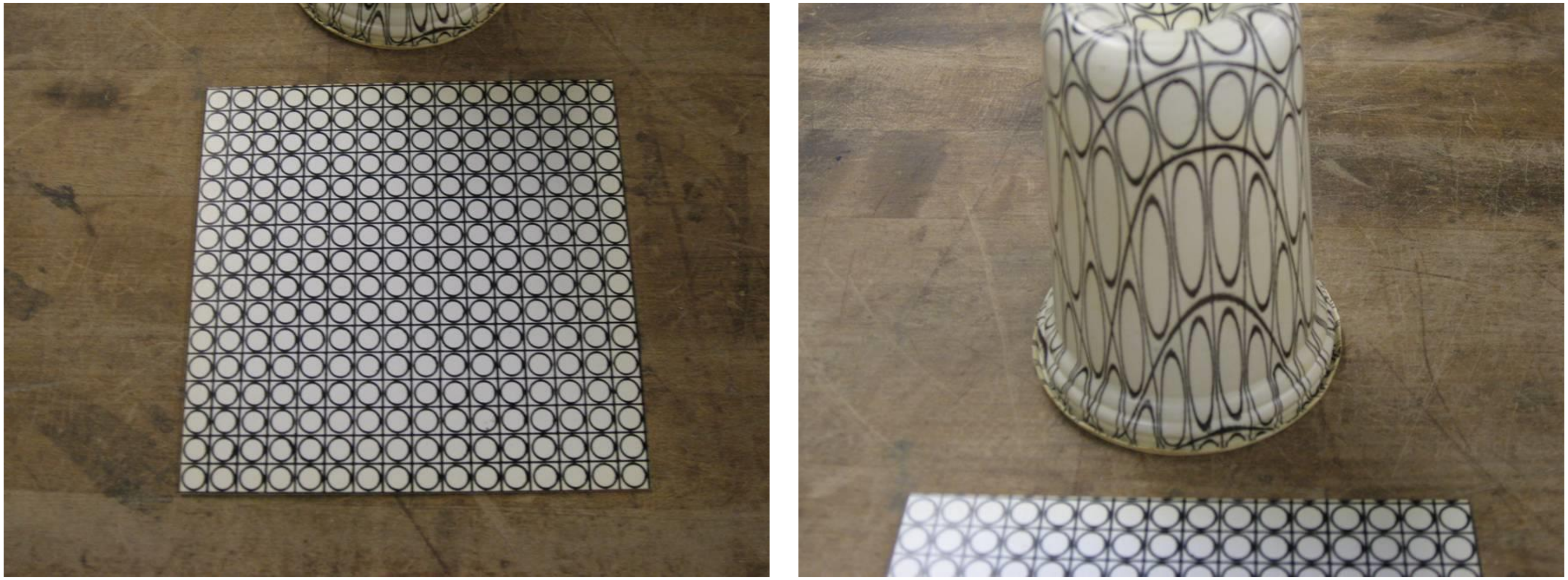
deformation patterns



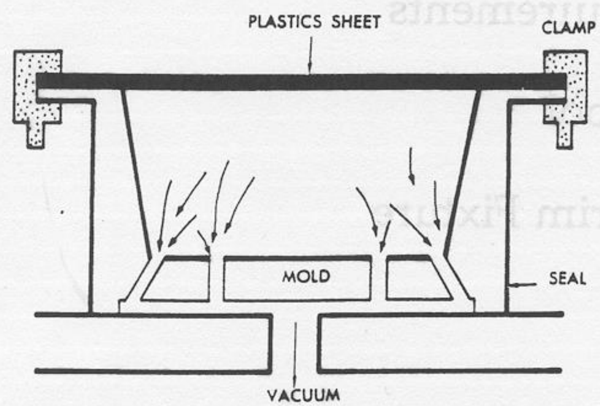
$$d(Ah) = A\,dh + h\,dA = 0$$

$$dA/A = -\,dh/h$$

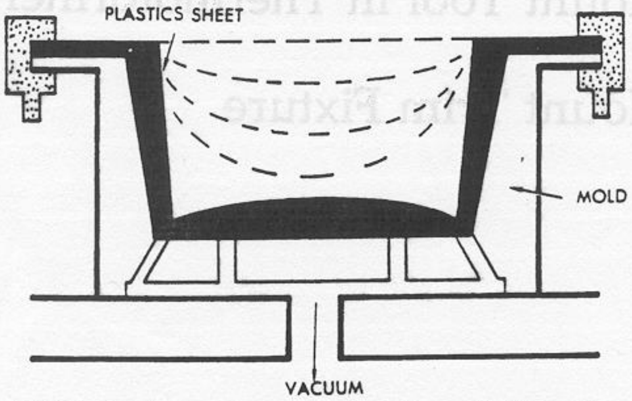
Deformation Patterns



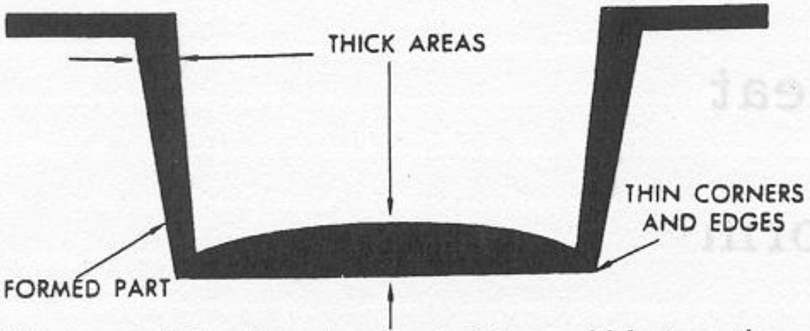
Thermoforming



(A) A clamped and heated plastic sheet is forced down into the mold by air pressure after a vacuum is drawn in the mold. (Atlas Vac Machine Co.)

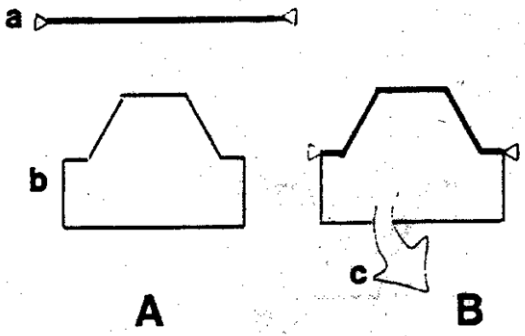


(B) Plastics sheet cools as it contacts the mold. (Atlas Vac Machine Co.)

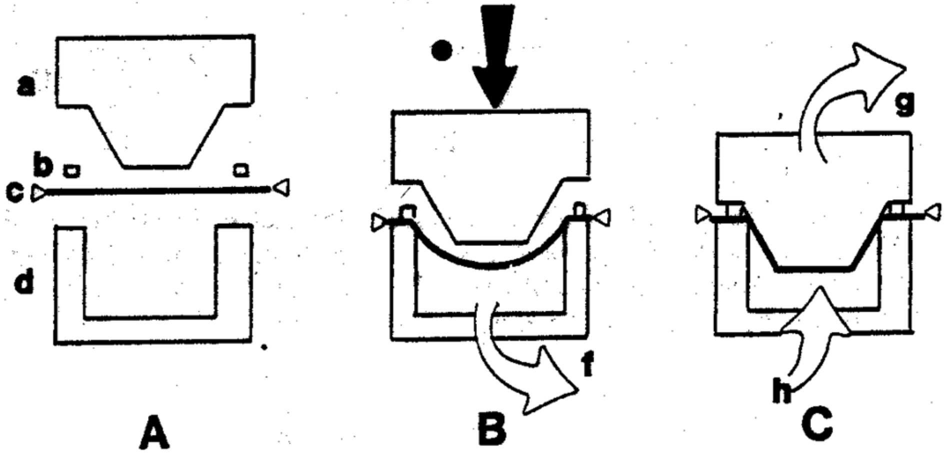


(C) Areas of the sheet that touched the mold last are the thinnest. (Atlas Vac Machine Co.)

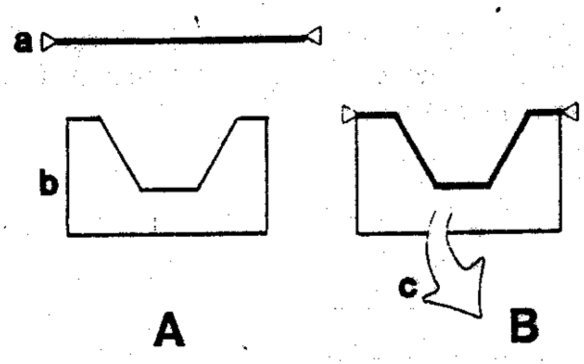
Variations on the process



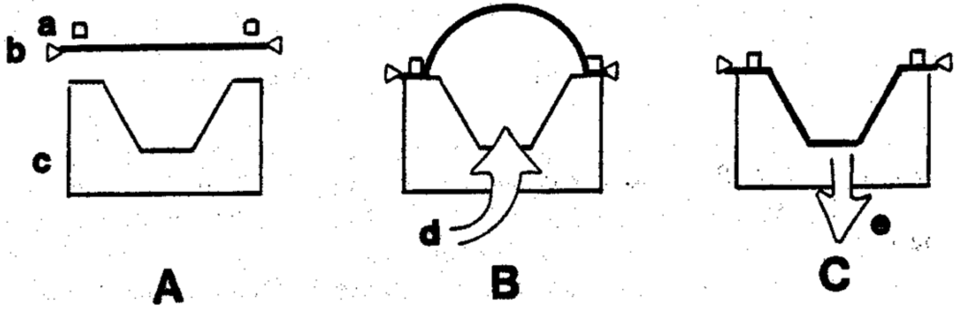
Drape Forming



Vacuum Snap-Back Forming



Vacuum Forming

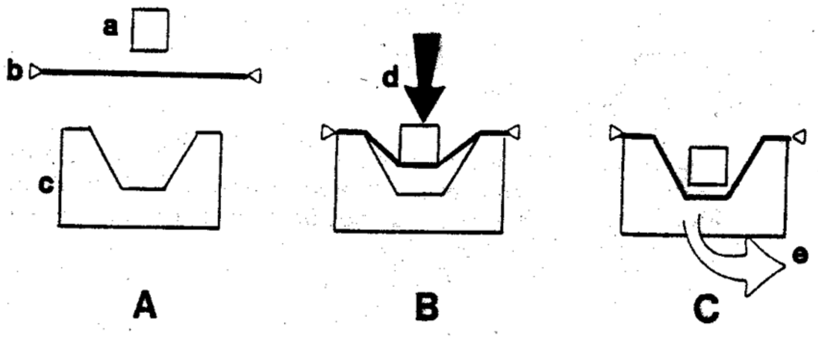


Billow Vacuum Forming

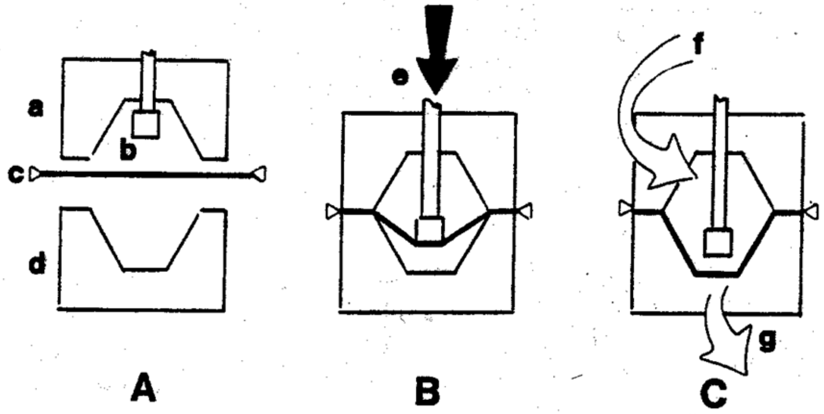
Thermoforming Patterns

Vacuum holes

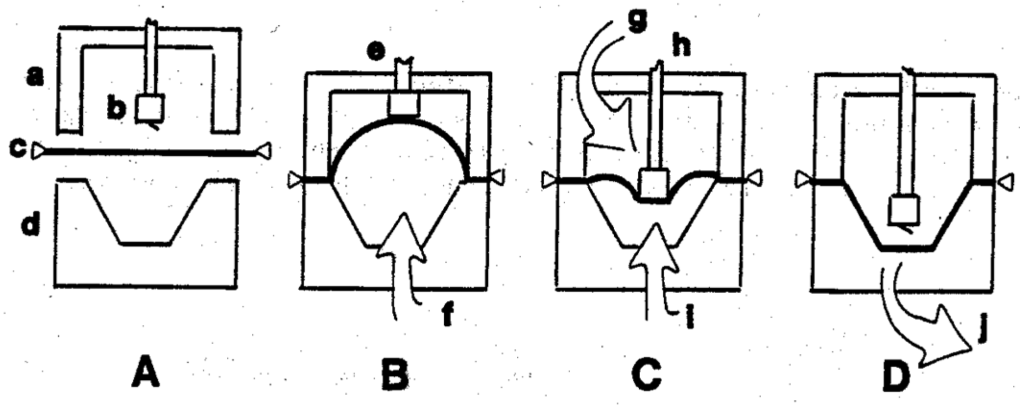
Variations on the process



Plug-assist Vacuum Forming

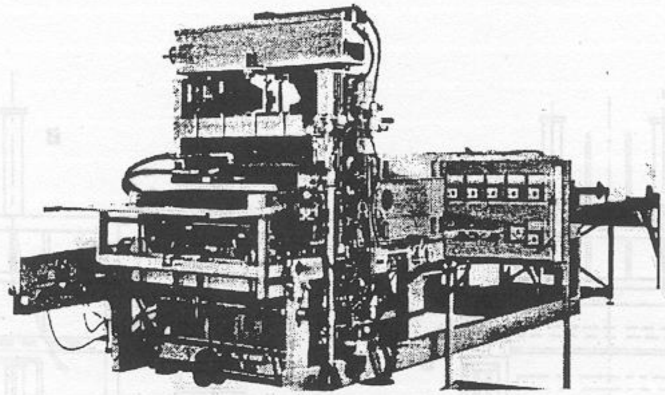


Plug-assist Pressure Forming

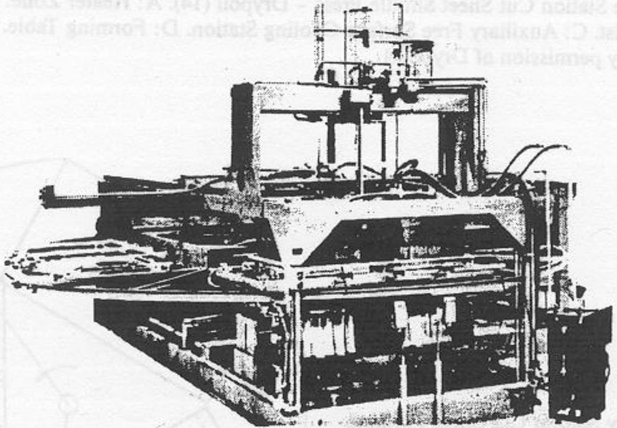


Pressure Reverse Draw with Plug-assisted

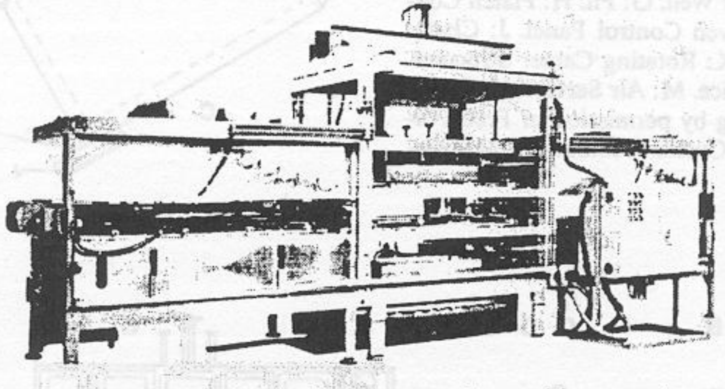
Production Equipment



(A) High-speed pressure/vacuum former operates from either roll stock or inline with an extruder.



(B) Rotary style of unit used for large industrial components at a fairly high production rate.



(C) Twin-sheet thermoforming machine with separate, independent clamping frames.

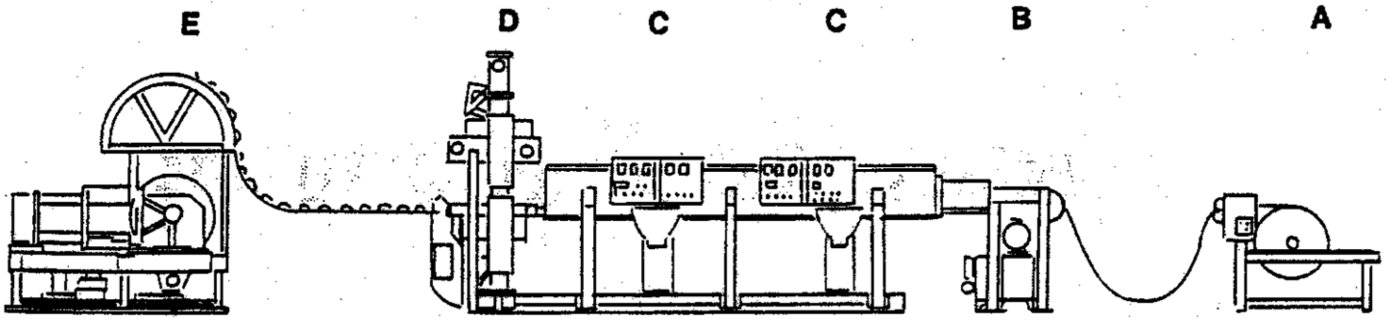


Figure 1.2 Schematic - Battenfeld Gloenco Rollfed Sheet + Thermoforming Line (13). A: Rollfed Sheet Take-off Station. B: Pin Chain Engagement. C: Heater Zone. D: Forming Station. E: In-Line Separate Mechanical Toggle-Clamp Trim Station.

Brown Machine: http://www.youtube.com/watch?v=hAlqrDiCu-M

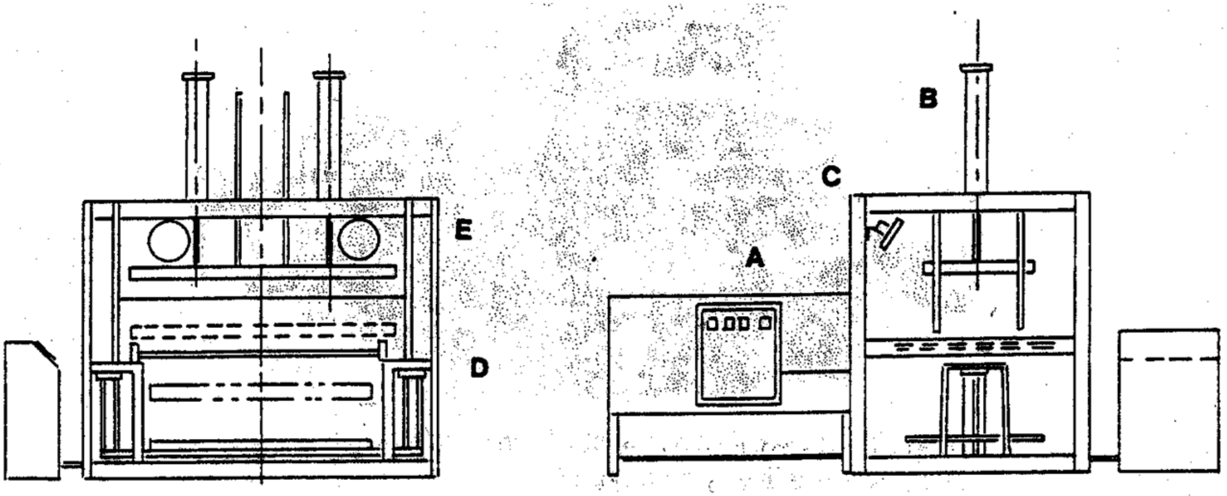


Figure 1.3 Single Station Cut Sheet Shuttle Press - Drypoll (14). A: Heater Zone. B: Pneumatic/Hydraulic Plug Assist. C: Auxiliary Free Surface Cooling Station. D: Forming Table. E: Vacuum Tanks. (Drawing used by permission of Drypoll.)

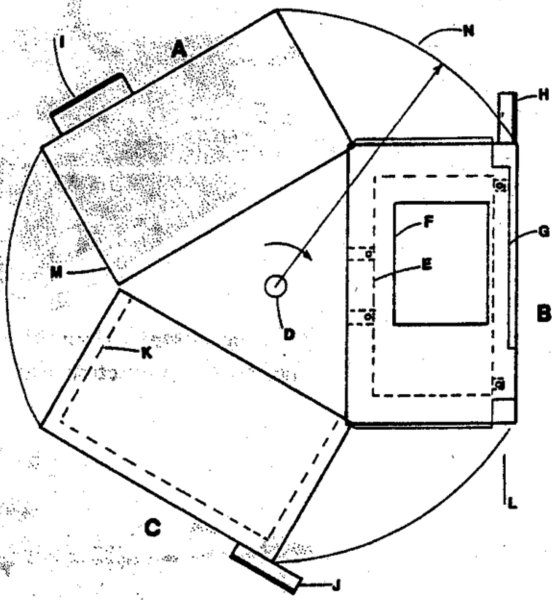


Figure 1.4 Rotary Station Cut Sheet Forming Press - Custom Automated Machinery (15). A: Heating Station. B: Forming Station. C: Load/Unload Station. D: Drive Center. E: Platen. F: Motor Well. G: Pit. H: Platen Control Panel. I: Oven Control Panel. J: Clamp Control Panel. K: Rotating Center Structure. L: Vacuum Service. M: Air Service. N: Safety Guard. (Drawing by permission of Fred Pollack, President, Custom Automated Machinery, Inc.)

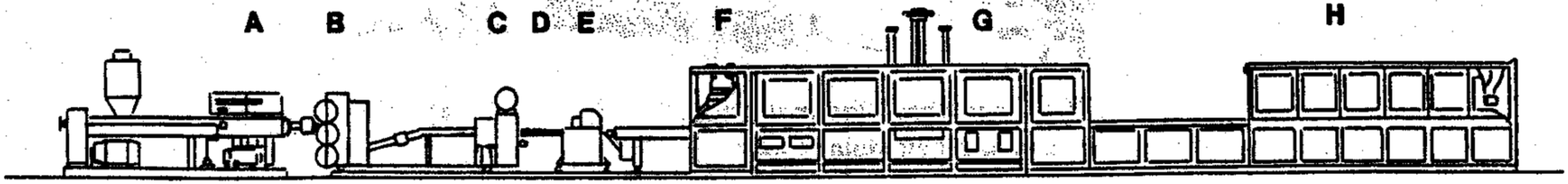


Figure 1.7 In-line Heavy-Gage Sheet Forming System - Shelly (13). A: Extruder. B: Down-Roll Stack and Cooling Table. C: Edge Trim. D: Hold-Down Table. E: Edge Clamp Engagement. F: Sheet Heating Zone. G: Forming Station. H: In-line Trimming Station.

Double Diaphragm Forming

Laminate wrinkling scaling laws: T. G. Gutowski et al.

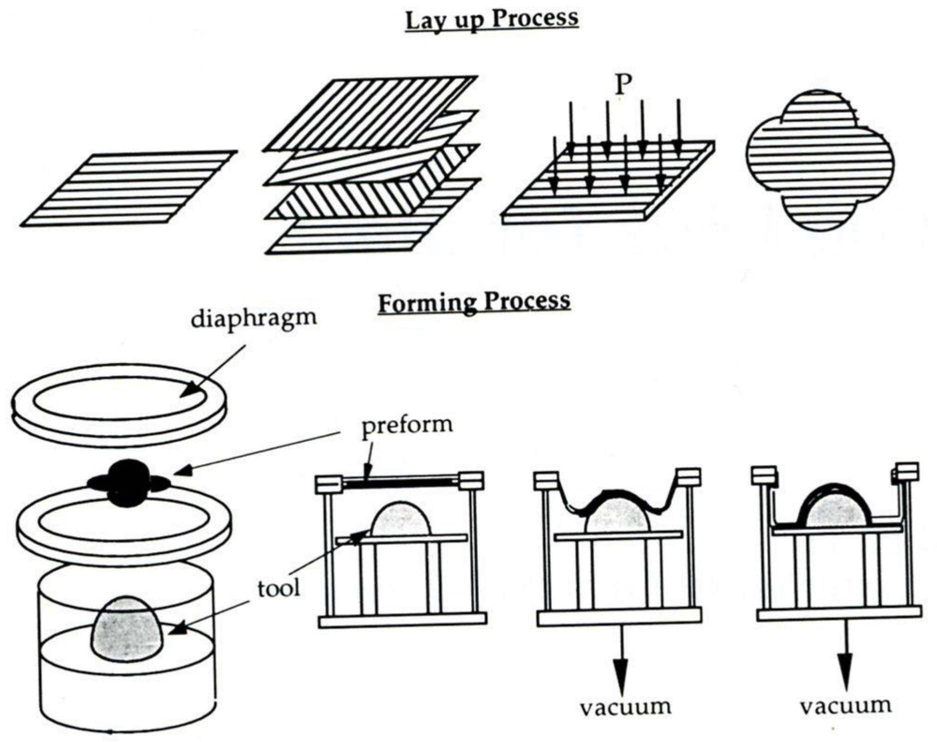


Figure 1 Schematic representation of the diaphragm forming process

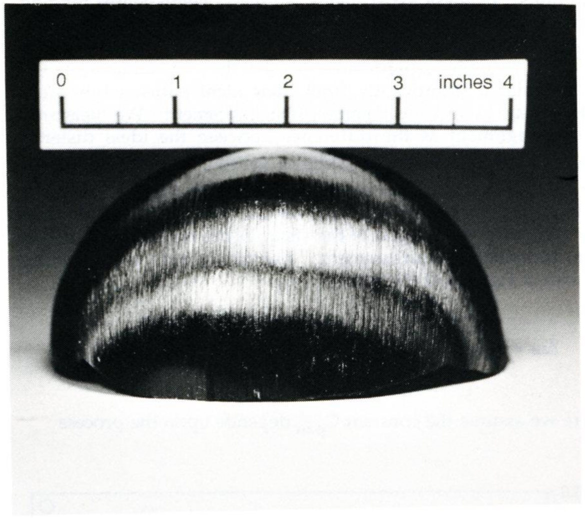


Fig.11 Hemisphere formed between elastic diaphragms

Temp, Time, Size & Shear

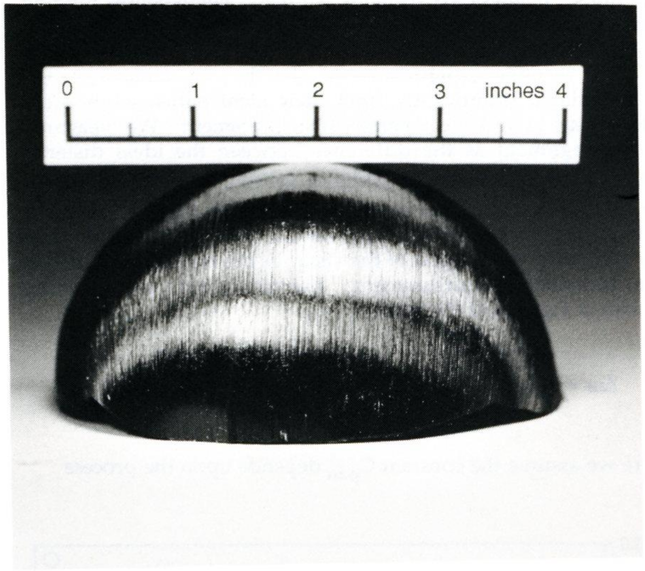
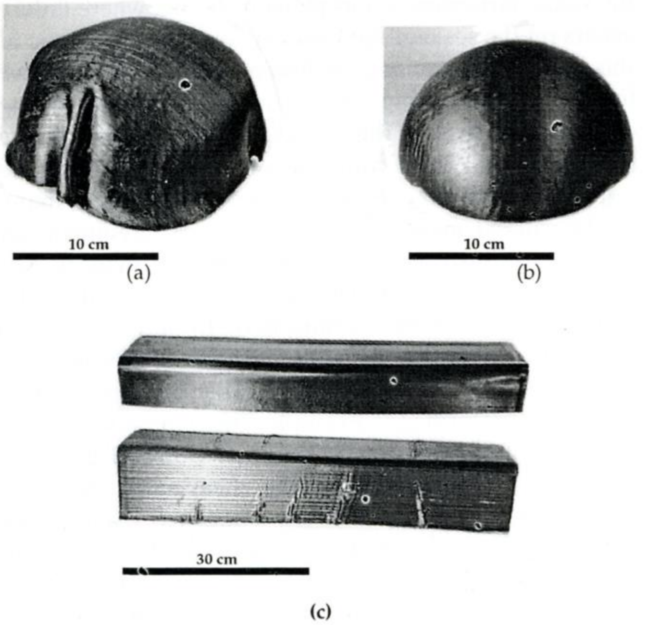


Fig.11 Hemisphere formed between elastic diaphragms



(a) (b)

(c)

Figure 3 (a) Illustration of laminate wrinkling on a 16-ply [0/90] hemisphere, (b) the same hemisphere formed without wrinkles and (c) laminate wrinkling on a C-channel

Ideal Shear Vs Actual

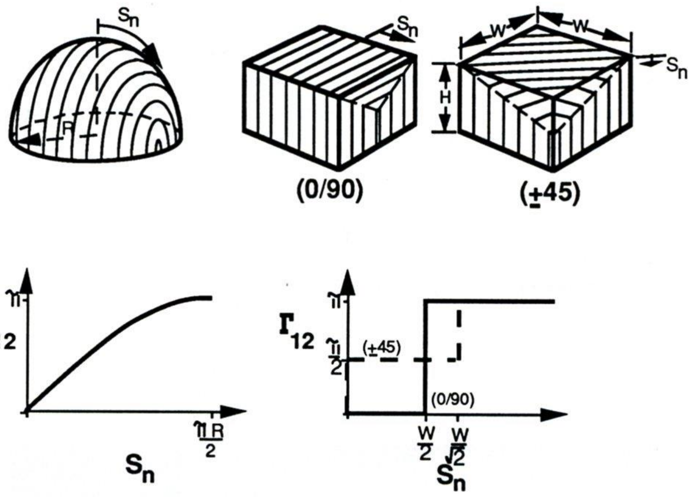


Fig.8 Fiber patterns and shear distributions for boxes and hemispheres

Laminate wrinkling scaling laws: T. G. Gutowski et al.

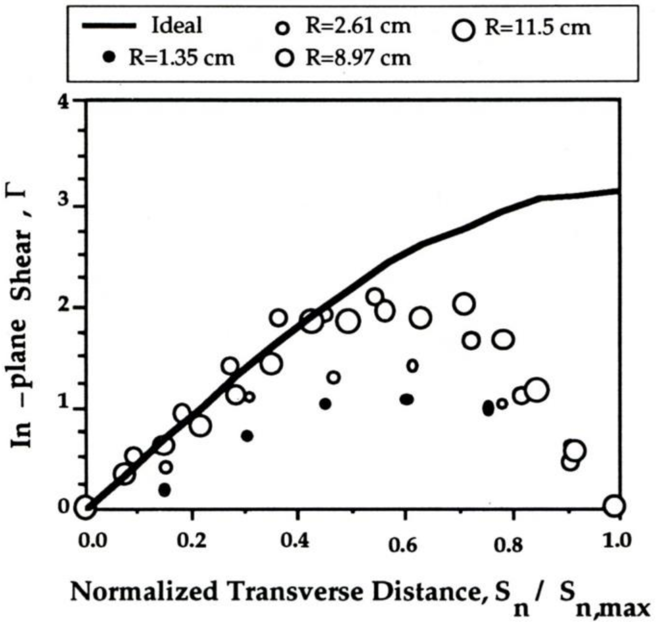


Figure 24 Comparison of ideal fibre and actual fibre shears for [0/90] hemispheres

Parts made in Lab

Laminate wrinkling scaling laws: T. G. Gutowski et al.

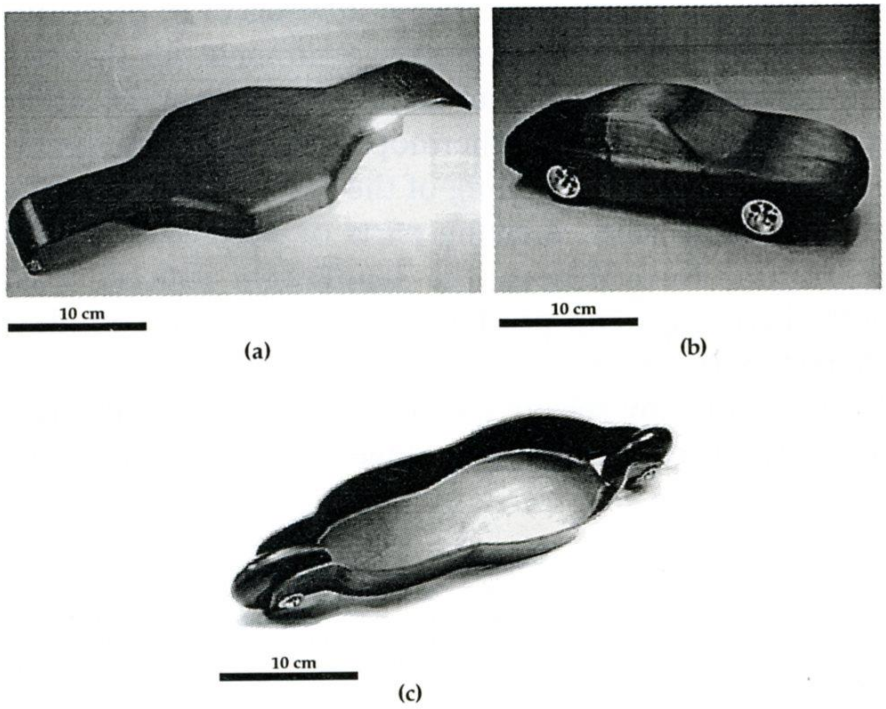
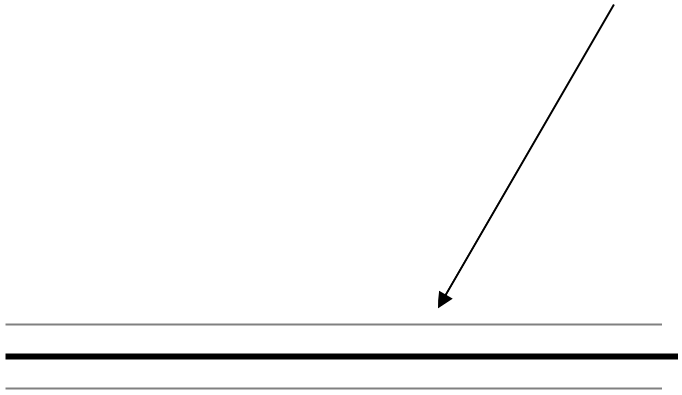
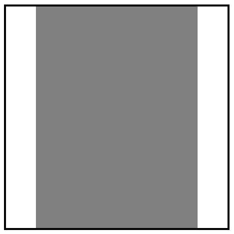


Figure 32 Thermoset matrix parts made by the diaphragm forming process: (a) chassis for a radio-controlled model car, (b) scale-model automotive body and (c) roller blade

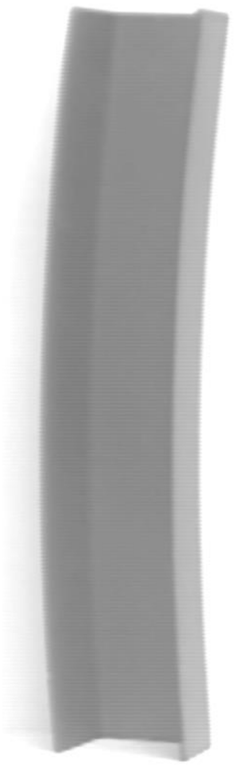
Double diaphragm forming





Forming
tool

Curing
tool



Former MIT grad student Sam Truslow

MIT Building 35

Prototype machine at Boeing

Diaphragm forming of Composites

Demo part for Boeing 777

More videos

http://www.youtube.com/watch?v=KPFAoLmJ5og

superplastic forming of aluminum at Kirkham University

http://www.youtube.com/watch?v=NPLWxxyIJcE&NR=1&feature=fvwp

thermoforming blow and then vacuum